

NACA RM L50B21

NACA

RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS
OF THE NACA 10-(5)(066)-03 PROPELLER

UNDER OPERATING CONDITIONS

By Albert J. Evans and Wallace Luchuk

Langley Aeronautical Laboratory
Langley Air Force Base, Va.

CLASSIFICATION CANCELLED

CLASSIFIED DOCUMENT

Authority *NACA R 7-2584* Date *8/2-7/54*
By *DATA 9/7/54* See *-----*
Information classified information affecting the National Defense of the United States within the meaning of the Espionage Act, USC 5011 was 82. Its transmission in the revelation of its contents in any manner to an unauthorized person is prohibited by law. Information so classified may be imparted to persons in the military and naval service of the United States, appropriate civilian officers and employees of the Federal Government who have a legitimate interest therein, and to United States citizens of known loyalty and discretion who if necessary must be informed thereof.

NATIONAL ADVISORY COMMITTEE
FOR AERONAUTICS

WASHINGTON

April 18, 1950

CONFIDENTIAL

UNCLASSIFIED

UNCLASSIFIED

NACA RM L50B21

~~CONFIDENTIAL~~

NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

RESEARCH MEMORANDUM

PRESSURE DISTRIBUTIONS ON THE BLADE SECTIONS
OF THE NACA 10-(5)(066)-03 PROPELLER
UNDER OPERATING CONDITIONS

By Albert J. Evans and Wallace Luchuk

SUMMARY

A broad investigation has been made in the Langley 16-foot high-speed tunnel to determine propeller section aerodynamic characteristics by measuring the surface pressure distribution on the airfoil sections of a rotating propeller. Five specially designed propellers incorporating NACA 16-series airfoil sections were tested. The design parameters of the five propellers covered a range of section thickness ratio and design camber.

This paper presents the data obtained from the tests of one of the five propellers. The present tests were conducted on the NACA 10-(5)(066)-03 propeller which had the highest cambered blades of the group. The design camber of all the sections tested was 0.5 and the thickness-chord ratio varied from 16 percent to 4 percent. The data are presented in tabular form as pressure coefficient, normal-force coefficient, chordwise-force coefficient, and moment coefficient. A geometric angle-of-attack range from -3.5° to 11° was covered in the Mach number range from 0.40 to 0.80. For higher Mach numbers, from 0.80 to 1.15, the section nominal angle of attack varied from -2.5° to 3.5° .

The results are presented as preliminary data for each propeller test made and no attempt has been made to analyze the data.

INTRODUCTION

Since propeller sections operate at speeds considerably higher than those encountered on other parts of an airplane, the propeller designer and analyst have continually been faced with a lack of airfoil data in the transonic speed range. At subsonic speeds above the critical speed of the airfoil nearly all available data are subject to wind-tunnel

~~CONFIDENTIAL~~

UNCLASSIFIED

choking effects, and attempts at extrapolation to higher values of Mach number have yielded uncertain results. Even if the two-dimensional data were available for supercritical values of Mach number, the effects of velocity gradient along the blade, the three-dimensional tip effects, and the action of the centrifugal force on the boundary layer along the blade impose problems that need to be investigated on the operating propeller.

As a first step toward obtaining propeller section data, tests were made in the Langley 16-foot high-speed tunnel whereby section aerodynamic characteristics were determined by measuring the surface pressure distributions on the operating propeller blade sections of an NACA 10-(3)(08)-03 propeller. Preliminary results of these tests are presented in reference 1.

The success of the initial investigation led to the inauguration of a broad program of tests during which five propellers were tested in the two-blade configuration and to a limited extent in the one-blade configuration. The five propellers were designed especially for this investigation and the design parameters covered a range of section thickness-chord ratio and a range of section design lift coefficient. The propellers tested are designated as follows:

NACA 10-(3)(066)-03
NACA 10-(3)(049)-03
NACA 10-(3)(090)-03
NACA 10-(5)(066)-03
NACA 10-(0)(066)-03

The results of the tests of the NACA 10-(3)(066)-03, the NACA 10-(3)(049)-03, and the NACA 10-(3)(090)-03 propellers were reported in references 2, 3, and 4, respectively. It is pointed out that the propeller designations as given in references 2 and 3 are in error in that the digits after the last hyphen in the designation should read 03 instead of 033.

This paper presents the results of the NACA 10-(5)(066)-03 propeller which is the highest cambered propeller of the present program. The results are presented as pressure coefficient, normal-force coefficient, pitching-moment coefficient, and chordwise-force coefficient in tabular form. No analysis of the data is presented other than that which is considered essential for a clear understanding of the data presented.

SYMBOLS

The symbols used throughout this paper, some of which are defined in figure 3, are as follows:

B	number of blades
b	blade chord, feet
c	distance from section leading edge to any point on the chord, feet
\bar{c}	distance from section leading edge to any point about which pitching moments are taken, feet
c_c	section chordwise-force coefficient
c_l	section lift coefficient
c_{ld}	blade-section design lift coefficient
c_m	section pitching-moment coefficient about the quarter-chord point
c_n	section normal-force coefficient
D	propeller diameter, feet
F_c	section chordwise pressure force, pounds
F_n	section normal pressure force, pounds
G	Goldstein induced-velocity correction factor for a finite number of blades
h	blade-section maximum thickness, feet
J	advance ratio (V/nD)
M	Mach number of advance
M_x	helical section Mach number $\left(M \sqrt{1 + \left(\frac{\pi x}{J} \right)^2} \right)$
m	section pitching moment, pound-feet
N	propeller rotational speed, rpm.

n	propeller rotational speed, rps
P	pressure coefficient $\left(\frac{p - p_0}{q_x} \right)$
p	static pressure at a point on the airfoil surface, pounds per square foot
p ₀	free-stream static pressure, pounds per square foot
q _x	resultant dynamic pressure at a radial station x, pounds per square foot $\left(\frac{1}{2} \rho W_0^2 \right)$
R	propeller-tip radius, feet
r	radius to a blade element, feet
r _p	polar ordinate, feet
s	distance along surface of blade section, feet
V	velocity of advance (corrected for wind-tunnel-wall interference effects), feet per second
W ₀	velocity vector $\left(V \sqrt{1 + \left(\frac{\pi x}{J} \right)^2} \right)$
W	resultant velocity at blade section, feet per second
w ₁	induced velocity at blade section, feet per second
x	fraction of propeller-tip radius (r/R)
y	normal distance from chord line to upper or lower surface of airfoil, inches
α _i	induced angle of attack, degrees
α _x	angle of attack of blade element, corrected for induced flow and blade deflection, at radial station x, degrees $(\beta_x - \phi + \Delta\beta)$
α _x '	geometric angle of attack of blade element at radial station x, degrees $(\beta_x - \phi_0)$
β	blade angle, degrees

$\beta_{0.75R}$	blade angle at 0.75 tip radius, degrees
β_x	blade angle at station x, degrees
$\Delta\beta$	change in blade angle caused by operation loads, degrees
γ	ratio of specific heats for air (1.4)
θ	polar angular ordinate, radians
ρ	mass density of air in free stream, slugs per cubic foot
σ	solidity $\left(B \frac{b}{D} / \pi x \right)$
ϕ	helix angle, degrees
ϕ_0	geometric helix angle, degrees $\left(\tan^{-1} (J/\pi x) \right)$
ψ	slope angle at the surface of the section, referenced to chord, degrees
ω	propeller rotational speed, radians per second
Subscripts:	
L	lower-surface value
U	upper-surface value

APPARATUS

Basic equipment.- The tests were made with the NACA 2000-horsepower propeller dynamometer in the Langley 16-foot high-speed tunnel. A complete description of the dynamometer is contained in reference 5. The pressure-transfer device used to transfer the pressures measured at the blade surface orifices from the rotating members of the test setup to the stationary manometers is described in reference 2 together with a description of the optical deflectometer. The deflectometer was necessary for an accurate determination of the blade-section angles of attack because the blades twisted due to the air loads and centrifugal force acting on the blade when the propeller was operating. A schematic diagram of the test setup is shown in figure 1.

Propellers.- The propeller blades were of solid duralumin construction and were designated the NACA 10-(5)(066)-03 design. The digits

in the propeller designation describe the propeller diameter and the airfoil section at the design radius ($\frac{r}{R} = 0.70$) as follows: propeller diameter, 10 feet; section design lift coefficient, 0.50; section thickness-chord ratio, 0.066; and solidity per blade, 0.03. The blades had a rectangular plan form with a blade width of 8 inches and were made up of NACA 16-series sections throughout having a design lift coefficient of 0.50 along the entire radius with the exception of a small portion near the tip. Due to inaccuracies in the fabrication process the section at the $\frac{r}{R} = 0.975$ station was not precisely an NACA 16-series section.

From measurements made at the $\frac{r}{R} = 0.975$ station the actual section was determined and the ordinates are given in table 1 together with a sketch of the actual section compared with an NACA 16-series section. Blade-form characteristic curves are presented in figure 2.

Twenty-four pressure tubes were imbedded in the surface of one of the blades together with a resistance thermometer imbedded in the thrust face. Details of the blade construction, pressure tube and orifice installation, and temperature measurements are described in reference 2.

TESTS

The tests were made at a blade-angle setting of 45° at the $\frac{r}{R} = 0.75$ station. For most of the tests a constant rotational speed was used and a range of advance ratio was covered by changing the tunnel airspeed, which was varied from about 215 to 500 miles per hour. At higher speeds, however, the dynamometer could not deliver sufficient torque for operation at constant rotational speed and for this reason high-speed data were obtained by operating the tunnel at constant high values of Mach number and the advance ratio was varied by changing rotational speed. The test procedure and techniques employed are described in detail in reference 2.

Pressure-distribution data were obtained on the sections located at the following stations with the test blade operating in a two-blade propeller; $\frac{r}{R} = 0.30, 0.45, 0.60, 0.70, 0.78, 0.85, 0.90, 0.95$, and 0.975 .

In order to extend the range of advance ratio to lower values and, consequently, to extend the range of angle of attack and normal-force coefficient to high values, pressure data were obtained on the section

at the $\frac{r}{R} = 0.95$ station with the test blade operating as a one-blade propeller. The details of the one-blade test procedure are also described in reference 2.

The range of Mach number and angle of attack covered and the operating conditions for each test are specified in tables 2 to 10. The table index provides an outline of the test schedule.

REDUCTION OF DATA

The following equations, which are explained in detail in reference 2, have been used in the reduction of the section data presented herein.

Section pressure coefficient:

$$P = \frac{P - P_o}{q_x} \quad (1)$$

Section normal force:

$$F_n = \int_0^b p \cos \psi \, ds = \int_0^b \left[(P_L - P_o) - (P_U - P_o) \right] dc \quad (2)$$

Section normal-force coefficient:

$$c_n = \frac{F_n}{q_x b} = \int_0^{1.0} (P_L - P_U) \frac{dc}{b} \quad (3)$$

Section chordwise force:

$$F_c = \int_0^b p \sin \psi \, ds = \int_0^b \left[(P_U - P_o) \tan \psi_U - (P_L - P_o) \tan \psi_L \right] dc \quad (4)$$

Section chordwise-force coefficient:

$$c_c = \frac{F_c}{q_x b} = \int_0^{1.0} \left[P_U \tan \psi_U - P_L \tan \psi_L \right] \frac{dc}{b} \quad (5)$$

or, in polar coordinates,

$$c_c = \int_0^{2\pi} (P) \left[\frac{\sin \psi}{\sin(\theta - \psi)} \right] \left(\frac{r_p}{b} \right) d\theta \quad (6)$$

Equation (5) was used to evaluate that portion of chordwise-force coefficient from $\frac{c}{b} = 0.025$ to $\frac{c}{b} = 1.0$ and equation (6) was used to evaluate the chordwise-force coefficient from $\frac{c}{b} = 0$ to $\frac{c}{b} = 0.025$.

Section pitching-moment coefficient:

$$c_m = \frac{m}{q_x b^2} = \frac{\bar{c}}{b} \int_0^{1.0} (P_L - P_U) \frac{dc}{b} - \int_0^{1.0} (P_L - P_U) \frac{c}{b} \frac{dc}{b} \quad (7)$$

where $\frac{\bar{c}}{b} = 0.25$.

Section angle of attack:

$$\alpha_x = \alpha_x' + \Delta\beta - \alpha_1$$

where α_1 , the induced angle of attack, was computed by use of Goldstein's correction for a finite number of blades as applied by Lock in reference 6 as described in reference 2.

The torsional deflection of the blades $\Delta\beta$ due to the combination of the air loads and centrifugal loads on the blades was measured during the tests as described in reference 2 and were verified by independent calculations. The accuracy of the measurements is believed to be within 0.1° .

For the one-blade propeller tests no torsional deflection measurements were made and values for the angle-of-blade twist for the one-blade tests were estimated by extrapolation of the two-blade data to lower values of advance ratio. The extrapolation was determined by computing the twist for the higher values of normal-force and moment coefficients obtained at the lower values of advance ratio with the one-blade propeller. A knowledge of the blade loading needed for calculating $\Delta\beta$ was obtained from wake-survey measurements made during the one-blade tests, and the moment coefficient was determined by extrapolation of the curve of moment coefficient against normal-force coefficient from the two-blade propeller tests. Some accuracy in the estimation of the value of the deflection angle was lost by the extrapolation process, but the values presented are believed to be within 0.2° . In certain cases

for which the values of the blade deflection angle were determined by extrapolations which were considered too great, or doubtful, the value of the angle has been omitted from the tables. Extrapolated values have been identified in the tables.

Values of the induced angles and the blade torsional deflection angles are presented for each test point in tables 2 to 10.

Tunnel-wall interference.- The data presented herein have been corrected to equivalent free air by the application of the Glauert tunnel-wall interference correction (reference 7).

RESULTS AND DISCUSSION

Pressure distribution.- The values of pressure coefficient obtained on the surface of the propeller sections are presented in tabular form in tables 2 to 10, and three typical pressure plots are shown in figure 4. The curves shown in figure 4 are plotted from the data presented in tables 8(a), 8(d), and 8(h). The three curves in figure 4 are plotted for a value of angle of attack close to 0° and are typical of the pressure distribution obtained in the subsonic and transonic speed ranges.

The symbols on the curves of figure 4 represent the chordwise points at which pressure orifices were located on the upper and lower surfaces of the blade section. The value of stagnation pressure on the leading edge of the section, which is recorded on the plots and appears in the data tables, was determined by computation from the equation

$$P = 1.0 + \frac{1}{4}M_x^2 + \frac{1}{4}\left(\frac{2 - \gamma}{6}\right)M_x^4$$

The value of the pressure coefficient at the trailing edge of the sections was determined from plots such as those in figure 4 by fairing the pressure-distribution curves of the upper and lower surface to a common value at the trailing edge. The notation "faired value" which appears in the data tables occurs wherever a pressure reading was either not obtained or was considered faulty.

The high negative pressure peaks near the nose on the lower surface of the section, shown in figure 4, were caused by a reverse curvature of the airfoil section. The reverse curvature of the section surface occurred because of the relatively high camber and low thickness ratio of the section at the $\frac{r}{R} = 0.90$ radius station.

Aerodynamic coefficients.- Values of normal-force coefficient, moment coefficient, and chordwise-force coefficient obtained by integration of the pressure-distribution plots are presented for each test run in tables 2 to 10. A detailed description of the method used to obtain values of chordwise-force coefficient is presented in reference 2.

A typical plot of the aerodynamic coefficients obtained is shown in figure 5 with propeller advance ratio as a common parameter. The propeller advance ratio provides a convenient parameter against which to plot the aerodynamic coefficients since both the angle of attack and section Mach number varied simultaneously during a test run. From plots such as the one illustrated in figure 5, cross plots can be made to obtain the variation of the aerodynamic coefficients with angle of attack or Mach number. The data plotted in figure 5 were obtained from table 8(d).

Induced angle.- The values of the section induced angle of attack presented herein have been computed by Goldstein's vortex theory as applied by Lock in reference 6. Goldstein's theory assumes that the blades operate with the Betz loading for minimum induced energy loss. The present blades were designed for the purpose of supplying section data on a given family of airfoil sections, and the loading was not considered in the design. As a consequence the test blades never operate with the ideal loading assumed in the theory used for calculating the induced angle of attack. The values of induced angle presented in the tables are therefore admittedly not precise, particularly for stations near the tip but are of sufficient interest to have warranted their calculation. Work is progressing on the problem of obtaining values of induced angle of attack for this propeller when operating with the arbitrary loadings obtained during the tests. An analysis of the problem of the calculation of the induced flow for propellers with arbitrary loading is beyond the scope of this paper, but some of the work that has been done on this problem has been reported in references 8, 9, and 10.

The relative magnitude of the induced angle of attack and the effect of its application on the lift-curve slope is shown for one section in figure 6. Figure 6 is a plot of normal-force coefficient against the uncorrected angle of attack $(\beta_x + \Delta\beta - \phi_0)$ compared with a plot of normal-force coefficient against angle of attack corrected for the induced angle $(\beta_x + \Delta\beta - \phi)$. Also shown in figure 6 is a plot of lift coefficient against angle of attack as determined from wind-tunnel tests on a two-dimensional model (reference 11). The application of the induced angle to the geometric angle of attack brought the lift curve for the propeller data much closer to that for the tunnel data. The lack of agreement between the propeller data and the wind-tunnel model data is due, in part, to the inexact value of induced angle used for correcting the angle of attack and may also be due to the fact that,

even though the correct value of induced angle were known, the boundary-layer flow on the blade due to centrifugal force and the presence of a Mach number gradient along the blade radius would affect the data obtained on the propeller blade so that it would not be in complete agreement with data from two-dimensional model tests.

Langley Aeronautical Laboratory
National Advisory Committee for Aeronautics
Langley Air Force Base, Va.

REFERENCES

1. Evans, Albert J., and Liner, George: Preliminary Investigation to Determine Propeller Section Characteristics by Measuring the Pressure Distribution on an NACA 10-(3)(08)-03 Propeller under Operating Conditions. NACA RM L8E11, 1948.
2. Maynard, Julian D., and Murphy, Maurice P.: Pressure Distributions on the Blade Sections of the NACA 10-(3)(066)-033 Propeller under Operating Conditions. NACA RM L9L12, 1950.
3. Gray, W. H., and Hunt, Robert M.: Pressure Distributions on the Blade Sections of the NACA 10-(3)(049)-033 Propeller under Operating Conditions. NACA RM L9L23, 1950.
4. Johnson, Peter J.: Pressure Distributions on the Blade Sections of the NACA 10-(3)(090)-03 Propeller under Operating Conditions. NACA RM L50A26, 1950.
5. Corson, Blake W., Jr., and Maynard, Julian D.: The NACA 2000-Horsepower Propeller Dynamometer and Tests at High Speed of an NACA 10-(3)(08)-03 Two-Blade Propeller. NACA RM L7L29, 1948.
6. Lock, C. N. H., and Yeatman, D.: Tables for Use in an Improved Method of Airscrew Strip Theory Calculation. R. & M. No. 1674, British A.R.C., 1935.
7. Glauert, H.: The Elements of Aerofoil and Airscrew Theory. American ed., The Macmillan Co., 1943, pp. 222-226.
8. Theodorsen, Theodore: The Theory of Propellers. II - Method for Calculating the Axial Interference Velocity. NACA Rep. 776, 1944.
9. Kawada, Sandi: Calculation of Induced Velocity by Helical Vortices and Its Application to Propeller Theory. Rep. No. 172, (vol. XIV, 1), Aero. Res. Inst., Tokyo Imperial Univ., Jan. 1939.
10. Tsien, Hsue-Shen, and Lees, Lester: The Glauert-Prandtl Approximation for Subsonic Flows of a Compressible Fluid. Jour. Aero. Sci., vol. 12, no. 2, April 1945, pp. 173-187, 202.
11. Lindsey, W. F., Stevenson, D. B., and Daley, Bernard N.: Aerodynamic Characteristics of 24 NACA 16-Series Airfoils at Mach Numbers between 0.3 and 0.8. NACA TN 1546, 1948.

TABLE INDEX

Table 1.- Ordinates for the Blade Section at the 0.975 Radius of the
NACA 10-(5)(066)-03 Propeller

Table 2.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-516.25 Propeller Blade Section ($x = 0.30$; $\beta_x = 68.78^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 3.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-510.00 Propeller Blade Section ($x = 0.45$; $\beta_x = 59.25^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 4.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-507.50 Propeller Blade Section ($x = 0.60$; $\beta_x = 51.33^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 5.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-506.62 Propeller Blade Section ($x = 0.70$; $\beta_x = 47.00^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 6.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-505.85 Propeller Blade Section ($x = 0.78$; $\beta_x = 43.90^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 7.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-505.30 Propeller Blade Section ($x = 0.85$; $\beta_x = 41.10^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

Table 8.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-504.80 Propeller Blade Section ($x = 0.90$; $\beta_x = 39.50^\circ$;
 $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

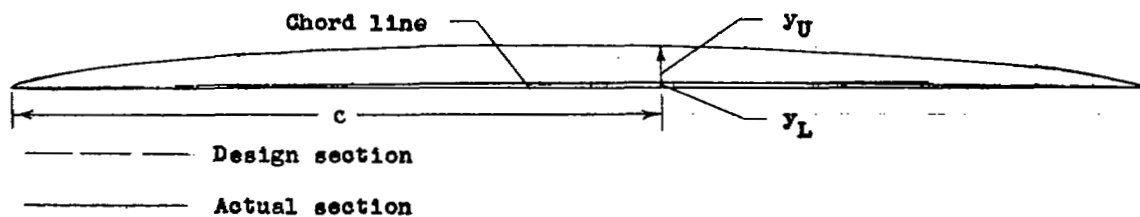
Table 9.- Pressure Coefficients and Aerodynamic Characteristics of an
NACA 16-504.40 Propeller Blade Section ($x = 0.95$; $\beta_x = 38.35^\circ$;
 $\beta_{0.75R} = 45^\circ$)

- (a) $N = 1140$ rpm; $B = 2$
- (b) $N = 1350$ rpm; $B = 2$
- (c) $N = 1500$ rpm; $B = 2$
- (d) $N = 1600$ rpm; $B = 2$
- (e) $M = 0.56$; $B = 2$
- (f) $M = 0.58$; $B = 2$
- (g) $M = 0.60$; $B = 2$
- (h) $M = 0.65$; $B = 2$
- (i) $N = 1500$ rpm; $B = 1$
- (j) $M = 0.56$; $B = 1$
- (k) $M = 0.58$; $B = 1$
- (l) $M = 0.60$; $B = 1$
- (m) $M = 0.65$; $B = 1$

Table 10.- Pressure Coefficients and Aerodynamic Characteristics of the
Blade Section ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)

- (a) $N = 1140$ rpm
- (b) $N = 1350$ rpm
- (c) $N = 1500$ rpm
- (d) $N = 1600$ rpm
- (e) $M = 0.56$
- (f) $M = 0.58$
- (g) $M = 0.60$
- (h) $M = 0.65$

TABLE 1.- ORDINATES FOR THE BLADE SECTION AT THE 0.975 RADIUS OF
THE NACA 10-(5)(066)-03 PROPELLER



c (in.)	y_U (in.)	y_L (in.)
0	0	0
.048	.028	.006
.10	.040	.008
.20	.062	.009
.40	.102	.010
.60	.134	.006
.80	.161	.004
1.20	.203	.006
1.60	.235	.008
2.00	.263	-.005
2.40	.283	-.022
3.20	.305	-.028
4.00	.312	-.032
4.80	.296	-.028
5.60	.267	-.023
6.40	.212	-.020
7.20	.158	-.015
7.60	.097	-.008
8.00	0	0

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	J	1.661	1.811	1.949	2.095	2.236	2.432	2.614	2.715	2.658	2.554	2.361	2.176	2.035	1.887	1.752
M_{∞}	σ_{T1}	.336	.361	.383	.403	.427	.459	.489	.508	.497	.477	.445	.416	.393	.369	.351
$\Delta\delta$	0	8.27	6.19	4.51	2.92	1.55	-.12	-1.47	-2.16	-1.78	-1.04	.46	2.12	3.55	5.24	6.98
α_1	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
c_n	1.75	1.36	1.06	.78	.50	.18	-.05	-.16	-.10	.06	.30	.63	.89	1.19	1.51	1.75
c_m	.7174	.5677	.4503	.3368	.2165	.0794	-.0242	-.0723	-.0439	.0258	.1303	.2710	.3813	.5039	.6245	.752
c_e	-.0051	-.0090	-.0131	-.0170	-.0186	-.0217	-.0313	-.0338	-.0313	-.0272	-.0198	-.0172	-.0174	-.0107	-.0087	-.0087
c/b	Pressure coefficient, P															
Upper surface	$\alpha 0.000$	1.029	1.033	1.037	1.042	1.047	1.054	1.061	1.066	1.063	1.058	1.051	1.044	1.040	1.035	1.031
	.025	-1.373	-.833	-.461	-.151	.103	.365	.549	.630	.587	.493	.292	.002	-.257	-.611	-1.030
	.050	-1.521	-1.163	-.871	-.614	-.385	-.127	.063	.099	.099	-.002	-.212	-.490	-.720	-1.004	-1.297
	.100	-1.266	-1.042	-.840	-.667	-.499	-.306	-.162	-.098	-.136	-.206	-.368	-.572	-.741	-.934	-1.127
	.200	-1.123	-.992	-.871	-.767	-.652	-.518	-.417	-.373	-.398	-.445	-.563	-.699	-.809	-.934	-1.044
	.300	-.927	-.846	-.762	-.701	-.620	-.529	-.457	-.432	-.449	-.477	-.557	-.650	-.727	-.802	-.882
	.400	-.853	-.808	-.754	-.715	-.652	-.591	-.542	-.527	-.537	-.547	-.607	-.673	-.727	-.777	-.827
	.500	-.721	-.703	-.668	-.649	-.605	-.566	-.537	-.532	-.537	-.535	-.575	-.619	-.657	-.686	-.716
	.600	-.602	-.620	-.610	-.610	-.582	-.553	-.532	-.555	-.557	-.545	-.563	-.589	-.608	-.616	-.620
	.700	-.416	-.460	-.465	-.475	-.459	-.457	-.460	-.470	-.466	-.445	-.451	-.458	-.468	-.466	-.448
	.800	-.185	-.209	-.215	-.208	-.195	-.206	-.230	-.250	-.240	-.208	-.197	-.199	-.204	-.219	-.200
Lower surface	.900	-.093	-.009	.039	.051	.084	.110	.126	.123	.122	.129	.109	.072	.048	.017	-.042
	.950	-.077	0	.057	.054	.084	.119	.136	.136	.136	.139	.113	.072	.055	.037	-.024
	$\alpha 0.000$.653	.443	.261	.034	-.179	-.493	-.792	-.961	-.867	-.652	-.374	-.072	.059	.348	.530
	.075	.447	.277	.139	-.029	-.170	-.373	-.557	-.672	-.611	-.469	-.298	-.095	.044	.204	.346
	.150	.271	.139	.042	-.079	-.172	-.309	-.428	-.498	-.459	-.367	-.257	-.122	-.023	.087	.193
	.250	.158	.057	-.020	-.114	-.185	-.281	-.360	-.418	-.387	-.315	-.245	-.148	-.075	.014	.096
	.350	.074	-.013	-.075	-.149	-.201	-.273	-.337	-.380	-.361	-.299	-.247	-.169	-.116	-.049	.022
	.450	-.014	-.091	-.145	-.212	-.252	-.309	-.377	-.389	-.373	-.325	-.286	-.225	-.182	-.127	-.056
	.550	-.077	-.139	-.176	-.225	-.258	-.298	-.333	-.359	-.349	-.307	-.283	-.235	-.204	-.165	-.117
	.650	-.141	-.178	-.193	-.236	-.256	-.281	-.302	-.323	-.314	-.284	-.271	-.238	-.216	-.190	-.172
	.750	-.181	-.209	-.215	-.236	-.246	-.256	-.257	-.269	-.265	-.245	-.251	-.235	-.224	-.215	-.190
	.850	-.181	-.191	-.173	-.180	-.170	-.166	-.152	-.152	-.153	-.146	-.168	-.171	-.171	-.181	-.177
	.925	-.137	-.130	-.091	-.082	-.064	-.050	-.027	-.023	-.025	-.025	-.053	-.068	-.082	-.111	-.126
	.975	-.112	-.087	-.020	-.008	.014	.035	.065	.073	.067	.063	.029	.005	-.009	-.049	-.088
	$\alpha 1.000$	-.106	-.066	.024	.036	.056	.099	.114	.128	.118	.110	.072	.043	.036	-.012	-.063

^aNo orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	1.801	1.925	2.061	2.188	2.372	2.522	2.657	2.576	2.431	2.271	2.125	1.986	1.852
M_x	.416	.439	.465	.490	.527	.556	.583	.568	.535	.503	.476	.449	.425
α_x	6.32	4.79	3.27	2.00	.37	-.81	-1.77	-1.20	-.11	1.24	2.62	4.09	5.67
$\Delta\theta$.02	.02	.01	.01	0	0	-.01	-.01	0	0	.01	.01	.02
α_1	1.42	1.13	.86	.57	.26	0	-.16	-.05	.14	.42	.72	1.02	1.29
c_{D1}	.5935	.4768	.3690	.2477	.1155	-.0013	-.0723	-.0245	.0632	.1806	.3116	.4348	.5445
c_{D2}	-.0033	-.0093	-.0151	-.0172	-.0179	-.0213	-.0262	-.0275	-.0203	-.0172	-.0151	-.0134	-.0046
c_c													
c/b	Pressure coefficient, P												
Upper surface	a_0	1.044	1.049	1.055	1.062	1.071	1.079	1.087	1.083	1.073	1.065	1.058	1.052
	.025	-1.057	-.621	-.262	.008	.291	.485	.605	.539	.382	.148	-.133	-.443
	.050	-1.227	-.942	-.674	-.445	-.191	.002	.136	.064	-.103	-.323	-.567	-.812
	.100	-1.090	-.902	-.712	-.550	-.360	-.214	-.108	-.168	-.299	-.461	-.641	-.809
	.200	-1.030	-.920	-.803	-.696	-.566	-.469	-.392	-.437	-.529	-.641	-.760	-.864
	.300	-.867	-.799	-.720	-.651	-.559	-.500	-.445	-.474	-.542	-.617	-.694	-.757
	.400	-.820	-.781	-.729	-.681	-.615	-.579	-.545	-.564	-.609	-.660	-.715	-.751
	.500	-.703	-.687	-.654	-.625	-.579	-.565	-.545	-.556	-.583	-.612	-.649	-.664
	.600	-.613	-.624	-.605	-.590	-.566	-.567	-.564	-.566	-.576	-.595	-.607	-.606
	.700	-.420	-.442	-.443	-.437	-.423	-.434	-.439	-.435	-.440	-.449	-.449	-.437
	.800	-.180	-.200	-.191	-.183	-.177	-.180	-.191	-.182	-.185	-.187	-.199	-.193
Lower surface	.900	-.033	.021	.050	.070	.100	.114	.123	.082	.103	.078	.052	.042
	.950	-.020	.039	.061	.073	.106	.122	.130	.088	.109	.081	.057	.059
	.0375	.483	.300	.105	-.108	-.394	-.685	-.925	-.786	-.548	-.258	-.006	.222
	.075	.310	.167	.029	-.121	-.307	-.500	-.653	-.564	-.408	-.227	-.054	.109
	.150	.170	.064	-.032	-.138	-.262	-.394	-.479	-.429	-.334	-.211	-.093	.024
	.250	.073	-.006	-.078	-.158	-.249	-.341	-.411	-.369	-.302	-.215	-.130	-.031
	.350	0	-.067	-.120	-.183	-.253	-.328	-.380	-.353	-.299	-.230	-.162	-.086
	.450	-.090	-.145	-.188	-.239	-.293	-.357	-.394	-.373	-.334	-.278	-.225	-.159
	.550	-.137	-.176	-.207	-.249	-.289	-.339	-.365	-.351	-.325	-.282	-.238	-.185
	.650	-.170	-.200	-.218	-.249	-.280	-.316	-.331	-.323	-.308	-.278	-.246	-.202
	.750	-.210	-.224	-.227	-.244	-.260	-.278	-.282	-.280	-.278	-.263	-.249	-.220
	.850	-.197	-.191	-.174	-.178	-.173	-.172	-.161	-.168	-.185	-.187	-.188	-.176
	.925	-.137	-.109	-.078	-.070	-.057	-.043	-.027	-.037	-.059	-.072	-.083	-.086
	.975	-.097	-.042	-.002	.010	.033	.051	.068	.060	.032	.009	-.004	-.016
	a_1	-.050	.011	.051	.053	.087	.108	.120	.083	.085	.062	.040	.050

No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $N = 1500$ r.p.m.

	J	1.962	2.048	2.132	2.238	2.322	2.412	2.501	2.599	2.543	2.467	2.361	2.283	2.185	2.114	2.139
M_x		.495	.514	.531	.555	.575	.595	.614	.639	.623	.605	.581	.564	.543	.529	.507
α_x		4.34	3.40	2.55	1.52	.78	.03	-.66	-1.38	-.98	-.40	.45	1.12	2.02	2.72	3.76
$\Delta\delta$.02	.02	.02	.01	.01	0	0	0	0	0	.01	.01	.01	.02	.02
α_1		1.09	.93	.75	.50	.34	.17	.02	-.14	-.05	.08	.26	.42	.62	.78	1.00
α_m		.4645	.3974	.3226	.2181	.1497	.0761	.0068	-.0613	-.0226	.0361	.1135	.1819	.2690	.3355	.4258
α_o		-.0044	-.0085	-.0102	-.0133	-.0142	-.0149	-.0151	-.0221	-.0203	-.0161	-.0151	-.0138	-.0123	-.0113	-.0077
c/b	Pressure coefficient, P															
Upper surface	$\alpha = 0.000$	1.064	1.068	1.072	1.079	1.085	1.091	1.097	1.107	1.100	1.094	1.087	1.082	1.075	1.072	1.066
	.025	-.502	-.282	-.097	.107	.257	.387	.498	.598	.545	.453	.321	.188	.012	-.146	-.377
	.050	-.889	-.715	-.555	-.372	-.239	-.113	.006	.117	.059	-.040	-.177	-.296	-.456	-.596	-.788
	.100	-.879	-.762	-.645	-.511	-.411	-.315	-.221	-.132	-.180	-.258	-.367	-.454	-.572	-.672	-.807
	.200	-.923	-.854	-.780	-.692	-.631	-.562	-.494	-.432	-.466	-.519	-.601	-.653	-.735	-.796	-.875
	.300	-.803	-.762	-.712	-.656	-.616	-.569	-.523	-.483	-.506	-.539	-.601	-.629	-.682	-.723	-.771
	.400	-.788	-.764	-.732	-.694	-.672	-.641	-.611	-.591	-.740	-.619	-.664	-.675	-.714	-.738	-.767
	.500	-.692	-.681	-.660	-.635	-.628	-.608	-.591	-.586	-.589	-.594	-.626	-.627	-.648	-.663	-.677
	.600	-.618	-.620	-.610	-.601	-.601	-.591	-.584	-.591	-.589	-.584	-.603	-.595	-.606	-.610	-.613
	.700	-.438	-.447	-.442	-.437	-.440	-.433	-.431	-.440	-.435	-.428	-.443	-.434	-.443	-.441	-.438
	.800	-.187	-.187	-.175	-.168	-.161	-.144	-.132	-.135	-.134	-.135	-.158	-.159	-.174	-.175	-.183
	.900	.017	.030	.048	.066	.077	.093	.107	.112	.107	.103	.081	.075	.054	.042	.027
	.950	.032	.046	.056	.073	.082	.099	.112	.115	.114	.108	.085	.082	.065	.053	.046
Lower surface	$\alpha = 0.000$.0375	.258	.123	-.009	-.201	-.355	-.507	-.682	-.905	-.790	-.605	-.443	-.274	-.113	.027
	.075	.135	.035	-.055	-.182	-.293	-.393	-.504	-.649	-.576	-.455	-.350	-.233	-.126	-.031	.082
	.150	.039	-.030	-.094	-.182	-.258	-.326	-.398	-.482	-.441	-.366	-.301	-.217	-.145	-.075	.006
	.250	-.025	-.079	-.127	-.191	-.248	-.297	-.347	-.415	-.381	-.323	-.282	-.217	-.166	-.113	-.051
	.350	-.061	-.125	-.162	-.215	-.260	-.297	-.336	-.391	-.365	-.319	-.287	-.233	-.193	-.153	-.100
	.450	-.158	-.197	-.225	-.270	-.308	-.335	-.368	-.407	-.389	-.351	-.329	-.284	-.253	-.217	-.176
	.550	-.190	-.218	-.243	-.276	-.308	-.330	-.352	-.384	-.370	-.342	-.327	-.288	-.265	-.235	-.202
	.650	-.212	-.234	-.249	-.276	-.301	-.315	-.331	-.354	-.346	-.323	-.318	-.284	-.267	-.242	-.218
	.750	-.236	-.245	-.254	-.270	-.285	-.290	-.293	-.303	-.302	-.290	-.295	-.272	-.267	-.250	-.235
	.850	-.199	-.194	-.193	-.197	-.198	-.194	-.185	-.182	-.186	-.187	-.204	-.195	-.198	-.191	-.192
	.925	-.116	-.102	-.090	-.084	-.080	-.069	-.056	-.044	-.030	-.058	-.082	-.079	-.090	-.091	-.103
	.975	-.052	-.023	-.007	.001	.009	.023	.040	.054	.046	.035	.011	.010	-.005	-.009	-.032
	$\alpha = 1.000$.040	.035	.049	.071	.070	.087	.098	.102	.115	.096	.059	.068	.035	.026	.001

No orifices.



TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = c.30$; $B_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1600$ rpm.

J	2.134	2.224	2.303	2.395	2.474	2.554	2.611	2.585	2.510	2.436	2.350	2.253	2.182
M_{x1}	.553	.574	.591	.613	.632	.651	.664	.658	.639	.621	.601	.578	.562
α_{x1}	2.53	1.67	.96	.18	-.45	-1.05	-1.45	-1.27	-.72	-.15	.35	1.40	2.06
$\Delta\beta$.01	.01	.01	.01	0	0	0	0	0	0	.01	.01	.01
α_{x1}	.86	.68	.50	.32	.17	.01	-.10	-.05	.09	.25	.44	.61	.78
c_n	.3710	.2948	.2206	.1416	.0742	.0058	-.0445	-.0206	.0381	.1097	.1935	.2639	.3374
c_m	-.0077	-.0084	-.0087	-.0102	-.0108	-.0129	-.0154	-.0144	-.0126	-.0113	-.0107	-.0100	-.0090
c_c													
a/b	Pressure coefficient, P												
Upper surface	$\beta_{0.000}$	1.078	1.084	1.090	1.097	1.103	1.110	1.115	1.113	1.106	1.100	1.093	1.086
	.025	-.203	-.005	.143	.285	.407	.513	.577	.546	.461	.347	.205	-.123
	.050	-.681	-.512	-.370	-.226	-.107	.006	.079	.048	-.048	-.162	-.300	-.454
	.100	-.753	-.627	-.524	-.416	-.319	-.229	-.170	-.197	-.274	-.362	-.469	-.585
	.200	-.871	-.788	-.727	-.652	-.588	-.525	-.482	-.499	-.557	-.616	-.686	-.766
	.300	-.778	-.720	-.684	-.636	-.595	-.557	-.531	-.539	-.576	-.611	-.655	-.710
	.400	-.782	-.744	-.727	-.696	-.672	-.655	-.644	-.644	-.665	-.678	-.706	-.741
	.500	-.696	-.670	-.665	-.646	-.635	-.633	-.633	-.628	-.635	-.635	-.650	-.671
	.600	-.628	-.613	-.621	-.611	-.610	-.617	-.627	-.617	-.614	-.604	-.606	-.622
	.700	-.442	-.437	-.442	-.435	-.433	-.441	-.448	-.440	-.436	-.429	-.432	-.445
	.800	-.173	-.157	-.153	-.129	-.113	-.104	-.098	-.097	-.105	-.117	-.135	-.162
Lower surface	.900	.027	.043	.052	.068	.084	.090	.094	.096	.089	.081	.063	.049
	.950	.042	.057	.059	.072	.085	.093	.097	.099	.093	.085	.070	.056
	.0375	.081	-.062	-.214	-.365	-.523	-.712	-.862	-.782	-.612	-.428	-.265	-.122
	.075	.007	-.087	-.201	-.303	-.408	-.536	-.630	-.579	-.468	-.344	-.234	-.132
	.150	-.053	-.118	-.199	-.270	-.341	-.423	-.479	-.450	-.382	-.293	-.220	-.153
	.250	-.096	-.145	-.207	-.257	-.307	-.368	-.413	-.388	-.335	-.274	-.220	-.170
	.350	-.144	-.180	-.233	-.271	-.312	-.363	-.401	-.382	-.337	-.281	-.238	-.201
	.450	-.214	-.244	-.290	-.321	-.354	-.396	-.423	-.407	-.375	-.328	-.293	-.262
	.550	-.236	-.262	-.298	-.321	-.347	-.381	-.402	-.389	-.363	-.326	-.300	-.276
	.650	-.251	-.266	-.299	-.314	-.336	-.360	-.377	-.367	-.349	-.317	-.298	-.280
	.750	-.265	-.272	-.294	-.300	-.309	-.321	-.327	-.323	-.315	-.296	-.287	-.280
	.850	-.214	-.207	-.216	-.213	-.209	-.210	-.206	-.207	-.211	-.202	-.207	-.211
	.925	-.117	-.103	-.103	-.090	-.080	-.075	-.067	-.068	-.077	-.079	-.089	-.101
	.975	-.041	-.019	-.013	.001	.013	.024	.032	.031	.018	.012	0	-.015
	$\beta_{1.000}$	0	.030	.033	.073	.065	.075	.085	.081	.071	.060	.047	.038

^aNo orifice.

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(e) $M = 0.56$.

J	2.111	2.138	2.180	2.218	2.259	2.314	2.358	2.393	2.442	2.485	2.540	2.622
M_x	.623	.620	.614	.617	.612	.615	.614	.610	.609	.604	.606	.604
α_x	2.74	2.49	2.08	1.77	1.35	.86	.49	.20	-.20	-.53	-.94	-1.53
$\Delta\theta$.04	.03	.02	.02	.02	.02	.02	.01	0	0	0	-.01
α_1	.70	.64	.57	.49	.43	.32	.22	.16	.08	.02	-.08	-.17
c_{D1}	.3032	.2774	.2452	.2116	.1858	.1381	.0974	.0684	.0348	.0065	-.0361	-.0774
c_{D0}	-.0070	-.0082	-.0084	-.0090	-.0111	-.0133	-.0147	-.0164	-.0175	-.0203	-.0249	-.0272
c/b	Pressure coefficient, P											
Upper surface	0.000	1.100	1.099	1.097	1.098	1.096	1.098	1.097	1.096	1.095	1.094	1.094
	.025	.033	.073	.124	.187	.235	.307	.367	.409	.457	.499	.560
	.050	-.510	-.469	-.414	-.350	-.300	-.224	-.160	-.111	-.055	-.009	.061
	.100	-.648	-.614	-.567	-.516	-.472	-.411	-.355	-.317	-.272	-.231	-.178
	.200	-.828	-.800	-.768	-.731	-.695	-.649	-.604	-.572	-.536	-.502	-.461
	.300	-.754	-.738	-.714	-.690	-.665	-.635	-.600	-.579	-.552	-.529	-.500
	.400	-.771	-.760	-.745	-.732	-.711	-.691	-.665	-.652	-.630	-.613	-.594
	.500	-.679	-.677	-.669	-.666	-.651	-.642	-.623	-.616	-.603	-.593	-.585
	.600	-.606	-.612	-.607	-.610	-.604	-.602	-.593	-.593	-.589	-.584	-.586
	.700	-.410	-.420	-.421	-.431	-.428	-.432	-.428	-.436	-.438	-.437	-.448
	.800	-.116	-.125	-.122	-.127	-.125	-.125	-.123	-.132	-.139	-.145	-.163
Lower surface	.900	.040	.042	.049	.051	.061	.069	.082	.088	.096	.103	.106
	.950	.049	.052	.061	.063	.070	.062	.088	.093	.101	.108	.113
	.0375	-.022	-.075	-.126	-.207	-.256	-.352	-.426	-.503	-.587	-.661	-.802
	.075	-.065	-.102	-.138	-.195	-.228	-.294	-.340	-.393	-.447	-.493	-.583
	.150	-.102	-.130	-.155	-.199	-.218	-.265	-.293	-.329	-.361	-.392	-.447
	.250	-.137	-.153	-.169	-.204	-.218	-.252	-.272	-.295	-.320	-.342	-.384
	.350	-.168	-.186	-.201	-.228	-.237	-.265	-.277	-.297	-.317	-.331	-.368
	.450	-.240	-.253	-.264	-.286	-.293	-.315	-.325	-.338	-.352	-.364	-.391
	.550	-.256	-.269	-.278	-.296	-.300	-.317	-.321	-.333	-.343	-.349	-.369
	.650	-.268	-.279	-.285	-.300	-.300	-.312	-.312	-.320	-.324	-.328	-.343
	.750	-.276	-.283	-.285	-.293	-.290	-.294	-.291	-.294	-.294	-.298	-.291
	.850	-.218	-.220	-.216	-.220	-.211	-.210	-.200	-.198	-.192	-.186	-.187
	.925	-.113	-.115	-.106	-.105	-.097	-.090	-.077	-.074	-.066	-.057	-.052
	.975	-.037	-.033	-.023	-.019	-.007	-.001	-.014	-.018	-.028	-.036	-.047
	1.000	.005	.012	.025	.027	.047	.035	.056	.067	.072	.081	.093

No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($\alpha = 0.30$; $\beta_x = 68.78^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued $(r) H = 0.58$.

		2.106	2.140	2.172	2.212	2.253	2.288	2.327	2.371	2.416	2.462	2.525	2.566	2.598
J		.646	.643	.639	.639	.638	.635	.633	.632	.630	.629	.631	.625	.621
M_x		2.81	2.47	2.16	1.78	1.40	1.09	.75	.38	.01	-.35	-.83	-1.13	-1.36
$\Delta\delta$.05	.05	.04	.04	.03	.03	.03	.02	.02	.01	.01	0	0
α_1		.70	.63	.56	.47	.39	.35	.28	.21	.13	.04	-.05	-.10	-.16
α_2		.3006	.2716	.2413	.2058	.1716	.1510	.1242	.0939	.0594	.0168	-.0206	-.0439	-.0710
α_3		.0003	-.0044	-.0041	-.0066	-.0088	-.0085	-.0088	-.0097	-.0098	-.0142	-.0162	-.0177	-.0213
c/b														
		Pressure coefficient, P												
Upper surface	$a_0.000$	1.108	1.107	1.106	1.106	1.105	1.104	1.104	1.103	1.102	1.102	1.103	1.101	1.100
	.025	.047	.108	.169	.218	.267	.310	.358	.395	.457	.499	.559	.588	.618
	.050	-.509	-.444	-.377	-.325	-.270	-.225	-.173	-.130	-.064	-.016	.056	.092	.128
	.100	-.662	-.604	-.549	-.502	-.455	-.418	-.375	-.339	-.280	-.241	-.180	-.152	-.125
	.200	-.864	-.814	-.770	-.733	-.694	-.665	-.632	-.602	-.554	-.519	-.467	-.439	-.421
	.300	-.782	-.750	-.720	-.697	-.666	-.652	-.626	-.605	-.569	-.546	-.504	-.487	-.473
	.400	-.800	-.776	-.756	-.741	-.717	-.709	-.692	-.677	-.650	-.632	-.598	-.586	-.579
	.500	-.701	-.686	-.677	-.669	-.652	-.654	-.643	-.635	-.618	-.608	-.585	-.577	-.578
	.600	-.619	-.614	-.613	-.611	-.601	-.608	-.606	-.603	-.596	-.593	-.578	-.577	-.586
	.700	-.414	-.416	-.420	-.421	-.417	-.428	-.432	-.433	-.432	-.436	-.430	-.434	-.447
	.800	-.117	-.114	-.113	-.114	-.106	-.115	-.118	-.118	-.117	-.124	-.131	-.148	-.169
Lower surface	.900	.031	.043	.048	.054	.061	.062	.071	.077	.089	.094	.112	.114	.110
	.950	.039	.051	.060	.064	.073	.070	.078	.082	.092	.099	.117	.120	.116
	.0375	-.029	-.080	-.154	-.213	-.268	-.345	-.413	-.480	-.575	-.661	-.765	-.843	-.943
	.075	-.077	-.116	-.164	-.203	-.238	-.293	-.338	-.381	-.441	-.497	-.561	-.608	-.670
	.150	-.116	-.141	-.176	-.201	-.225	-.265	-.294	-.324	-.363	-.397	-.430	-.460	-.500
	.250	-.142	-.160	-.186	-.205	-.222	-.252	-.274	-.295	-.321	-.346	-.372	-.395	-.425
	.350	-.184	-.198	-.219	-.231	-.243	-.267	-.284	-.300	-.321	-.341	-.355	-.373	-.399
	.450	-.254	-.265	-.281	-.291	-.298	-.318	-.333	-.346	-.360	-.375	-.382	-.395	-.415
	.550	-.274	-.278	-.291	-.299	-.303	-.322	-.331	-.342	-.351	-.361	-.366	-.375	-.390
	.650	-.290	-.291	-.300	-.304	-.305	-.318	-.326	-.332	-.336	-.343	-.342	-.347	-.360
	.750	-.297	-.293	-.296	-.297	-.293	-.305	-.306	-.309	-.306	-.307	-.298	-.300	-.306
	.850	-.235	-.227	-.225	-.221	-.214	-.218	-.215	-.213	-.204	-.200	-.185	-.182	-.186
	.925	-.192	-.116	-.110	-.104	-.094	-.097	-.090	-.087	-.075	-.068	-.050	-.046	-.046
	.975	-.049	-.034	-.024	-.017	-.005	-.007	.003	.008	.018	.030	.048	.052	.054
	a1.000	.072	.028	.036	.056	.058	.051	.079	.070	.080	.094	.100	.110	.105

No orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $P_x = 68.76^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(g) $M = 0.50$.

J	2.108	2.142	2.180	2.224	2.262	2.296	2.344	2.380	2.426	2.473	2.520	2.578
M_x	.665	.660	.658	.660	.659	.654	.655	.651	.649	.647	.646	.644
α_T	2.79	2.45	2.08	1.67	1.32	1.02	.60	.30	-.07	-.44	-.79	-1.22
$\Delta\delta$.06	.06	.04	.03	.02	.01	0	0	0	0	0	0
α_1	.69	.61	.53	.45	.38	.31	.22	.16	.08	.01	-.07	-.14
c_n	.2968	.2645	.2310	.1935	.1639	.1348	.0977	.0703	.0352	.0035	-.0290	-.0639
c_m	-.0043	-.0066	-.0059	-.0082	-.0079	-.0113	-.0121	-.0118	-.0135	-.0132	-.0167	-.0213
c_o												
c/b	Pressure coefficient, P											
Upper surface	$\theta_0.000$	1.116	1.114	1.113	1.114	1.113	1.111	1.111	1.110	1.109	1.108	1.107
	.025	.035	.108	.156	.220	.278	.314	.366	.406	.449	.498	.536
	.050	-.501	-.428	-.372	-.301	-.237	-.197	-.140	-.096	-.047	.007	.053
	.100	-.668	-.601	-.550	-.489	-.435	-.400	-.352	-.315	-.271	-.227	-.187
	.200	-.905	-.840	-.790	-.739	-.694	-.662	-.625	-.591	-.556	-.521	-.485
	.300	-.822	-.776	-.738	-.704	-.673	-.651	-.630	-.606	-.579	-.554	-.531
	.400	-.847	-.810	-.779	-.756	-.732	-.718	-.705	-.683	-.666	-.651	-.631
	.500	-.734	-.714	-.694	-.682	-.668	-.662	-.659	-.646	-.635	-.628	-.617
	.600	-.643	-.634	-.626	-.621	-.617	-.617	-.624	-.617	-.613	-.614	-.612
	.700	-.427	-.424	-.422	-.422	-.423	-.427	-.435	-.435	-.437	-.442	-.447
	.800	-.135	-.127	-.116	-.106	-.102	-.105	-.106	-.102	-.104	-.109	-.114
Lower surface	.900	.014	.029	.039	.049	.056	.066	.069	.078	.085	.090	.095
	.950	.025	.042	.051	.059	.064	.071	.072	.083	.090	.095	.100
	.0375	-.050	-.112	-.163	-.234	-.310	-.367	-.461	-.527	-.601	-.709	-.802
	.075	-.097	-.138	-.171	-.221	-.274	-.308	-.371	-.411	-.460	-.531	-.588
	.150	-.135	-.161	-.184	-.216	-.251	-.274	-.320	-.347	-.376	-.421	-.455
	.250	-.163	-.180	-.195	-.216	-.243	-.260	-.293	-.310	-.334	-.366	-.395
	.350	-.202	-.215	-.226	-.243	-.262	-.274	-.301	-.316	-.331	-.358	-.380
	.450	-.278	-.284	-.291	-.303	-.320	-.327	-.351	-.360	-.369	-.390	-.408
	.550	-.297	-.298	-.302	-.311	-.321	-.327	-.346	-.353	-.361	-.378	-.387
	.650	-.314	-.313	-.310	-.314	-.321	-.325	-.339	-.342	-.347	-.358	-.364
	.750	-.319	-.313	-.308	-.306	-.307	-.306	-.315	-.313	-.311	-.318	-.317
	.850	-.253	-.242	-.233	-.226	-.221	-.217	-.218	-.215	-.207	-.206	-.202
	.925	-.141	-.125	-.114	-.102	-.096	-.089	-.089	-.081	-.076	-.072	-.066
	.975	-.060	-.038	-.024	-.011	-.004	.002	.004	.012	.019	.025	.032
	$\alpha_1.000$	-.002	.006	.030	.034	.040	.055	.050	.062	.072	.080	.091

^aNo orifice.

NACA

TABLE 2.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-516.25 PROPELLER BLADE SECTION ($x = 0.30$; $\beta_x = 68.78^\circ$; $\beta = 45^\circ$; $B = 2$) - Computed
0.75R(h) $M = 0.65$.

J	2.077	2.101	2.130	2.151	2.184	2.208	2.239	2.261	2.293	2.319	2.350	2.383	2.412	2.451
M_x	.730	.727	.725	.722	.720	.719	.717	.715	.713	.710	.709	.707	.705	.703
$\Delta\delta_x$	3.11	2.86	2.57	2.36	2.04	1.81	1.53	1.33	1.04	.82	.55	.28	.04	-.27
α_1	.06	.06	.05	.05	.04	.04	.03	.02	0	0	0	-.01	-.01	-.01
α_2	.63	.61	.54	.50	.44	.38	.33	.27	.22	.18	.12	.04	.01	-.09
c_{D1}	.2684	.2613	.2342	.2142	.1903	.1665	.1419	.1187	.0968	.0774	.0510	.0181	.0039	-.0381
c_{D2}	-.0029	-.0007	-.0003	-.0015	-.0002	0	-.0033	-.0046	-.0048	-.0062	-.0046	-.0085	-.0066	-.0121
c_c	.0041	.0041	.0042	.0041	.0052	.0057	.0063	.0072	.0085	.0079	.0080	.0098	.0100	.0137
o/b	Pressure coefficient, P													
Upper surface	$a_0.000$	1.141	1.140	1.139	1.138	1.137	1.137	1.136	1.135	1.134	1.133	1.133	1.132	1.131
	$a_0.025$.196	.216	.250	.279	.313	.339	.367	.391	.427	.4390	.4265	.4460	.4365
	$a_0.050$	-.385	-.361	-.320	-.290	-.251	-.225	-.188	-.159	-.116	-.092	-.049	-.014	.012
	$a_0.100$	-.594	-.571	-.535	-.508	-.472	-.447	-.414	-.388	-.349	-.328	-.288	-.256	-.234
	$a_0.200$	-.919	-.909	-.884	-.855	-.818	-.790	-.750	-.717	-.678	-.654	-.616	-.585	-.563
	$a_0.300$	-.834	-.825	-.810	-.794	-.774	-.760	-.733	-.709	-.681	-.667	-.638	-.613	-.598
	$a_0.400$	-1.065	-1.034	-1.006	-.964	-.930	-.898	-.858	-.828	-.799	-.785	-.758	-.734	-.718
	$a_0.500$	-.841	-.808	-.798	-.781	-.772	-.766	-.747	-.731	-.720	-.713	-.700	-.688	-.680
	$a_0.600$	-.641	-.645	-.652	-.650	-.651	-.656	-.650	-.649	-.647	-.644	-.644	-.639	-.640
	$a_0.700$	-.363	-.376	-.385	-.385	-.388	-.395	-.400	-.406	-.411	-.414	-.416	-.416	-.424
	$a_0.800$	-.091	-.092	-.089	-.078	-.066	-.063	-.060	-.059	-.058	-.053	-.047	-.042	-.046
Lower surface	$a_0.900$	-.015	-.003	.007	.020	.028	.036	.043	.048	.055	.051	.060	.072	.074
	$a_0.950$	-.009	.002	.014	.026	.032	.040	.050	.053	.062	.057	.066	.078	.080
	$a_1.000$	-.0375	-.076	-.107	-.160	-.194	-.247	-.285	-.328	-.378	-.440	-.494	-.564	-.616
	$a_1.075$	-.121	-.143	-.178	-.204	-.241	-.270	-.297	-.333	-.374	-.410	-.456	-.488	-.525
	$a_1.150$	-.158	-.172	-.196	-.213	-.240	-.260	-.277	-.301	-.328	-.352	-.382	-.398	-.421
	$a_1.250$	-.186	-.193	-.217	-.223	-.242	-.257	-.269	-.287	-.304	-.324	-.344	-.357	-.375
	$a_1.350$	-.234	-.240	-.252	-.262	-.279	-.291	-.297	-.311	-.325	-.339	-.354	-.362	-.375
	$a_1.450$	-.317	-.322	-.330	-.336	-.349	-.357	-.360	-.371	-.381	-.392	-.402	-.404	-.414
	$a_1.550$	-.341	-.340	-.346	-.350	-.359	-.364	-.365	-.372	-.378	-.388	-.395	-.394	-.401
	$a_1.650$	-.369	-.366	-.369	-.369	-.374	-.377	-.373	-.375	-.378	-.385	-.387	-.385	-.389
	$a_1.750$	-.379	-.370	-.367	-.363	-.366	-.364	-.356	-.354	-.354	-.357	-.352	-.345	-.344
	$a_1.850$	-.307	-.296	-.285	-.279	-.277	-.273	-.259	-.255	-.248	-.249	-.241	-.232	-.229
	$a_1.925$	-.190	-.172	-.160	-.150	-.146	-.137	-.122	-.117	-.109	-.108	-.099	-.089	-.087
	$a_1.975$	-.109	-.086	-.071	-.061	-.052	-.042	-.026	-.020	-.011	-.010	-.003	.009	.010
	$a_1.000$	-.009	-.001	.013	.010	.027	.026	.044	.044	.048	.048	.058	.055	.067

^aNo orifice.^bPaired value.

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75x} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

J	1.589	1.778	1.965	2.152	2.285	2.400	2.522	2.659	2.794	2.469	2.338	2.190	2.049	1.872	1.679	1.541
M_∞	.369	.395	.422	.450	.468	.487	.506	.527	.546	.498	.477	.454	.434	.411	.381	.364
$\frac{C_L}{C_D}$	10.91	7.74	4.98	2.55	.99	-.25	-1.48	-2.75	-4.24	-.95	.41	2.09	3.85	6.31	9.35	11.79
ΔC_L	.17	.13	.10	.06	.04	.01	-.01	-.03	-.02	0	.03	.05	.08	.11	.15	.17
C_L	2.62	2.12	1.64	1.19	.88	.62	.35	.09	.23	.47	.78	1.07	1.43	1.87	2.37	2.78
C_D	1.0555	.8684	.6774	.5000	.3703	.2645	.1497	.0394	.0987	.2000	.3290	.4510	.5942	.7703	.9626	1.1174
C_D	-.0311	-.0462	-.0600	-.0728	-.0767	-.0803	-.0756	-.0608	-.0813	-.0805	-.0791	-.0757	-.0669	-.0537	-.0421	-.0223
ϕ/h	Pressure coefficient, P															
Upper surface	.0000	1.035	1.040	1.046	1.052	1.056	1.061	1.065	1.071	1.068	1.063	1.058	1.053	1.048	1.043	1.037
	.025	-.285	-.1912	-.1161	-.0523	-.158	.103	.339	.524	.443	.236	-.033	-.399	-.851	-.1564	-.2351
	.050	-.2176	-.1561	-.1049	-.0517	-.354	.147	.039	.205	.131	-.045	-.264	-.532	-.845	-.1321	-.1951
	.100	-.1592	-.1207	-.0872	-.0593	-.411	.264	.124	.006	-.051	.188	-.354	-.537	-.745	-.1036	-.1401
	.200	-.1200	-.0986	-.0777	-.0602	-.475	.373	.282	-.186	-.229	.326	-.444	-.566	-.701	-.887	-.1103
	.300	-.1008	-.0872	-.0731	-.0605	-.517	.441	.373	-.300	-.331	.405	-.497	-.584	-.679	-.811	-.955
	.400	-.0866	-.0751	-.0638	-.0602	-.536	.477	.430	-.371	-.398	.452	-.526	-.599	-.658	-.748	-.845
	.500	-.0741	-.0709	-.0632	-.0591	-.541	.502	.471	-.429	-.449	.489	-.542	-.581	-.633	-.689	-.747
	.600	-.0612	-.0625	-.0603	-.0573	-.541	.515	.497	-.467	-.484	.506	-.547	-.569	-.598	-.627	-.642
	.700	-.0441	-.0488	-.0501	-.0508	-.490	.472	.440	-.445	-.456	.472	-.505	-.514	-.511	-.505	-.485
	.800	-.0211	-.0260	-.0314	-.0353	-.357	.360	.323	-.338	-.350	.358	-.383	-.396	-.396	-.297	-.246
Lower surface	.900	-.0086	-.024	-.019	-.003	-.085	-.087	-.088	-.083	-.088	-.087	-.104	-.091	-.053	-.016	-.059
	.950	-.078	.010	.066	.099	.097	.098	.104	.107	.106	.101	.078	.093	.097	.036	-.039
	.0375	.836	.651	.411	.129	-.085	-.279	-.516	-.757	-.643	-.407	-.197	.052	.284	.532	.747
	.075	.682	.515	.325	.111	-.041	-.175	-.332	-.489	-.414	-.257	-.123	.058	.224	.414	.595
	.150	.498	.367	.220	.070	-.039	-.127	-.248	-.344	-.296	-.193	-.099	.026	.150	.289	.426
	.250	.369	.264	.155	.032	-.049	-.125	-.205	-.275	-.241	-.171	-.099	.001	.097	.203	.309
	.350	.285	.198	.112	.017	-.041	-.092	-.155	-.208	-.181	-.126	-.081	-.008	.065	.130	.235
	.450	.219	.183	.073	-.001	-.044	-.084	-.136	-.177	-.153	-.111	-.081	-.022	.037	.105	.172
	.550	.144	.094	.039	-.018	-.058	-.084	-.126	-.154	-.139	-.107	-.083	-.040	.009	.095	.113
	.650	.085	.050	.014	-.027	-.055	-.074	-.104	-.125	-.114	-.092	-.081	-.045	.009	.089	.063
	.750	.027	.013	-.009	-.030	-.044	-.051	-.073	-.085	-.077	-.065	-.062	-.043	-.022	.006	.012
	.850	.006	.013	.014	.014	.010	.015	.003	-.003	.006	.012	.002	.006	.012	.022	0
	.925	-.011	.021	.050	.070	.084	.088	.088	.078	.085	.086	.071	.073	.050	.033	0
	.975	-.057	.010	.063	.123	.135	.144	.137	.138	.141	.143	.131	.127	.084	.036	-.027
	1.000	-.082	0	.071	.153	.160	.172	.160	.169	.176	.172	.165	.153	.105	.033	-.048

*No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45^\circ$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	2.647	2.473	2.329	2.207	2.087	1.978	1.872	1.768	1.619	1.526	2.027	2.143	2.269	2.408	2.550
M_x	.626	.590	.565	.543	.522	.504	.487	.468	.477	.495	.513	.532	.557	.582	.609
$\Delta \delta$	-.64	-.99	.51	1.89	3.29	4.80	6.31	7.90	7.10	5.53	4.14	2.66	1.17	-.33	-1.75
$\Delta \delta$	-.08	-.02	.03	.08	.11	.16	.20	.23	.21	.18	.14	.09	.05	0	-.04
α	.10	.43	.75	1.05	1.39	1.65	1.94	2.25	2.10	1.80	1.55	1.23	.92	.59	.26
α	.0426	.1852	.3187	.4445	.5800	.6858	.7981	.9200	.8606	.7426	.6439	.5148	.3890	.2503	.1097
α	-.0751	-.0726	-.0711	-.0706	-.0657	-.0560	-.0475	-.0408	-.0444	-.0524	-.0582	-.0688	-.0688	-.0705	-.0719
α															
α/b	Pressure coefficient, P														
Upper surface	0.000	1.101	1.090	1.082	1.077	1.070	1.065	1.061	1.056	1.059	1.063	1.067	1.072	1.080	1.087
	.025	.549	.289	-.021	-.354	-.769	-1.188	-1.669	-2.065	-1.922	-1.425	-1.007	-.554	-.190	.145
	.050	.228	-.008	-.262	-.518	-.808	-1.096	-1.434	-1.734	-1.570	-1.256	-.970	-.662	-.393	-.127
	.100	.015	-.172	-.362	-.544	-.737	-.922	-1.105	-1.319	-1.216	-.999	-.843	-.642	-.452	-.260
	.200	-.195	-.329	-.466	-.593	-.714	-.828	-.948	-1.062	-1.007	-.882	-.776	-.655	-.526	-.393
	.300	-.322	-.424	-.524	-.616	-.701	-.787	-.863	-.933	-.901	-.820	-.743	-.659	-.565	-.467
	.400	-.412	-.483	-.558	-.627	-.683	-.743	-.794	-.832	-.816	-.761	-.712	-.655	-.586	-.513
	.500	-.474	-.521	-.574	-.623	-.657	-.697	-.722	-.739	-.732	-.704	-.675	-.642	-.590	-.540
	.600	-.519	-.539	-.574	-.605	-.623	-.644	-.647	-.641	-.647	-.635	-.628	-.616	-.579	-.547
	.700	-.486	-.491	-.508	-.525	-.526	-.526	-.511	-.480	-.495	-.508	-.518	-.526	-.504	-.488
Lower surface	.800	-.351	-.342	-.346	-.350	-.339	-.313	-.277	-.228	-.253	-.283	-.317	-.344	-.333	-.334
	.900	-.041	-.027	-.029	-.033	-.025	-.008	-.007	-.029	-.015	.002	-.004	-.030	-.016	-.022
	.950	.120	.118	.103	.090	.093	.052	.024	-.010	.009	.044	.076	.095	.101	.115
	.0375	-.789	-.470	-.196	.020	.238	.391	.544	.687	.620	.478	.338	.136	-.063	-.319
	.075	-.544	-.300	-.121	.033	.195	.309	.428	.548	.493	.378	.272	.121	-.022	-.205
	.150	-.392	-.229	-.101	.007	.127	.207	.299	.395	.348	.262	.181	.068	-.030	-.157
	.250	-.315	-.196	-.111	.035	.059	.120	.197	.283	.242	.165	.104	.016	-.059	-.146
	.350	-.243	-.149	-.081	.023	.050	.096	.153	.220	.186	.133	.085	.016	-.038	-.106
	.450	-.209	-.133	-.079	.033	.027	.062	.112	.165	.136	.091	.052	-.002	-.044	-.098
	.550	-.187	-.129	-.087	.052	.003	.023	.060	.108	.086	.049	.020	-.024	-.059	-.102
	.650	-.156	-.112	-.085	.059	-.019	-.003	.024	.061	.043	.017	-.004	-.037	-.059	-.093
	.750	-.111	-.084	-.069	.052	-.025	-.020	-.002	.023	.009	-.005	-.015	-.037	-.048	-.072
	.850	-.022	-.010	-.011	.008	.009	-.001	.006	.015	.009	.007	.008	.005	.001	-.007
	.925	.096	.057	.049	.043	.047	.018	.009	.004	.009	.019	.036	.051	.052	.056
	.975	.108	.100	.083	.073	.072	-.014	-.012	-.034	-.023	.004	.041	.077	.083	.096
	1.000	.165	.170	.131	.117	.132	.044	-.036	-.064	-.050	-.014	.063	.100	.123	.160

No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1500$ rpm.

	J	M_x	α_x	$\Delta\beta$	c_L	c_D	c_m	c_o										
	2.584	2.511	2.431	2.345	2.284	2.201	2.139	2.068	1.983	2.021	2.084	2.158	2.227	2.318	2.395	2.480	2.547	
	.690	.674	.654	.635	.621	.604	.592	.577	.560	.569	.582	.595	.612	.629	.646	.664	.678	
	-2.07	-1.37	-.57	.33	1.01	1.96	2.71	3.61	4.74	4.22	3.40	2.48	1.65	.63	-.20	-1.07	-.72	
	-.07	-.03	.03	.10	.15	.20	.22	.23	.23	.23	.23	.21	.19	.12	.06	0	-.05	
	.11	.30	.49	.70	.86	1.14	1.30	1.51	1.70	1.61	1.45	1.23	1.06	.80	.58	.38	.23	
	.0477	.1271	.2103	.2948	.3800	.4806	.5458	.6303	.7071	.6703	.6065	.5174	.4458	.3368	.2484	.1616	.0974	
	-.0775	-.0728	-.0734	-.0728	-.0698	-.0710	-.0693	-.0665	-.0577	-.0616	-.0695	-.0708	-.0714	-.0719	-.0713	-.0735	-.0755	
	c/p	Pressure coefficient, P																
Upper surface	$\alpha 0.000$	1.125	1.119	1.111	1.104	1.100	1.094	1.090	1.085	1.080	1.083	1.087	1.091	1.096	1.102	1.109	1.115	
	.025	.523	.420	.263	.090	-.110	-.367	-.568	-.843	-1.197	-1.033	-.778	-.488	-.262	-.002	.190	.349	
	.050	.202	.102	-.039	-.190	-.344	-.542	-.691	-.889	-1.137	-1.019	-.845	-.636	-.466	-.262	-.101	.154	
	.100	-.008	-.091	-.204	-.319	-.431	-.572	-.676	-.810	-.962	-.893	-.780	-.639	-.521	-.370	-.252	-.143	
	.200	-.227	-.292	-.372	-.460	-.529	-.628	-.697	-.783	-.871	-.831	-.766	-.676	-.596	-.491	-.407	-.330	
	.300	-.361	-.411	-.473	-.537	-.581	-.655	-.702	-.762	-.824	-.796	-.749	-.687	-.633	-.573	-.497	-.385	
	.400	-.460	-.496	-.538	-.584	-.610	-.664	-.697	-.739	-.780	-.760	-.734	-.691	-.653	-.594	-.556	-.515	
	.500	-.522	-.545	-.570	-.603	-.612	-.650	-.673	-.700	-.723	-.712	-.697	-.671	-.646	-.603	-.562	-.532	
	.600	-.567	-.578	-.584	-.604	-.600	-.626	-.637	-.653	-.660	-.657	-.653	-.639	-.626	-.599	-.591	-.570	
	.700	-.513	-.514	-.512	-.522	-.509	-.525	-.531	-.539	-.529	-.534	-.539	-.536	-.532	-.514	-.514	-.514	
	.800	-.337	-.337	-.331	-.336	-.317	-.325	-.324	-.327	-.296	-.308	-.328	-.332	-.333	-.323	-.329	-.331	-.338
	.900	.010	.008	.006	-.004	.011	.004	-.002	-.007	.006	.004	-.007	-.006	-.003	.012	.017	.011	.011
	.950	.126	.122	.116	.102	.105	.091	.083	.084	.055	.072	.083	.082	.088	.105	.110	.115	.125
Lower surface	.0375	-.969	-.573	-.448	-.287	-.106	.051	.154	.271	.396	.341	.246	.110	-.017	-.192	-.368	-.532	
	.075	-.497	-.419	-.287	-.183	-.047	.062	.137	.223	.315	.274	.204	.102	.013	-.111	-.237	-.345	
	.150	-.382	-.312	-.220	-.146	-.047	.030	.085	.145	.213	.183	.131	.058	.006	-.092	-.183	-.265	
	.250	-.315	-.261	-.194	-.146	-.073	.015	.026	.070	.124	.099	.060	.009	-.042	-.106	-.168	-.226	
	.350	-.246	-.204	-.149	-.109	-.046	-.003	.029	.066	.104	.086	.057	.012	-.028	-.077	-.126	-.174	
	.450	-.215	-.182	-.140	-.108	-.053	.017	.009	.035	.067	.054	.030	-.008	-.037	-.077	-.118	-.157	
	.550	-.197	-.171	-.138	-.114	-.066	.039	.017	.004	.029	.016	.001	-.032	-.054	-.085	-.121	-.152	
	.650	-.170	-.151	-.127	-.111	-.070	.048	.032	.017	.004	-.010	-.020	-.043	-.061	-.085	-.113	-.135	
	.750	-.125	-.116	-.101	-.093	-.061	-.046	-.034	-.027	-.020	-.023	-.026	-.043	-.056	-.070	-.091	-.105	
	.850	-.032	-.032	-.026	-.027	-.008	.001	.005	.006	-.004	0	.007	-.001	-.005	-.011	-.021	-.025	
	.925	.050	.040	.043	.037	.049	.048	.048	.036	.021	.028	.045	.043	.045	.045	.043	.046	.054
	.975	.099	.090	.083	.077	.079	.071	.065	.052	.015	.030	.060	.067	.070	.078	.077	.082	.096
	$\alpha 1.000$.120	.115	.101	.098	.092	.088	.074	.067	0	.033	.071	.078	.084	.090	.104	.115	.114

^aNo aiffice.

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45^\circ$; $\beta_2 = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

$\frac{y}{R}$	2.136 .634	2.227 .656	2.330 .677	2.424 .701	2.514 .719	2.469 .708	2.381 .687	2.295 .667	2.188 .641	2.108 .626	
$\frac{dy}{dx}$	2.75 .16	1.66 .11	.50 .04	-.50 -.04	-1.40 -.09	-.96 -.06	-.05 -.01	.88 .06	2.12 .13	3.09 .17	
$\Delta \delta$	1.36 .5716	1.11 .4671	.81 .3432	.56 .2368	.24 .1013	.40 .1703	.67 .2852	.89 .3781	1.20 .5032	1.45 .6052	
α_1	-.0744	-.0777	-.0805	-.0832	-.0855	-.0849	-.0826	-.0798	-.0760	-.0731	
α_2				.0162	.0209	.0204					
α_m											
α_0											
$\frac{a}{b}$	Pressure coefficient, P										
Upper surface	0.000	1.104	1.112	1.120	1.129	1.137	1.132	1.124	1.116	1.107	1.102
	.025	-.537	-.213	-.081	-.300	.478	.395	.210	-.014	-.342	-.648
	.050	-.701	-.452	-.205	-.016	.153	.075	-.093	-.284	-.545	-.778
	.100	-.710	-.527	-.341	-.189	-.048	-.117	-.253	-.401	-.594	-.758
	.200	-.743	-.623	-.492	-.379	-.269	-.321	-.425	-.531	-.660	-.768
	.300	-.763	-.681	-.585	-.503	-.414	-.455	-.536	-.609	-.698	-.773
	.400	-.760	-.707	-.641	-.586	-.523	-.553	-.608	-.651	-.710	-.760
	.500	-.730	-.697	-.658	-.630	-.592	-.608	-.641	-.659	-.691	-.724
	.600	-.673	-.676	-.658	-.656	-.644	-.648	-.653	-.648	-.660	-.676
	.700	-.560	-.564	-.582	-.570	-.569	-.572	-.569	-.548	-.547	-.551
	.800	-.331	-.333	-.335	-.344	-.345	-.349	-.344	-.326	-.323	-.323
	.900	-.001	-.012	-.022	-.034	-.036	-.036	-.033	-.022	-.011	-.001
	.950	-.065	-.076	-.084	-.092	-.102	-.101	-.093	-.087	-.080	-.070
Lower surface	.0375	.145	-.030	-.245	-.468	-1.069	-.588	-.367	-.164	.057	.201
	.075	.132	0	-.192	-.308	-.438	-.377	-.237	-.096	.065	.174
	.150	.078	-.014	-.111	-.225	-.351	-.288	-.174	-.078	.034	.109
	.250	.024	-.043	-.122	-.203	-.295	-.245	-.171	-.089	-.004	.051
	.350	.023	-.032	-.093	-.152	-.230	-.190	-.126	-.071	-.001	.044
	.450	.004	-.041	-.090	-.137	-.202	-.169	-.115	-.074	-.016	.020
	.550	-.022	-.059	-.099	-.133	-.188	-.160	-.117	-.085	-.039	-.008
	.650	-.036	-.065	-.093	-.115	-.177	-.138	-.105	-.085	-.049	-.025
	.750	-.039	-.056	-.074	-.085	-.115	-.098	-.079	-.071	-.045	-.032
	.850	.001	-.003	-.007	-.007	-.024	-.013	-.006	-.008	.004	.006
	.925	.046	.056	.051	.057	.052	.058	.057	.050	.053	.047
	.975	.061	.066	.072	.077	.081	.082	.078	.070	.070	.061
	1.000	.071	.071	.084	.086	.093	.098	.083	.075	.069	.065

^aNo orifice.

NACA

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $M = 0.56$.

	J	2.655	2.600	2.559	2.512	2.466	2.429	2.384	2.347	2.318	2.280	2.252	2.214	2.178	2.140	2.117
	M_x	.646	.646	.649	.652	.655	.657	.661	.659	.665	.668	.673	.675	.676	.676	.678
	a_{x1}	-2.71	-2.22	-1.83	-1.38	-.92	-.55	-.08	.31	.63	1.05	1.37	1.81	2.24	2.70	2.98
	$\Delta\beta$	-.08	-.05	-.03	0	.03	.05	.08	.10	.11	.13	.14	.15	.16	.17	.18
	a_1	.04	.13	.19	.29	.42	.57	.74	.87	.97	1.08	1.15	1.25	1.28	1.34	1.34
	a_n	.0168	.0542	.0826	.1239	.1806	.2000	.2406	.2832	.3148	.3690	.4084	.4548	.4826	.5355	.5613
	a_m	-.0782	-.0778	-.0773	-.0770	-.0747	-.0760	-.0754	-.0749	-.0754	-.0746	-.0760	-.0721	-.0708	-.0710	-.0698
	a_0															
	a/b	Pressure coefficient, P														
Upper surface	0.000	1.108	1.109	1.110	1.111	1.112	1.113	1.114	1.113	1.116	1.116	1.119	1.120	1.120	1.120	1.120
	.025	.573	.519	.480	.413	.327	.282	.205	.129	.127	.033	-.111	-.189	-.263	-.383	-.423
	.050	.250	.198	.158	.097	.022	-.021	-.090	-.156	-.214	-.298	-.365	-.428	-.492	-.552	-.626
	.100	.040	-.009	-.041	-.093	-.154	-.190	-.244	-.294	-.341	-.405	-.460	-.511	-.562	-.639	-.665
	.200	-.176	-.215	-.244	-.287	-.332	-.362	-.401	-.445	-.485	-.534	-.579	-.621	-.661	-.721	-.744
	.300	-.305	-.341	-.365	-.400	-.436	-.462	-.501	-.532	-.564	-.603	-.645	-.679	-.715	-.762	-.782
	.400	-.399	-.429	-.451	-.480	-.506	-.531	-.564	-.588	-.614	-.646	-.682	-.710	-.739	-.778	-.795
	.500	-.464	-.488	-.505	-.527	-.546	-.564	-.590	-.607	-.627	-.648	-.674	-.695	-.723	-.757	-.785
	.600	-.510	-.528	-.544	-.558	-.567	-.583	-.599	-.609	-.622	-.634	-.653	-.665	-.675	-.686	-.689
	.700	-.477	-.489	-.497	-.503	-.503	-.512	-.522	-.522	-.527	-.528	-.536	-.538	-.541	-.537	-.533
Lower surface	.800	-.343	-.344	-.343	-.340	-.348	-.328	-.328	-.323	-.319	-.309	-.308	-.302	-.293	-.280	-.268
	.900	-.023	-.016	-.007	-.003	.011	.014	.016	.019	.020	.023	.018	.021	.024	.024	.030
	.950	.131	.128	.125	.123	.120	.116	.108	.103	.100	.096	.087	.084	.079	.075	.078
	.0375	-.855	-.705	-.697	-.598	-.497	-.456	-.377	-.298	-.239	-.151	-.094	-.035	.014	.096	.121
	.075	-.542	-.499	-.464	-.405	-.316	-.289	-.244	-.187	-.145	-.079	-.039	.005	.043	.100	.119
	.150	-.390	-.362	-.338	-.300	-.242	-.222	-.187	-.147	-.119	-.073	-.045	.014	.012	.056	.071
	.250	-.314	-.293	-.276	-.250	-.207	-.193	-.168	-.142	-.125	-.092	-.073	-.048	-.029	.006	.016
	.350	-.240	-.227	-.213	-.192	-.157	-.148	-.128	-.106	-.089	-.062	-.048	-.029	-.014	.015	.022
	.450	-.260	-.194	-.187	-.171	-.143	-.134	-.122	-.103	-.089	-.067	-.056	-.040	-.029	.005	.004
	.550	-.181	-.178	-.171	-.160	-.136	-.133	-.123	-.109	-.100	-.079	-.073	-.060	-.050	-.029	.005
	.650	-.148	-.150	-.145	-.139	-.120	-.118	-.114	-.103	-.097	-.081	-.077	-.069	-.061	-.044	-.043
	.750	-.101	-.107	-.105	-.103	-.091	-.093	-.090	-.084	-.081	-.070	-.068	-.063	-.058	-.044	-.044
	.850	-.011	-.019	-.020	-.023	-.014	-.018	-.020	-.018	-.019	-.011	-.014	-.012	-.012	-.005	-.005
	.925	.069	.062	.059	.053	.056	.049	.045	.047	.044	.045	.041	.040	.037	.038	.035
	.975	.115	.108	.103	.097	.095	.086	.081	.078	.075	.075	.067	.066	.060	.055	.044
	1.000	.135	.125	.128	.124	.112	.102	.102	.092	.082	.093	.070	.082	.072	.065	.044

No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($x = 0.45$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(r) $M = 0.58$.

α	2.138	2.164	2.196	2.216	2.247	2.271	2.299	2.327	2.357	2.384	2.419	2.447	2.482	2.510	2.544	2.583
M_x	.703	.700	.699	.695	.694	.691	.689	.687	.684	.683	.680	.678	.676	.674	.672	.669
$C_{L_{max}}$	2.72	2.41	2.02	1.79	1.42	1.15	.84	.53	.21	-.08	-.45	-.73	-1.08	-1.36	-1.69	-2.06
ΔP	.16	.15	.13	.13	.11	.10	.09	.07	.05	.04	.02	.01	-.01	-.03	-.04	-.06
$C_{L_{1/2}}$	1.28	1.19	1.12	1.06	.98	.91	.82	.74	.68	.62	.53	.44	.38	.33	.27	.16
$C_{D_{1/2}}$.5381	.4994	.4703	.4458	.4135	.3845	.3490	.3161	.2897	.2632	.2245	.1897	.1639	.1406	.1055	.0690
C_{D_0}	-.0793	-.0767	-.0752	-.0754	-.0744	-.0752	-.0767	-.0749	-.0755	-.0770	-.0767	-.0770	-.0773	-.0777	-.0778	-.0780
$C_{D_{1/2}}$	-.0060	-.0031														
q/b	Pressure coefficient, P															
Upper surface	θ	1.131	1.129	1.129	1.127	1.127	1.126	1.125	1.124	1.123	1.122	1.121	1.120	1.119	1.119	1.118
	0.000	1.131	1.129	1.129	1.127	1.127	1.126	1.125	1.124	1.123	1.122	1.121	1.120	1.119	1.119	1.118
	.025	-.306	-.223	-.157	-.114	-.075	-.006	.053	.108	.173	.217	.290	.337	.386	.423	.464
	.050	-.538	-.471	-.414	-.374	-.324	-.281	-.232	-.108	-.127	-.088	-.022	.021	.069	.103	.141
	.100	-.615	-.556	-.511	-.477	-.434	-.401	-.361	-.324	-.277	-.247	-.192	-.158	-.119	-.088	-.057
	.200	-.720	-.670	-.634	-.602	-.570	-.541	-.510	-.479	-.440	-.415	-.371	-.342	-.311	-.286	-.259
	.300	-.794	-.745	-.716	-.685	-.656	-.630	-.602	-.577	-.542	-.521	-.483	-.458	-.429	-.409	-.387
	.400	-.833	-.789	-.762	-.730	-.705	-.680	-.657	-.636	-.607	-.588	-.554	-.533	-.508	-.491	-.473
	.500	-.884	-.843	-.816	-.786	-.766	-.742	-.716	-.697	-.671	-.647	-.621	-.591	-.576	-.556	-.542
	.600	-.929	-.890	-.866	-.842	-.816	-.796	-.776	-.754	-.734	-.717	-.699	-.679	-.664	-.644	-.629
	.700	-.951	-.914	-.888	-.866	-.842	-.822	-.802	-.782	-.762	-.747	-.734	-.719	-.704	-.694	-.684
Lower surface	θ	1.131	1.129	1.129	1.127	1.127	1.126	1.125	1.124	1.123	1.122	1.121	1.120	1.119	1.119	1.118
	0.000	1.131	1.129	1.129	1.127	1.127	1.126	1.125	1.124	1.123	1.122	1.121	1.120	1.119	1.119	1.118
	.025	-.306	-.223	-.157	-.114	-.075	-.006	.053	.108	.173	.217	.290	.337	.386	.423	.464
	.050	-.538	-.471	-.414	-.374	-.324	-.281	-.232	-.108	-.127	-.088	-.022	.021	.069	.103	.141
	.100	-.615	-.556	-.511	-.477	-.434	-.401	-.361	-.324	-.277	-.247	-.192	-.158	-.119	-.088	-.057
	.200	-.720	-.670	-.634	-.602	-.570	-.541	-.510	-.479	-.440	-.415	-.371	-.342	-.311	-.286	-.259
	.300	-.794	-.745	-.716	-.685	-.656	-.630	-.602	-.577	-.542	-.521	-.483	-.458	-.429	-.409	-.387
	.400	-.833	-.789	-.762	-.730	-.705	-.680	-.657	-.636	-.607	-.588	-.554	-.533	-.508	-.491	-.473
	.500	-.884	-.843	-.816	-.786	-.766	-.742	-.716	-.697	-.671	-.647	-.621	-.591	-.576	-.556	-.542
	.600	-.929	-.890	-.866	-.842	-.816	-.796	-.776	-.754	-.734	-.717	-.699	-.679	-.664	-.644	-.629
	.700	-.951	-.914	-.888	-.866	-.842	-.822	-.802	-.782	-.762	-.747	-.734	-.719	-.704	-.694	-.684

TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45^\circ$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(g) $M = 0.60$.

	J	2.169	2.192	2.217	2.238	2.266	2.293	2.319	2.346	2.378	2.411	2.430	2.468	2.492	2.525	2.561
M_{∞}		.725	.723	.718	.716	.713	.711	.709	.706	.707	.705	.700	.701	.696	.693	.691
$\Delta\delta$		2.34	2.07	1.78	1.53	1.21	.90	.61	.32	-.02	-.36	-.56	-.95	-1.18	-1.51	-1.85
α_1		.18	.16	.14	.11	.08	.06	.03	.01	-.02	-.04	-.05	-.06	-.08	-.09	-.10
α_n		1.14	1.09	1.01	.95	.86	.79	.72	.65	.58	.51	.45	.38	.32	.25	.17
α_m		.4768	.4606	.4265	.4000	.3626	.3323	.3045	.2735	.2452	.2187	.1935	.1619	.1368	.1065	.0729
α_o		-.0808	-.0773	-.0724	-.0752	-.0757	-.0769	-.0770	-.0793	-.0793	-.0770	-.0770	-.0788	-.0777	-.0793	-.0793
α_o		.0009	.0005	.0021	.0040	.0072	.0094	.0112	.0132	.0151	.0163	.0175	.0198			
a/b	Pressure coefficient, P															
Upper surface	a_o	1.139	1.138	1.136	1.135	1.134	1.133	1.133	1.132	1.132	1.131	1.129	1.129	1.128	1.126	1.126
	.025	.032	-.102	-.060	-.010	.065	.119	.160	.217	.266	.304	.344	.399	.437	.479	.516
	.050	-.408	-.376	-.338	-.293	-.230	-.179	-.141	-.093	-.047	-.012	.025	.079	.112	.153	.189
	.100	-.907	-.822	-.745	-.611	-.358	-.319	-.288	-.247	-.210	-.181	-.152	-.108	-.080	-.046	-.013
	.200	-.697	-.627	-.594	-.564	-.520	-.486	-.460	-.427	-.395	-.368	-.346	-.306	-.286	-.257	-.227
	.300	-.760	-.723	-.692	-.663	-.627	-.595	-.571	-.542	-.513	-.488	-.468	-.435	-.417	-.390	-.364
	.400	-.859	-.810	-.777	-.741	-.705	-.673	-.650	-.623	-.596	-.569	-.554	-.522	-.508	-.485	-.459
	.500	-.830	-.784	-.756	-.731	-.709	-.688	-.670	-.642	-.630	-.609	-.598	-.575	-.564	-.544	-.524
	.600	-.768	-.736	-.715	-.700	-.691	-.679	-.670	-.688	-.674	-.627	-.618	-.603	-.597	-.583	-.566
	.700	-.557	-.550	-.541	-.543	-.546	-.549	-.552	-.549	-.545	-.536	-.536	-.530	-.532	-.524	-.514
	.800	-.293	-.291	-.289	-.295	-.301	-.311	-.318	-.322	-.326	-.323	-.330	-.333	-.341	-.343	-.340
Lower surface	.900	.015	.021	.023	.023	.021	.019	.015	.014	.012	.017	.009	.008	-.002	-.006	-.007
	.950	.096	.104	.109	.111	.111	.112	.111	.115	.116	.120	.122	.125	.122	.126	.130
	.0375	-.041	-.061	-.093	-.139	-.202	-.259	-.307	-.363	-.425	-.463	-.514	-.530	-.542	-.630	-.790
	.075	-.146	-.009	-.043	-.076	-.122	-.162	-.196	-.237	-.277	-.295	-.326	-.371	-.419	-.452	-.472
	.150	-.023	-.029	-.046	-.068	-.098	-.124	-.147	-.179	-.209	-.223	-.248	-.281	-.314	-.338	-.355
	.250	-.099	-.061	-.071	-.088	-.111	-.132	-.153	-.169	-.190	-.198	-.216	-.239	-.265	-.280	-.295
	.350	-.048	-.047	-.057	-.071	-.088	-.102	-.117	-.132	-.148	-.155	-.168	-.186	-.208	-.221	-.228
	.450	-.060	-.059	-.065	-.073	-.090	-.102	-.113	-.124	-.138	-.140	-.153	-.167	-.184	-.194	-.199
	.550	-.084	-.080	-.085	-.090	-.102	-.111	-.121	-.129	-.139	-.140	-.149	-.161	-.173	-.179	-.181
	.650	-.095	-.089	-.091	-.096	-.104	-.109	-.115	-.122	-.128	-.126	-.133	-.140	-.151	-.154	-.151
	.750	-.089	-.082	-.084	-.088	-.091	-.092	-.095	-.099	-.100	-.100	-.104	-.105	-.114	-.114	-.109
	.850	-.034	-.026	-.026	-.027	-.026	-.025	-.022	-.024	-.024	-.022	-.022	-.020	-.025	-.022	-.017
No orifice.	.925	-.026	.035	.036	.037	.041	.043	.044	.047	.050	.054	.054	.059	.056	.061	.067
	.975	.064	.072	.075	.080	.085	.089	.090	.096	.099	.103	.107	.112	.141	.117	.124
a_1	1.000	.085	.099	.094	.108	.107	.095	.120	.122	.122	.132	.138	.155	.175	.140	.156

No orifice.



TABLE 3.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-510.00 PROPELLER BLADE SECTION ($\alpha = 0.45^\circ$; $\beta_x = 59.25^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded.(h) $M = 0.65$.

	J	2.123	2.139	2.172	2.179	2.206	2.218	2.253	2.273	2.299	2.303	2.333	2.356	2.380	2.417
M_{x1}		.808	.801	.801	.794	.791	.785	.788	.782	.780	.774	.772	.770	.765	.764
α_1		2.91	2.71	2.31	2.23	1.90	1.76	1.36	1.13	.84	.80	.47	.21	-.04	-.43
$\Delta\delta$.11	.09	.06	.05	.03	.01	-.01	-.03	-.05	-.05	-.07	-.09	-.11	-.13
α_1		1.06	1.02	.96	.91	.86	.83	.75	.71	.64	.62	.56	.46	.40	.33
b_n		.4419	.4265	.4013	.3832	.3600	.3503	.3161	.2987	.2697	.2626	.2374	.1968	.1703	.1400
c_m		-.0968	-.0983	-.0960	-.0911	-.0934	-.0921	-.0901	-.0888	-.0875	-.0888	-.0849	-.0836	-.0846	-.0846
c_d		.0240	.0248	.0234	.0230	.0232	.0222	.0191	.0197	.0197	.0201	.0199	.0203	.0205	.0210
c/b	Pressure coefficient, P														
Upper surface	θ	0.000	1.174	1.171	1.171	1.168	1.166	1.164	1.165	1.162	1.162	1.159	1.158	1.155	1.155
		.025	.082	.081	.118	.133	.171	.185	.224	.239	.282	.291	.326	.395	.436
		.050	-.231	-.217	-.183	-.171	-.137	-.123	-.088	-.074	-.033	-.025	.007	.072	.113
		.100	-.361	-.348	-.318	-.310	-.284	-.276	-.244	-.235	-.200	-.197	-.170	-.116	-.079
		.200	-.566	-.548	-.512	-.505	-.483	-.476	-.449	-.440	-.409	-.407	-.383	-.337	-.304
		.300	-.654	-.659	-.637	-.638	-.620	-.618	-.595	-.587	-.560	-.559	-.535	-.509	-.461
		.400	-.789	-.795	-.771	-.775	-.760	-.760	-.740	-.736	-.713	-.714	-.691	-.652	-.612
		.500	-.909	-.921	-.895	-.896	-.880	-.875	-.845	-.827	-.800	-.800	-.779	-.732	-.693
		.600	-1.002	-1.006	-.976	-.975	-.960	-.960	-.939	-.919	-.878	-.863	-.831	-.799	-.766
		.700	-.499	-.473	-.464	-.507	-.534	-.613	-.636	-.668	-.665	-.713	-.700	-.685	-.625
Lower surface	θ	.800	-.368	-.370	-.327	-.310	-.294	-.270	-.246	-.230	-.228	-.246	-.248	-.263	-.297
		.900	-.286	-.293	-.250	-.228	-.202	-.166	-.129	-.077	-.040	-.029	-.002	.011	.026
		.950	-.181	-.198	-.164	-.146	-.131	-.100	-.065	-.020	.009	.019	.039	.058	.088
		.0375	-.102	-.141	-.167	-.207	-.257	-.294	-.331	-.358	-.415	-.469	-.521	-.640	-.868
		.075	-.090	-.080	-.096	-.128	-.165	-.193	-.217	-.235	-.277	-.312	-.338	-.364	-.370
		.150	-.056	-.079	-.088	-.110	-.136	-.156	-.170	-.182	-.208	-.238	-.257	-.289	-.328
		.250	-.092	-.109	-.115	-.132	-.155	-.171	-.183	-.192	-.209	-.230	-.242	-.278	-.289
		.350	-.086	-.101	-.101	-.118	-.135	-.148	-.155	-.162	-.174	-.193	-.200	-.218	-.237
		.450	-.105	-.117	-.115	-.128	-.142	-.153	-.158	-.162	-.170	-.187	-.191	-.204	-.216
		.550	-.142	-.152	-.144	-.157	-.168	-.178	-.178	-.179	-.183	-.197	-.197	-.206	-.210

No orifice.

NACA

TABLE 4.-- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$) $\beta_{0.75} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	1.569	1.718	1.860	1.998	2.150	2.309	2.459	2.594	2.685	2.621	2.511	2.380	2.231	2.079	1.931	1.796	1.636
J	.419	.434	.454	.472	.489	.511	.532	.544	.562	.552	.535	.519	.497	.478	.461	.439	.426
α_x'	11.56	8.98	6.71	4.66	2.57	.56	-1.20	-2.24	-3.60	-2.95	-1.77	-.29	1.52	3.53	5.64	7.72	10.38
$\Delta\theta$.50	.42	.35	.29	.20	.10	.01	-.06	-.14	-.10	-.03	.06	.15	.25	.32	.39	.46
α_1	2.84	2.58	2.13	1.75	1.35	.93	.56	.34	.02	.17	.41	.74	1.14	1.54	1.96	2.33	2.68
α_{11}	1.0892	.9890	.8264	.6832	.5316	.3661	.2229	.1361	.0071	.0665	.1642	.2923	.4465	.6019	.7587	.9000	1.0245
α_{12}	-.0562	-.0439	-.0578	-.0659	-.0767	-.0784	-.0789	-.0864	-.0900	-.0847	-.0819	-.0793	-.0787	-.0813	-.0819	-.0505	-.0442
α_0																	
ϕ/b	Pressure coefficient, P																
Upper surface	0.000	1.045	1.048	1.053	1.057	1.061	1.067	1.073	1.076	1.081	1.078	1.073	1.069	1.063	1.059	1.054	1.050
	.025	-1.807	-2.745	-1.643	-1.109	-.560	-.086	.264	.441	.618	.753	.880	.995	1.088	1.158	1.209	1.240
	.050	-1.750	-2.149	-1.430	-1.038	-.667	-.309	-.029	.117	.283	.427	.567	.694	.808	.905	1.000	1.087
	.100	-1.730	-1.587	-1.098	-.842	-.603	-.356	-.158	-.050	.085	.230	.374	.508	.632	.747	.850	1.000
	.200	-1.475	-1.001	-.879	-.722	-.578	-.409	-.274	-.197	-.099	-.143	-.230	-.340	-.483	-.645	-.799	1.000
	.300	-1.156	-.826	-.785	-.679	-.578	-.454	-.331	-.238	-.124	-.247	-.319	-.400	-.508	-.644	-.731	1.000
	.400	-.898	-.738	-.733	-.662	-.596	-.499	-.423	-.379	-.315	-.347	-.402	-.460	-.542	-.669	-.747	1.000
	.500	-.693	-.632	-.640	-.597	-.550	-.480	-.425	-.392	-.345	-.367	-.411	-.451	-.513	-.574	-.618	1.000
	.600	-.542	-.536	-.561	-.534	-.511	-.458	-.420	-.396	-.364	-.380	-.411	-.439	-.483	-.524	-.547	1.000
	.700	-.411	-.414	-.447	-.447	-.442	-.409	-.387	-.375	-.356	-.363	-.384	-.398	-.424	-.447	-.445	1.000
Lower surface	0.000	1.045	1.048	1.053	1.057	1.061	1.067	1.073	1.076	1.081	1.078	1.073	1.069	1.063	1.059	1.054	1.050
	.025	-1.807	-2.745	-1.643	-1.109	-.560	-.086	.264	.441	.618	.753	.880	.995	1.088	1.158	1.209	1.240
	.050	-1.750	-2.149	-1.430	-1.038	-.667	-.309	-.029	.117	.283	.427	.567	.694	.808	.905	1.000	1.087
	.100	-1.730	-1.587	-1.098	-.842	-.603	-.356	-.158	-.050	.085	.230	.374	.508	.632	.747	.850	1.000
	.200	-1.475	-1.001	-.879	-.722	-.578	-.409	-.274	-.197	-.099	-.143	-.230	-.340	-.483	-.645	-.799	1.000
	.300	-1.156	-.826	-.785	-.679	-.578	-.454	-.331	-.238	-.124	-.247	-.319	-.400	-.508	-.644	-.731	1.000
	.400	-.898	-.738	-.733	-.662	-.596	-.499	-.423	-.379	-.315	-.347	-.402	-.460	-.542	-.669	-.747	1.000
	.500	-.693	-.632	-.640	-.597	-.550	-.480	-.425	-.392	-.345	-.367	-.411	-.451	-.513	-.574	-.618	1.000
	.600	-.542	-.536	-.561	-.534	-.511	-.458	-.420	-.396	-.364	-.380	-.411	-.439	-.483	-.524	-.547	1.000
	.700	-.411	-.414	-.447	-.447	-.442	-.409	-.387	-.375	-.356	-.363	-.384	-.398	-.424	-.447	-.445	1.000

*No orifice.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$; $P_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	1.709	1.822	1.937	2.081	2.199	2.322	2.450	2.580	2.668	2.625	2.524	2.388	2.282	2.136	2.025	1.875	1.762
M_{∞}	.517	.531	.550	.571	.587	.609	.630	.651	.666	.659	.640	.618	.600	.576	.561	.536	.520
α	9.13	7.30	5.26	3.50	1.93	.40	-1.10	-2.52	-3.43	-2.99	-1.92	-.38	.89	2.76	4.28	6.48	8.26
$\Delta\theta$.69	.58	.44	.32	.22	.09	-.05	-.17	-.25	-.21	-.12	.01	.13	.27	.37	.53	.64
c_L	2.76	2.39	2.00	1.65	1.26	.93	.57	.24	.04	.14	.40	.75	1.04	1.47	1.81	2.18	2.59
c_H	1.0626	.9252	.7781	.6471	.4935	.3674	.2271	.0977	.0161	.0574	.1603	.2965	.4097	.5768	.7071	.8432	.9994
c_D	-.0416	-.0487	-.0708	-.0772	-.0803	-.0790	-.0858	-.0928	-.1000	-.0939	-.0882	-.0855	-.0856	-.0821	-.0742	-.0649	-.0416
c_c																	
ϕ/b	Pressure coefficient, P																
Upper surface	0.000	1.068	1.072	1.078	1.084	1.089	1.096	1.103	1.110	1.116	1.113	1.106	1.099	1.093	1.085	1.081	1.073
	.025	-2.868	-2.664	-1.411	-.867	-.359	.009	.309	.571	.636	.581	.446	.177	-.126	-.593	-1.107	-1.612
	.050	-2.213	-1.626	-1.294	-.927	-.563	-.272	-.010	.199	.300	.249	.119	-.127	-.383	-.735	-1.089	-1.527
	.100	-1.807	-1.250	-1.001	-.785	-.548	-.342	-.151	.011	.096	.052	-.054	-.237	-.420	-.661	-.880	-1.153
	.200	-1.227	-.990	-.837	-.707	-.561	-.417	-.284	-.165	-.101	-.135	-.214	-.348	-.471	-.630	-.763	-.932
	.300	-.937	-.871	-.772	-.685	-.582	-.477	-.378	-.285	-.235	-.261	-.324	-.427	-.516	-.630	-.722	-.835
	.400	-.795	-.800	-.741	-.685	-.614	-.532	-.460	-.391	-.354	-.373	-.419	-.499	-.561	-.646	-.708	-.783
	.500	-.672	-.695	-.661	-.621	-.572	-.513	-.462	-.413	-.388	-.402	-.433	-.490	-.532	-.593	-.632	-.680
	.600	-.561	-.585	-.579	-.564	-.534	-.489	-.458	-.426	-.413	-.420	-.438	-.480	-.504	-.546	-.566	-.590
	.700	-.426	-.448	-.468	-.472	-.461	-.433	-.419	-.405	-.405	-.405	-.411	-.432	-.440	-.466	-.466	-.490
	.800	-.310	-.294	-.341	-.364	-.376	-.367	-.370	-.378	-.390	-.381	-.374	-.374	-.365	-.369	-.351	-.319
	.900	-.149	-.077	-.074	-.088	-.096	-.097	-.109	-.125	-.142	-.130	-.118	-.107	-.093	-.090	-.080	-.072
	.950	-.083	-.023	.020	.036	.048	.063	.067	.066	.056	.063	.069	.063	.062	.046	.032	-.006
Lower surface	.0375	.751	.684	.525	.349	.126	-.092	-.385	-.765	-1.219	-1.037	-.599	-.295	-.003	.237	.434	.618
	.075	.612	.554	.422	.287	.126	-.020	-.207	-.417	-.816	-.557	-.316	-.125	.047	.212	.354	.497
	.150	.446	.397	.289	.183	.061	-.045	-.167	-.279	-.377	-.308	-.238	-.125	-.003	.119	.233	.346
	.250	.354	.317	.235	.157	.069	-.004	-.090	-.177	-.235	-.200	-.139	-.055	.032	.117	.194	.278
	.350	.295	.270	.203	.141	.073	.016	-.050	-.120	-.161	-.138	-.089	-.025	.045	.111	.172	.239
	.450	.224	.203	.148	.097	.040	-.002	-.077	-.110	-.137	-.122	-.086	-.037	.021	.074	.123	.176
	.550	.139	.127	.083	.044	.001	-.031	-.071	-.110	-.126	-.117	-.091	-.057	-.012	.027	.065	.108
	.650	.106	.102	.071	.042	.008	-.016	-.047	-.073	-.082	-.077	-.058	-.037	.001	.029	.057	.086
	.750	.044	.006	.035	.016	-.005	-.018	-.037	-.050	-.051	-.050	-.043	-.032	-.006	.009	.027	.040
	.850	.054	.068	.069	.060	.050	.049	.040	.068	.035	.036	.039	.040	.056	.062	.065	.066
	.925	-.005	.019	.037	.042	.048	.058	.060	.066	.070	.070	.067	.056	.060	.050	.043	.025
	.975	-.034	-.001	.035	.054	.069	.090	.101	.113	.117	.116	.112	.091	.086	.064	.047	.011
	1.000	-.041	-.009	.033	.062	.043	.127	.145	.160	.146	.145	.142	.125	.108	.073	.052	.010

No orifices.

NACA

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1500$ rpm.

J	2.027	2.105	2.193	2.306	2.417	2.520	2.589	2.559	2.483	2.383	2.254	2.171	2.069	1.981
M_x	.638	.650	.663	.684	.705	.727	.740	.732	.715	.694	.674	.655	.639	.623
α_x	4.25	3.17	2.01	.59	-.72	-1.87	-2.61	-2.29	-1.47	-.33	1.23	2.30	3.66	4.90
$\Delta\theta$.56	.48	.37	.20	0	-.19	-.33	-.26	-.11	.06	.29	.40	.52	.60
α_1	1.89	1.62	1.30	.92	.59	.22	-.05	.10	.42	.69	1.07	1.40	1.75	2.08
c_n	.7361	.6342	.5119	.3645	.2316	.0865	-.0181	.0400	.1652	.2732	.4206	.5497	.6871	.8110
c_m	-.0762	-.0793	-.0850	-.0880	-.0905	-.0973	-.1078	-.1021	-.0905	-.0880	-.0854	-.0818	-.0783	-.0723
c_o														
a/b	Pressure coefficient, P													
Upper surface	0.000	1.106	1.110	1.115	1.123	1.131	1.140	1.145	1.142	1.135	1.127	1.119	1.112	1.106
	.025	-1.012	-.644	-.292	.100	.374	.598	.639	.599	.488	.286	-.044	-.380	-.822
	.050	-1.166	-.862	-.575	-.243	.010	.193	.282	.238	.120	-.075	-.364	-.641	-1.000
	.100	-.886	-.722	-.545	-.317	-.127	.021	.098	.060	-.043	-.193	-.401	-.585	-.802
	.200	-.802	-.691	-.583	-.428	-.289	-.176	-.112	-.145	-.227	-.339	-.485	-.604	-.743
	.300	-.761	-.685	-.603	-.489	-.382	-.295	-.244	-.269	-.336	-.418	-.526	-.613	-.720
	.400	-.744	-.693	-.639	-.561	-.477	-.411	-.369	-.389	-.441	-.506	-.583	-.642	-.717
	.500	-.698	-.626	-.594	-.543	-.484	-.442	-.415	-.425	-.464	-.505	-.555	-.591	-.643
	.600	-.608	-.589	-.572	-.544	-.507	-.487	-.474	-.480	-.501	-.521	-.548	-.567	-.600
	.700	-.543	-.539	-.532	-.532	-.516	-.521	-.527	-.523	-.525	-.523	-.528	-.529	-.543
	.800	-.334	-.339	-.347	-.350	-.343	-.354	-.361	-.357	-.356	-.333	-.344	-.338	-.341
Lower surface	.900	-.062	-.064	-.074	-.079	-.078	-.091	-.101	-.097	-.093	-.081	-.075	-.065	-.069
	.950	.030	.045	.052	.064	.080	.078	.078	.078	.076	.071	.064	.057	.054
	.0375	.407	.280	.110	-.151	-.418	-1.238	-1.572	-1.515	-.562	-.315	-.038	.167	.342
	.075	.345	.253	.131	-.044	-.210	-.387	-1.192	-.600	-.312	-.150	.030	.174	.297
	.150	.247	.180	.090	-.035	-.149	-.259	-.274	-.269	-.225	-.110	.021	.124	.212
	.250	.202	.149	.080	-.008	-.088	-.178	-.212	-.198	-.147	-.063	.035	.108	.172
	.350	.165	.133	.079	.004	-.056	-.130	-.166	-.148	-.103	-.037	.041	.102	.143
	.450	.127	.095	.049	-.010	-.058	-.117	-.147	-.131	-.096	-.043	.019	.070	.108
	.550	.093	.064	.025	-.020	-.055	-.102	-.127	-.115	-.088	-.046	.004	.044	.078
	.650	.060	.035	.003	-.034	-.058	-.092	-.108	-.100	-.083	-.052	-.015	.019	.046
	.750	.045	.025	.003	-.020	-.035	-.056	-.064	-.060	-.051	-.031	-.007	.019	.035
	.850	.062	.068	.054	.040	.038	.025	.022	.024	.028	.037	.050	.065	.069
	.925	.073	.071	.066	.067	.075	.073	.076	.077	.073	.072	.071	.076	.071
	.975	.055	.064	.071	.084	.104	.111	.120	.118	.109	.096	.082	.076	.060
	1.000	.032	.058	.072	.088	.122	.178	.183	.199	.155	.144	.127	.117	.108

No orifices.



TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION. ($x = 0.60$; $\beta_x = 31.33^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1600$ rpm.

$\frac{r}{R}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$	$C_{p,u}$	$C_{p,l}$
0.000	2.095	2.183	2.237	2.314	2.383	2.458	2.531	2.509	2.434	2.354	2.280	2.221	2.141	
0.025	.683	.699	.712	.726	.738	.753	.774	.764	.746	.730	.716	.702	.687	
0.050	3.31	2.14	1.45	.90	-.32	-1.19	-2.21	-1.75	-.91	.02	.92	1.65	2.69	
0.100	.43	.30	.21	.08	-.07	-.23	-.41	-.34	-.18	0	.14	.23	.37	
0.200	1.79	1.50	1.29	1.00	.79	.46	.14	.28	.62	.87	1.10	1.35	1.62	
0.300	.7032	.5897	.5077	.3948	.3135	.1839	.0548	.1103	.2439	.3426	.4342	.5316	.6381	
0.400	-.0862	-.0864	-.0942	-.0942	-.0944	-.0986	-.1047	-.1041	-.0929	-.0921	-.0921	-.0895	-.0860	
0.500						.0215	.0264	.0239						
0.600														
0.700														
0.800														
0.900														
0.950														
1.000														
Upper surface														
0.000	1.122	1.129	1.134	1.139	1.144	1.150	1.159	1.155	1.148	1.141	1.135	1.130	1.124	
0.025	-.718	-.347	-.127	.129	.297	.483	.604	.592	.432	.229	.048	-.197	-.518	
0.050	-1.010	-.635	-.436	-.208	-.074	.131	.270	.206	.055	-.129	-.293	-.507	-.795	
0.100	-.841	-.628	-.493	-.323	-.197	-.053	.070	.014	-.105	-.264	-.357	-.536	-.725	
0.200	-.806	-.668	-.576	-.452	-.356	-.243	-.136	-.185	-.283	-.410	-.497	-.600	-.728	
0.300	-.801	-.712	-.648	-.554	-.477	-.386	-.291	-.334	-.417	-.521	-.586	-.659	-.747	
0.400	-.809	-.762	-.723	-.661	-.603	-.531	-.447	-.485	-.551	-.636	-.674	-.720	-.773	
0.500	-.711	-.693	-.677	-.644	-.610	-.564	-.501	-.528	-.574	-.631	-.644	-.663	-.691	
0.600	-.628	-.625	-.624	-.616	-.609	-.602	-.568	-.580	-.591	-.600	-.608	-.609	-.621	
0.700	-.505	-.512	-.520	-.525	-.526	-.543	-.562	-.548	-.513	-.510	-.509	-.498	-.500	
0.800	-.333	-.343	-.354	-.365	-.339	-.363	-.387	-.385	-.370	-.383	-.363	-.346	-.340	
0.900	-.044	-.040	-.043	-.045	-.040	-.049	-.049	-.049	-.040	-.060	-.046	-.036	-.041	
0.950	.033	.044	.049	.056	.067	.069	.077	.075	.075	.050	.056	.055	.041	
Lower surface														
0.0375	.332	.175	.043	-.143	-.311	-.486	-.639	-.850	-.416	-.269	-.086	.096	.250	
0.075	.285	.171	.075	-.056	-.153	-.281	-.428	-.611	-.248	-.133	-.007	.119	.226	
0.150	.183	.097	.026	-.066	-.135	-.251	-.371	-.469	-.206	-.139	-.044	.055	.136	
0.250	.131	.059	.048	-.020	-.067	-.157	-.207	-.291	-.116	-.067	.003	.075	.133	
0.350	.154	.106	.063	.008	-.027	-.101	-.152	-.189	-.069	-.033	.025	.082	.127	
0.450	.110	.071	.035	-.010	-.038	-.100	-.147	-.122	-.070	-.047	.008	.052	.089	
0.550	.052	.022	-.006	-.039	-.059	-.109	-.147	-.126	-.085	-.072	-.031	.011	.039	
0.650	.035	.031	.006	-.022	-.036	-.076	-.102	-.087	-.057	-.050	-.017	.018	.041	
0.750	.028	.004	-.010	-.025	-.031	-.059	-.075	-.063	-.046	-.050	-.024	.005	.018	
0.850	.075	.068	.056	.045	.045	.028	.026	.032	.038	.025	.045	.063	.069	
0.925	.055	.056	.052	.051	.057	.049	.054	.053	.055	.033	.046	.058	.053	
0.975	.052	.060	.060	.067	.078	.077	.090	.091	.081	.053	.062	.063	.053	
1.000	.062	.079	.085	.100	.102	.110	.126	.135	.116	.089	.090	.080	.070	

No orifice.



TABLE 4.- PRESSURE COEFFICIENTS AND APPROXIMATE CHARACTERISTICS OF AN
NACA 16-507.50 PROPELLER BLADE SECTION ($x = 0.60$; $\beta_x = 51.33^\circ$;

$\beta_{0.75x} = 45^\circ$; $B = 2$) - Continued

(a) $M = 0.56$.

	J	2.621	2.563	2.527	2.492	2.447	2.403	2.379	2.338	2.302	2.269	2.246	2.212	2.188	2.168	2.135	2.117
M_x		.700	.701	.709	.715	.717	.722	.727	.732	.734	.738	.744	.745	.748	.754	.756	.759
α_x		-2.95	-2.94	-1.95	-1.57	-1.06	-.56	-.28	.21	.64	1.05	1.34	1.77	2.07	2.33	2.77	3.01
$\Delta\theta$		-.23	-.19	-.16	-.13	-.08	-.01	.03	.07	.09	.11	.12	.14	.17	.19	.25	.30
α_1		.01	.13	.26	.38	.47	.62	.69	.81	.92	1.03	1.12	1.22	1.29	1.37	1.47	1.53
c_n		-.0052	.0535	.1026	.1487	.1874	.2439	.2735	.3203	.3613	.4071	.4426	.4794	.5077	.5400	.5755	.6006
c_m		-.0908	-.0852	-.0857	-.0844	-.0844	-.0846	-.0850	-.0865	-.0840	-.0824	-.0828	-.0839	-.0872	-.0865	-.0885	-.0869
c_o															-.0002	-.0031	-.0051
a/b	Pressure coefficient, P																
Upper surface	$a_0,000$	1.129	1.130	1.133	1.135	1.136	1.138	1.140	1.142	1.143	1.144	1.146	1.147	1.148	1.151	1.152	1.153
	.025	.636	.589	.551	.497	.445	.397	.309	.217	.131	.040	-.009	-.080	-.141	-.201	-.276	-.328
	.050	.294	.244	.206	.155	.104	.084	-.019	-.101	-.173	-.249	-.293	-.356	-.411	-.466	-.538	-.594
	.100	.105	.062	.029	-.012	-.053	-.115	-.150	-.213	-.270	-.329	-.362	-.407	-.447	-.481	-.528	-.557
	.200	-.095	-.132	-.161	-.196	-.232	-.286	-.313	-.368	-.415	-.462	-.491	-.527	-.560	-.586	-.622	-.649
	.300	-.224	-.258	-.282	-.315	-.347	-.394	-.419	-.469	-.511	-.553	-.581	-.613	-.642	-.669	-.721	-.754
	.400	-.338	-.370	-.393	-.422	-.453	-.494	-.520	-.568	-.609	-.652	-.688	-.725	-.761	-.791	-.819	-.829
	.500	-.376	-.404	-.422	-.446	-.470	-.501	-.521	-.560	-.592	-.620	-.646	-.671	-.707	-.765	-.823	-.864
	.600	-.435	-.456	-.470	-.487	-.508	-.528	-.542	-.571	-.592	-.612	-.631	-.644	-.659	-.669	-.683	-.680
	.700	-.414	-.429	-.437	-.443	-.455	-.464	-.469	-.484	-.493	-.497	-.500	-.499	-.498	-.491	-.487	-.479
	.800	-.370	-.372	-.368	-.360	-.360	-.352	-.347	-.344	-.341	-.329	-.324	-.313	-.305	-.289	-.281	-.270
Lower surface	.900	-.120	-.111	-.098	-.085	-.078	-.065	-.058	-.053	-.051	-.044	-.040	-.034	-.034	-.030	-.031	-.030
	.950	.059	.063	.071	.073	.074	.075	.074	.065	.058	.054	.049	.044	.037	.033	.023	.020
	.0375	-1.318	-1.161	-.889	-.551	-.414	-.311	-.238	-.198	-.121	-.025	.021	.080	.120	.165	.207	.238
	.075	-.707	-.542	-.428	-.349	-.310	-.236	-.189	-.119	-.063	-.005	.024	.063	.091	.125	.157	.184
	.150	-.369	-.312	-.275	-.238	-.208	-.155	-.129	-.087	-.053	-.013	.007	.038	.057	.083	.107	.127
	.250	-.237	-.213	-.184	-.155	-.133	-.093	-.073	-.044	-.020	.009	.025	.047	.063	.082	.100	.117
	.350	-.171	-.156	-.134	-.111	-.095	-.063	-.047	-.025	-.008	.016	.028	.047	.059	.074	.088	.102
	.450	-.147	-.137	-.121	-.102	-.089	-.065	-.052	-.036	-.023	-.005	.005	.019	.029	.042	.054	.064
	.550	-.122	-.117	-.104	-.089	-.079	-.061	-.051	-.039	-.030	-.014	-.008	.004	.012	.021	.030	.039
	.650	-.101	-.100	-.092	-.081	-.076	-.061	-.052	-.047	-.041	-.031	-.025	-.016	-.011	-.003	.002	.008
	.750	-.058	-.062	-.056	-.049	-.048	-.038	-.034	-.031	-.029	-.022	-.020	-.013	-.011	-.006	-.003	.001
	.850	.023	.018	.023	.026	.025	.031	.033	.032	.031	.032	.034	.036	.037	.041	.041	.043
No orifice.	.925	.072	.068	.071	.072	.069	.069	.069	.063	.059	.058	.056	.057	.053	.053	.050	.049
	.975	.115	.109	.108	.106	.100	.094	.091	.081	.072	.066	.061	.057	.051	.048	.039	.035
	1.000	.130	.130	.120	.130	.113	.109	.100	.090	.075	.069	.060	.059	.050	.040	.030	.030

^aNo orifice.

NACA

TABLE 4. - PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($\alpha = 0.60$; $\beta_x = 51.33^\circ$) $R_{0.75R} = 45^\circ$; $B = 2$ - Continued $(x) M = 0.58$.

J	2.584	2.549	2.509	2.471	2.421	2.381	2.343	2.315	2.289	2.260	2.241	2.211	2.185	2.152	2.131
M_x	.727	.735	.739	.743	.744	.749	.753	.757	.760	.764	.772	.775	.779	.781	.788
a_x	-2.56	-2.18	-1.75	-1.33	-1.76	-1.30	.15	.49	.81	1.16	1.40	1.78	2.12	2.54	2.81
a_1	-33	-27	-21	-17	-12	-10	-8	-5	0	.05	.16	.22	.30	.34	.34
a_2	-3	10	21	37	51	61	76	83	91	1.00	1.08	1.16	1.25	1.36	1.44
a_m	-.0110	.0394	.0852	.1484	.2006	.2423	.3006	.3271	.3574	.3926	.4239	.4568	.4910	.5355	.5632
a_n	-.0988	-.0964	-.0932	-.0909	-.0893	-.0879	-.0892	-.0886	-.0890	-.0882	-.0918	-.0911	-.0928	-.0973	-.1009
a_c						.0192	.0159	.0141	.0128	.0108	.0097	.0077	.0067	.0031	.0024
o/b	Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.140	1.143	1.145	1.147	1.147	1.149	1.150	1.152	1.153	1.155	1.158	1.159	1.161	1.165
	.025	.634	.590	.556	.492	.435	.372	.304	.247	.200	.155	.089	.039	-.026	-.127
	.050	.289	.246	.204	.148	.093	.034	-.045	-.075	-.116	-.173	-.213	-.257	-.316	-.410
	.100	.102	.067	.037	-.014	-.062	-.110	-.170	-.233	-.297	-.370	-.448	-.531	-.615	-.796
	.200	-.102	-.133	-.162	-.205	-.249	-.290	-.342	-.397	-.422	-.448	-.471	-.503	-.553	-.694
	.300	-.236	-.261	-.288	-.327	-.368	-.411	-.457	-.469	-.499	-.530	-.552	-.573	-.615	-.699
	.400	-.359	-.381	-.408	-.445	-.490	-.532	-.579	-.597	-.630	-.663	-.692	-.721	-.741	-.796
	.500	-.399	-.416	-.441	-.471	-.510	-.548	-.583	-.591	-.622	-.666	-.721	-.760	-.792	-.853
	.600	-.462	-.472	-.493	-.512	-.547	-.577	-.603	-.608	-.637	-.669	-.681	-.725	-.807	-.925
	.700	-.441	-.442	-.456	-.463	-.485	-.497	-.503	-.497	-.508	-.513	-.516	-.514	-.510	-.494
	.800	-.372	-.361	-.359	-.351	-.355	-.349	-.338	-.317	-.319	-.306	-.295	-.281	-.270	-.249
Lower surface	.900	-.099	-.079	-.071	-.059	-.057	-.051	-.043	-.028	-.034	-.029	-.023	-.028	-.031	-.047
	.950	.073	.084	.084	.082	.076	.070	.064	.070	.058	.050	.045	.036	.023	-.027
	.0375	-.1562	-.1398	-.1262	-.1149	-.1044	-.0999	-.0912	-.0875	-.083	-.083	.024	.023	.081	.152
	.075	-.878	-.581	-.462	-.319	-.290	-.251	-.163	-.110	-.087	-.037	-.001	.028	.067	.116
	.150	-.325	-.276	-.256	-.221	-.198	-.166	-.115	-.079	-.066	-.035	-.009	.014	.042	.079
	.250	-.233	-.195	-.179	-.145	-.126	-.102	-.063	-.035	-.029	-.004	.014	.030	.051	.079
	.350	-.176	-.143	-.129	-.103	-.089	-.072	-.040	-.016	-.013	.003	.020	.032	.050	.070
	.450	-.152	-.126	-.118	-.096	-.087	-.075	-.051	-.030	-.029	-.016	-.002	.007	.021	.036
	.550	-.127	-.107	-.101	-.085	-.080	-.071	-.051	-.034	-.036	-.025	-.015	-.008	.002	.014
	.650	-.106	-.092	-.089	-.079	-.079	-.075	-.059	-.043	-.047	-.041	-.033	-.030	-.023	-.015
	.750	-.061	-.052	-.053	-.047	-.049	-.050	-.040	-.027	-.031	-.029	-.026	-.024	-.020	-.019
	.850	.021	.028	.027	.029	.023	.021	.025	.035	.029	.028	.031	.028	.028	.024
	.925	.073	.078	.075	.074	.066	.059	.059	.067	.058	.054	.050	.046	.037	.029
	.975	.113	.115	.111	.106	.093	.083	.077	.062	.070	.061	.058	.048	.039	.025
	$a_{1.000}$.125	.150	.150	.128	.115	.102	.098	.096	.081	.074	.060	.057	.042	-.024

^aNo crillet.

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($x = 0.60$; $\beta_x = 51.33^\circ$; $\beta_{0.728} = 45^\circ$; $B = 2$) - Continued(c) $M = 0.60$.

J	2.112	2.148	2.192	2.229	2.275	2.307	2.348	2.387	2.431	2.477	2.533	2.567
M_x	.814	.808	.800	.796	.794	.795	.780	.771	.766	.760	.762	.754
α_x	3.08	2.60	2.02	1.55	.97	.58	.09	-.37	-.88	-1.40	-2.02	-2.38
$\Delta\theta$.18	.15	.10	.05	-.02	-.07	-.14	-.19	-.25	-.30	-.37	-.42
α_1	1.46	1.39	1.25	1.09	.95	.83	.70	.57	.45	.34	.17	.05
α_n	.5729	.5458	.4910	.4297	.3793	.3258	.2771	.2274	.1768	.1329	.0698	.0194
α_m	-.1259	-.1208	-.1160	-.1085	-.1059	-.1031	-.1032	-.1045	-.1065	-.1042	-.1119	-.1159
α_c	.0182	.0162	.0154	.0159	.0165	.0177	.0191	.0200	.0219	.0232	.0254	.0265
q/b	Pressure coefficient, P											
Upper surface	$\alpha_0.000$	1.177	1.174	1.171	1.168	1.168	1.164	1.162	1.158	1.156	1.153	1.151
	.025	-.009	.038	.097	.177	.258	.315	.369	.417	.476	.524	.614
	.050	-.375	-.324	-.253	-.177	-.097	-.038	.019	.066	.124	.176	.271
	.100	-.357	-.394	-.344	-.286	-.223	-.177	-.134	-.097	-.051	-.009	.041
	.200	-.573	-.516	-.481	-.438	-.390	-.355	-.320	-.288	-.246	-.209	-.136
	.300	-.680	-.657	-.626	-.564	-.517	-.487	-.456	-.427	-.390	-.354	-.286
	.400	-.789	-.766	-.724	-.706	-.673	-.636	-.613	-.583	-.542	-.503	-.435
	.500	-.856	-.833	-.803	-.765	-.724	-.692	-.645	-.601	-.571	-.539	-.479
	.600	-.921	-.899	-.863	-.834	-.789	-.735	-.704	-.671	-.631	-.588	-.527
	.700	-.919	-.916	-.899	-.885	-.829	-.770	-.738	-.697	-.655	-.613	-.568
	.800	-.981	-.954	-.901	-.876	-.820	-.764	-.731	-.689	-.647	-.604	-.546
Lower surface	$\alpha_0.000$	-.0375	.072	.021	-.042	-.138	-.227	-.329	-.446	-.641	-1.032	-1.476
	.075	.103	.069	.016	-.047	-.108	-.159	-.213	-.285	-.412	-.630	-1.213
	.150	.047	.021	-.011	-.060	-.100	-.142	-.178	-.208	-.245	-.286	-.275
	.250	.077	.059	.031	-.002	-.031	-.063	-.091	-.111	-.147	-.169	-.200
	.350	.061	.049	.028	0	-.021	-.046	-.066	-.084	-.111	-.127	-.158
	.450	.024	.016	-.001	-.020	-.035	-.054	-.070	-.084	-.105	-.117	-.140
	.550	-.007	-.011	-.021	-.035	-.044	-.057	-.070	-.079	-.094	-.102	-.116
	.650	-.044	-.041	-.046	-.054	-.056	-.065	-.073	-.076	-.087	-.091	-.096
	.750	-.067	-.060	-.053	-.056	-.051	-.053	-.056	-.057	-.061	-.060	-.056
	.850	-.029	-.010	.001	.007	.016	.019	.019	.023	.022	.025	.032
	.925	-.055	-.021	.004	.017	.033	.041	.046	.053	.056	.062	.073
	.975	-.118	-.063	-.017	.007	.028	.041	.051	.064	.074	.084	.098
	1.000	-.160	-.095	-.032	-.012	.020	.043	.053	.076	.082	.101	.109

^aNo crinloe.

TABLE 4.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-507.50 PROPELLER BLADE SECTION ($x = 0.60$; $\beta_x = 51.33^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

	2.448	2.403	2.388	2.350	2.313	2.299	2.264	2.235	2.202	2.183	2.162	2.125	2.116
J	.830	.834	.841	.843	.846	.853	.856	.861	.865	.871	.877	.878	.885
M_x	-1.07	-.56	-.38	.06	.51	.68	1.11	1.47	1.89	2.14	2.41	2.90	3.02
$\Delta\theta$	-.44	-.38	-.37	-.32	-.28	-.27	-.23	-.19	-.15	-.13	-.10	-.06	-.05
α_1	.06	.19	.27	.38	.47	.52	.62	.68	.80	.86	.93	1.01	1.08
α_2	.0232	.0748	.1058	.1484	.1852	.2045	.2419	.2658	.3155	.3374	.3645	.3929	.4219
α_m	-.1001	-.1008	-.1016	-.1021	-.1037	-.1045	-.1021	-.1013	-.1045	-.1080	-.1083	-.1093	-.1072
α_0	.0301	.0310	.0319	.0320	.0326	.0335	.0343	.0350	.0350	.0355	.0350	.0344	.0333
c/b	Pressure coefficient, P												
Upper surface	0.000	1.184	1.186	1.189	1.190	1.192	1.195	1.197	1.199	1.201	1.204	1.207	1.211
	.025	.574	.540	.519	.488	.448	.432	.392	.359	.315	.296	.273	.285
	.050	.239	.205	.187	.155	.115	.101	.065	.037	-.004	-.021	-.041	-.124
	.100	.074	.045	.031	.005	-.029	-.039	-.067	-.088	-.119	-.130	-.141	-.197
	.200	-.132	-.158	-.169	-.191	-.220	-.226	-.249	-.264	-.286	-.294	-.297	-.355
	.300	-.273	-.296	-.304	-.322	-.349	-.354	-.387	-.414	-.435	-.438	-.455	-.469
	.400	-.433	-.451	-.461	-.487	-.512	-.513	-.522	-.527	-.550	-.556	-.557	-.585
	.500	-.515	-.536	-.545	-.560	-.586	-.590	-.610	-.625	-.632	-.635	-.634	-.660
	.600	-.617	-.649	-.649	-.669	-.693	-.695	-.712	-.720	-.732	-.736	-.733	-.759
	.700	-.706	-.749	-.760	-.772	-.791	-.791	-.804	-.815	-.826	-.827	-.823	-.830
	.800	-.297	-.308	-.311	-.313	-.320	-.324	-.336	-.355	-.369	-.384	-.379	-.387
Lower surface	.900	-.075	-.111	-.140	-.163	-.197	-.217	-.242	-.267	-.286	-.300	-.302	-.319
	.950	-.016	-.054	-.085	-.116	-.163	-.197	-.233	-.267	-.291	-.307	-.309	-.335
	.0375	-.962	-.915	-.841	-.767	-.682	-.603	-.456	-.326	-.210	-.155	-.078	-.060
	.075	-.911	-.848	-.765	-.672	-.542	-.456	-.319	-.247	-.135	-.098	-.051	-.016
	.150	-.627	-.394	-.293	-.206	-.170	-.199	-.138	-.117	-.076	-.053	-.020	.033
	.250	-.183	-.171	-.162	-.150	-.136	-.120	-.099	-.082	-.048	-.028	.001	.042
	.350	-.157	-.152	-.143	-.130	-.117	-.103	-.087	-.071	-.042	-.027	.001	.030
	.450	-.166	-.162	-.155	-.143	-.135	-.123	-.110	-.100	-.075	-.062	-.037	-.012
	.550	-.165	-.163	-.158	-.149	-.145	-.137	-.129	-.124	-.103	-.092	-.069	-.048
	.650	-.165	-.168	-.165	-.160	-.164	-.161	-.159	-.159	-.144	-.136	-.114	-.097
	.750	-.133	-.142	-.142	-.143	-.152	-.155	-.161	-.167	-.159	-.156	-.137	-.126
	.850	-.044	-.059	-.063	-.070	-.087	-.095	-.109	-.122	-.118	-.118	-.104	-.099
	.925	-.002	-.023	-.034	-.046	-.072	-.088	-.110	-.130	-.135	-.139	-.128	-.127
	.975	.020	-.011	-.033	-.057	-.101	-.132	-.172	-.207	-.226	-.239	-.236	-.246
	1.000	.032	-.009	-.035	-.059	-.124	-.187	-.228	-.272	-.309	-.319	-.323	-.355

No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-306.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

J	1.608	1.766	1.945	2.139	2.254	2.367	2.514	2.654	2.592	2.443	2.321	2.195	2.066	1.875	1.667	
M _x	.473	.487	.507	.532	.546	.562	.579	.598	.587	.570	.552	.538	.521	.501	.478	
α _x	10.83	8.23	5.51	2.79	1.29	-.11	-1.82	-3.35	-2.69	-1.01	.46	2.05	3.79	6.55	9.84	
Δθ	.74	.62	.48	.33	.22	.11	-.05	-.22	-.15	.03	.16	.27	.39	.54	.69	
α ₁	2.97	2.69	2.13	1.57	1.21	.87	.48	.06	.28	.65	1.00	1.38	1.78	2.35	2.89	
c _n	1.0445	.9568	.7639	.5645	.4400	.3158	.1752	.0213	.1032	.2371	.3613	.4968	.6387	.8374	1.0219	
c _m	-.0465	-.0634	-.0829	-.0928	-.0944	-.0955	-.0950	-.1062	-.0990	-.0925	-.0928	-.0933	-.0887	-.0757	-.0503	
c/b	Pressure coefficient, P															
Upper surface	a ₀	1.057	1.061	1.066	1.072	1.076	1.081	1.086	1.092	1.088	1.083	1.078	1.074	1.070	1.064	1.059
	.025	-2.456	-2.495	-1.220	-.517	-.143	.162	.429	.593	.533	.321	.063	-.326	-.776	-1.531	-2.639
	.050	-2.250	-2.162	-1.268	-.714	-.427	-.180	.072	.245	.180	-.036	-.263	-.573	-.909	-1.430	-2.349
	.100	-1.824	-1.299	-.933	-.627	-.436	-.269	-.081	.063	.006	-.162	-.327	-.534	-.758	-1.096	-1.689
	.200	-1.233	-.923	-.782	-.579	-.453	-.340	-.210	-.101	-.142	-.265	-.378	-.517	-.658	-.860	-1.096
	.300	-.899	-.808	-.706	-.570	-.478	-.401	-.298	-.211	-.245	-.342	-.428	-.526	-.626	-.757	-.886
	.400	-.710	-.716	-.649	-.552	-.484	-.429	-.354	-.282	-.307	-.384	-.447	-.517	-.594	-.683	-.702
	.500	-.574	-.639	-.606	-.541	-.491	-.450	-.392	-.342	-.355	-.418	-.463	-.517	-.571	-.624	-.598
	.600	-.466	-.558	-.549	-.512	-.478	-.454	-.411	-.373	-.383	-.427	-.461	-.495	-.535	-.575	-.502
	.700	-.363	-.471	-.497	-.492	-.474	-.464	-.438	-.417	-.419	-.447	-.467	-.487	-.503	-.487	-.401
	.800	-.265	-.299	-.339	-.357	-.351	-.356	-.346	-.339	-.333	-.344	-.352	-.356	-.356	-.319	-.263
	.900	-.189	-.113	-.116	-.149	-.154	-.169	-.177	-.185	-.172	-.119	-.163	-.154	-.140	-.103	-.135
.950	-.154	-.031	.010	.015	.018	.009	.005	-.007	.007	.012	.013	.017	.011	-.005	-.087	
Lower surface	.0375	.779	.689	.522	.236	.043	-.192	-.511	-1.159	-.924	-.330	-.103	.143	.342	.607	.748
	.075	.640	.557	.413	.192	.052	-.117	-.298	-.904	-.527	-.210	-.055	.126	.271	.484	.610
	.150	.505	.434	.320	.161	.058	-.052	-.173	-.393	-.224	-.115	-.004	.113	.214	.376	.477
	.250	.407	.347	.263	.136	.067	-.015	-.104	-.189	-.133	-.059	.013	.102	.180	.307	.384
	.350	.323	.281	.203	.099	.045	-.023	-.093	-.134	-.108	-.057	0	.070	.127	.241	.307
	.450	.255	.209	.132	.052	.014	-.041	-.097	-.120	-.105	-.071	-.022	.033	.077	.172	.237
	.550	.201	.178	.137	.072	.039	-.007	-.047	-.069	-.054	-.028	.009	.054	.091	.157	.195
	.650	.136	.127	.096	.048	.024	-.011	-.041	-.052	-.041	-.028	0	.035	.059	.113	.136
	.750	.101	.112	.094	.061	.045	.017	-.001	-.007	.002	.008	.027	.052	.068	.103	.110
	.850	.068	.102	.099	.085	.077	.060	.051	.048	.056	.055	.057	.083	.084	.101	.088
	.925	.060	.117	.129	.140	.132	.121	.114	.108	.118	.121	.125	.130	.123	.125	.088
	.975	.142	.191	.203	.221	.244	.235	.237	.238	.245	.237	.236	.217	.210	.192	.179
1.000	.235	.248	.250	.285	.328	.332	.383	.338	.335	.350	.340	.287	.271	.308	.279	

^aNo orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued.(b) $N = 1350$ rpm.

	J	M_x	$q_{x'}$	$\Delta\theta$	α_1	c_{D1}	c_{D2}	c_{D3}	c_{D4}	c_{D5}	c_{D6}	c_{D7}	c_{D8}	c_{D9}	c_{D10}	c_{D11}	c_{D12}	c_{D13}	c_{D14}	c_{D15}	c_{D16}	c_{D17}	c_{D18}	c_{D19}	c_{D20}		
	1.663	1.786	1.885	1.984	2.095	2.209	2.312	2.438	2.547	2.637	2.704	2.804	2.886	2.971	3.049	3.162	3.068	1.958	1.845	1.734							
	.569	.580	.598	.606	.625	.642	.656	.676	.695	.708	.700	.684	.664	.644	.631	.618	.603	.587	.572	.552							
	9.90	7.92	6.40	4.94	3.39	1.87	.57	-.95	-2.19	-3.17	-2.60	-1.51	-.16	1.36	2.49	3.76	5.32	7.00	8.74								
	1.12	.93	.77	.62	.45	.27	.10	-.09	-.26	-.39	-.32	-.17	.01	.21	.34	.49	.66	.84	1.01								
	3.00	2.82	2.57	2.15	1.77	1.43	1.06	.69	.34	.07	.24	.51	.89	1.26	1.61	1.96	2.31	2.73	3.02								
	1.0639	1.0052	.9168	.7710	.6374	.5174	.3852	.2516	.1226	.0245	.0890	.1892	.3219	.4581	.5810	.7039	.8277	.9742	1.0742								
	-.0452	-.0598	-.0744	-.0847	-.0944	-.0991	-.1006	-.1031	-.1082	-.1167	-.1091	-.1032	-.0989	-.0992	-.0950	-.0860	-.0821	-.0633	-.0519								
c/b	Pressure coefficient, P																										
Upper surface	0.000	1.083	1.087	1.092	1.095	1.101	1.107	1.112	1.120	1.127	1.133	1.130	1.123	1.115	1.108	1.103	1.099	1.094	1.089	1.084							
	.025	-2.235	-2.939	-2.278	-1.103	-.663	-.248	.096	.361	.538	.633	.581	.460	.235	-.094	-.412	-.823	-1.221	-2.641	-3.241							
	.050	-2.169	-2.693	-1.487	-1.328	-.903	-.563	-.264	-.014	.171	.276	.219	.086	-.137	-.430	-.699	-1.028	-1.470	-2.239	-2.947							
	.100	-1.979	-1.252	-1.190	-.996	-.773	-.555	-.346	-.157	-.010	.081	.089	-.081	-.253	-.466	-.642	-.854	-1.065	-1.168	-1.624							
	.200	-1.350	-.980	-.929	-.815	-.687	-.555	-.415	-.282	-.175	-.102	-.143	-.226	-.351	-.499	-.608	-.728	-.847	-.963	-.978							
	.300	-.888	-.868	-.829	-.749	-.667	-.574	-.477	-.375	-.289	-.232	-.265	-.330	-.429	-.535	-.610	-.688	-.774	-.846	-.876							
	.400	-.700	-.765	-.741	-.689	-.632	-.568	-.501	-.428	-.364	-.320	-.344	-.395	-.467	-.543	-.593	-.646	-.707	-.749	-.770							
	.500	-.592	-.684	-.678	-.649	-.613	-.571	-.523	-.468	-.425	-.394	-.413	-.446	-.498	-.555	-.584	-.620	-.658	-.679	-.679							
	.600	-.484	-.589	-.601	-.587	-.571	-.545	-.505	-.479	-.453	-.437	-.446	-.464	-.498	-.535	-.550	-.577	-.586	-.596	-.581							
	.700	-.376	-.491	-.525	-.532	-.533	-.529	-.517	-.498	-.482	-.459	-.493	-.495	-.508	-.528	-.530	-.526	-.535	-.509	-.475							
	.800	-.256	-.395	-.334	-.351	-.368	-.373	-.374	-.367	-.372	-.380	-.376	-.368	-.371	-.378	-.370	-.375	-.349	-.316	-.286							
	.900	-.162	-.086	-.096	-.107	-.125	-.139	-.146	-.150	-.164	-.177	-.169	-.157	-.148	-.146	-.132	-.114	-.106	-.089	-.097							
	.950	-.122	-.017	-.004	.015	.023	.028	.029	.034	.026	.015	.021	.021	.032	.030	.024	.029	.022	.008	-.007	-.030						
Lower surface	.0375	.767	.700	.601	.468	.304	.112	-.120	-.357	-.548	-.702	-.822	-.984	-.1242	-.242	.014	.201	.369	.511	.650	.742						
	.075	.633	.569	.482	.372	.242	.104	-.066	-.229	-.458	-.636	-.749	-.823	-.948	-.1031	.169	.297	.406	.523	.608							
	.150	.499	.447	.376	.293	.201	.095	-.014	-.121	-.236	-.474	-.306	-.178	-.068	.044	.145	.238	.319	.411	.478							
	.250	.415	.366	.308	.241	.168	.095	.013	-.064	-.145	-.231	-.169	-.106	-.024	.057	.130	.200	.261	.335	.392							
	.350	.323	.291	.234	.179	.120	.066	.001	-.059	-.119	-.157	-.132	-.091	.030	.032	.091	.145	.195	.258	.313							
	.450	.245	.220	.159	.118	.071	.024	-.025	-.072	-.114	-.131	-.125	-.097	.049	.002	.044	.091	.130	.182	.240							
	.550	.205	.190	.159	.125	.084	.049	.007	-.026	-.063	-.078	-.070	-.047	.011	.026	.068	.104	.134	.177	.207							
	.650	.144	.140	.113	.088	.059	.031	.001	-.026	-.048	-.056	-.054	-.039	.016	.011	.044	.072	.096	.129	.150							
	.750	.112	.119	.104	.088	.067	.049	.026	.011	-.004	-.006	-.006	.003	.017	.034	.059	.079	.094	.116	.128							
	.850	.084	.111	.104	.097	.084	.079	.068	.063	.052	.050	.050	.057	.061	.070	.084	.095	.097	.108	.112							
	.925	.080	.125	.126	.129	.129	.132	.125	.127	.115	.109	.114	.115	.124	.122	.132	.133	.130	.127	.124							
	.975	.132	.163	.182	.197	.203	.218	.230	.239	.241	.239	.238	.241	.234	.220	.213	.205	.192	.173	.175							
	1.000	.235	.191	.189	.241	.249	.283	.322	.327	.356	.375	.331	.499	.330	.300	.268	.269	.232	.215	.215							

No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $N = 1500$ rpm.

J	1.962	2.051	2.130	2.212	2.315	2.388	2.475	2.595	2.528	2.436	2.341	2.267	2.173	2.096	2.013
M _x	.667	.680	.696	.709	.728	.740	.756	.777	.765	.746	.731	.715	.700	.687	.671
α _x	5.26	4.00	2.91	1.83	.53	-.36	-1.38	-2.72	-1.98	-.93	.21	1.13	2.34	3.37	4.52
Δθ	.95	.74	.56	.38	.12	-.05	-.25	-.59	-.39	-.15	.06	.24	.46	.63	.83
α ₁	2.51	2.17	1.80	1.46	1.14	.84	.49	-.07	.31	.69	1.00	1.27	1.59	1.92	2.26
c _n	.9032	.7794	.6510	.5274	.4132	.3068	.1800	-.0245	.1116	.2526	.3639	.4600	.5735	.6929	.8129
c _m	-.0705	-.0898	-.0991	-.1023	-.1042	-.1074	-.1144	-.1332	-.1183	-.1095	-.1057	-.1016	-.1012	-.0928	-.0867
c _c															
c/b	Pressure coefficient, P														
Upper surface	0.000	1.116	1.121	1.128	1.133	1.140	1.145	1.152	1.160	1.155	1.148	1.141	1.135	1.129	1.124
	.025	-1.418	-.817	-.458	-.135	.146	.334	.499	.643	.772	.829	.826	.811	-.284	-.625
	.050	-1.397	-1.159	-.830	-.515	-.241	-.039	.120	.287	.203	.042	-.161	-.372	-.654	-.994
	.100	-1.157	-.938	-.750	-.545	-.345	-.205	-.059	.089	.014	-.125	-.288	-.443	-.644	-.852
	.200	-1.102	-.972	-.783	-.590	-.450	-.335	-.236	-.118	-.176	-.291	-.413	-.523	-.647	-.778
	.300	-.848	-.787	-.713	-.632	-.529	-.453	-.361	-.257	-.308	-.403	-.497	-.580	-.672	-.740
	.400	-.760	-.720	-.673	-.624	-.555	-.503	-.437	-.348	-.397	-.467	-.534	-.590	-.650	-.694
	.500	-.706	-.686	-.662	-.635	-.590	-.562	-.518	-.453	-.487	-.536	-.576	-.611	-.648	-.670
	.600	-.623	-.616	-.605	-.594	-.568	-.559	-.541	-.509	-.525	-.547	-.564	-.579	-.600	-.607
	.700	-.548	-.557	-.560	-.567	-.558	-.566	-.568	-.552	-.578	-.568	-.564	-.562	-.566	-.555
.800	-.438	-.452	-.459	-.470	-.468	-.474	-.474	-.461	-.481	-.476	-.472	-.469	-.468	-.468	-.468
.900	-.093	-.098	-.103	-.111	-.108	-.113	-.120	-.119	-.119	-.116	-.111	-.111	-.110	-.098	-.093
.950	.004	.009	.020	.025	.040	.041	.043	.047	.048	.044	.039	.033	.021	.018	.008
Lower surface	0.0375	.513	.378	.238	.064	-.133	-.318	-1.031	-1.541	-1.447	-.424	-.216	-.031	.150	.314
	.075	.413	.306	.197	.066	-.072	-.206	-.315	-1.396	-.744	-.265	-.127	0	.131	.255
	.150	.327	.244	.166	.072	-.014	-.102	-.188	-.536	-.220	-.155	-.050	.031	.117	.208
	.250	.246	.209	.153	.083	.022	-.038	-.119	-.173	-.100	-.027	.036	.099	.167	.227
	.350	.205	.150	.104	.049	.001	-.050	-.109	-.125	-.127	-.078	-.020	.025	.075	.131
	.450	.126	.082	.044	0	-.032	-.074	-.120	-.139	-.138	-.097	-.054	-.016	.019	.066
	.550	.140	.103	.073	.033	.007	-.027	-.063	-.087	-.075	-.044	-.009	.021	.089	.121
	.650	.099	.070	.047	.015	-.004	-.029	-.056	-.073	-.064	-.040	-.017	.007	.028	.060
	.750	.096	.076	.060	.036	.026	.008	-.010	-.021	-.015	0	.016	.003	.044	.070
	.850	.099	.088	.078	.066	.063	.053	.044	.038	.042	.054	.058	.064	.072	.086
.925	.127	.124	.123	.116	.121	.114	.110	.107	.111	.114	.116	.119	.118	.095	
.975	.180	.186	.195	.197	.211	.219	.231	.236	.231	.231	.222	.214	.195	.194	
1.000	.235	.232	.240	.262	.275	.300	.320	.320	.338	.325	.298	.266	.248	.297	.250

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta = 45^\circ$; $B = 2$) - Continued
0.75B(d) $N = 1600$ rpm.

	2.071	2.144	2.212	2.290	2.370	2.450	2.536	2.480	2.418	2.329	2.259	2.183	2.100
J	.789	.745	.756	.771	.787	.804	.821	.809	.796	.777	.763	.748	.736
M_{∞}	3.72	2.73	1.83	.84	-.14	-1.09	-2.07	-1.44	-.71	.36	1.23	2.21	3.32
$\Delta\theta$.71	.53	.35	.14	-.09	-.35	-.65	-.47	-.24	.03	.23	.43	.64
α_1	2.09	1.76	1.52	1.22	.93	.47	0	.27	.68	1.06	1.33	1.62	1.93
c_n	.7548	.6348	.5484	.4445	.3368	.1710	-.0013	.0968	.2484	.3845	.4839	.5839	.6961
c_m	-.0967	-.1006	-.1067	-.1111	-.1139	-.1247	-.1308	-.1250	-.1185	-.1119	-.1080	-.1032	-.0977
c_c						.0226	.0285	.0244					
c/b	Pressure coefficient, P												
Upper surface													
a.000	1.141	1.147	1.152	1.158	1.165	1.172	1.180	1.174	1.168	1.160	1.154	1.148	1.143
.025	-.584	-.278	-.044	.186	.383	.528	.625	.574	.466	.291	.092	-.138	-.435
.050	-.948	-.705	-.454	-.218	-.013	.151	.268	.206	.081	-.110	-.311	-.549	-.855
.100	-.990	-.693	-.517	-.337	-.173	-.030	.077	.019	-.091	-.252	-.410	-.592	-.791
b.200	-.957	-.742	-.622	-.490	-.349	-.221	-.128	-.189	-.278	-.405	-.543	-.672	-.820
.300	-.878	-.767	-.693	-.584	-.473	-.366	-.275	-.325	-.410	-.524	-.629	-.727	-.835
.400	-.765	-.729	-.674	-.607	-.532	-.449	-.370	-.416	-.484	-.568	-.637	-.701	-.759
.500	-.742	-.737	-.715	-.671	-.613	-.552	-.487	-.527	-.580	-.643	-.694	-.729	-.749
.600	-.630	-.649	-.703	-.766	-.745	-.687	-.613	-.657	-.712	-.756	-.730	-.673	-.643
.700	-.549	-.566	-.580	-.599	-.688	-.760	-.719	-.749	-.720	-.619	-.590	-.579	-.563
.800	-.320	-.332	-.341	-.341	-.341	-.338	-.351	-.344	-.338	-.342	-.344	-.340	-.332
.900	-.070	-.073	-.076	-.073	-.073	-.073	-.065	-.073	-.071	-.073	-.077	-.078	-.076
.950	-.022	.026	.027	.034	.036	.039	.044	.040	.042	.037	.031	.024	.021
Lower surface													
a.375	.347	.193	.046	-.142	-.315	-.496	-.634	-.786	-.988	-.127	-.061	.108	.272
.075	.286	.167	.054	-.075	-.225	-.399	-.559	-.719	-.856	-.153	-.023	.102	.226
.150	.234	.147	.070	-.015	-.120	-.275	-.433	-.593	-.756	-.065	.022	.101	.191
b.250	.183	.124	.075	-.003	-.083	-.132	-.250	-.364	-.480	-.039	.030	.080	.166
.350	.153	.100	.052	.002	-.061	-.118	-.118	-.128	-.091	-.027	.020	.069	.124
.450	.085	.042	.004	-.034	-.084	-.136	-.138	-.145	-.110	-.058	-.021	.015	.061
.550	.108	.071	.037	.005	-.011	-.075	-.090	-.087	-.053	-.016	.016	.048	.087
.650	.075	.044	.019	-.007	-.013	-.069	-.082	-.081	-.053	-.024	.001	.025	.057
.750	.083	.060	.041	.023	0	-.021	-.029	-.029	-.008	.012	.028	.044	.068
.850	.096	.083	.071	.062	.049	.034	.029	.028	.044	.054	.063	.070	.087
.925	.134	.128	.121	.119	.109	.101	.100	.097	.107	.115	.116	.120	.128
.975	.189	.194	.197	.203	.205	.223	.233	.224	.215	.206	.199	.193	.189
a1.000	.230	.240	.240	.260	.270	.340	.330	.320	.310	.265	.260	.250	.250

aNo orifice.

bPaired value.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($\alpha = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $M = 0.56$.

	J	2.116	2.156	2.179	2.206	2.241	2.276	2.304	2.362	2.388	2.424	2.468	2.512	2.552	2.622
M_x		.818	.813	.805	.796	.791	.786	.778	.779	.772	.763	.761	.755	.750	.741
α_x		3.10	2.57	2.26	1.91	1.46	1.01	.66	-.05	-.36	-.79	-1.30	-1.80	-2.25	-3.01
$\Delta\theta$.30	.17	.12	.07	.04	.02	.01	-.06	-.11	-.18	-.27	-.34	-.38	-.43
α_1		1.77	1.69	1.57	1.50	1.34	1.23	1.13	.92	.79	.67	.52	.37	.22	.03
c_n		.6400	.6110	.5652	.5432	.4877	.4477	.4123	.3326	.2877	.2442	.1910	.1348	.0813	.0097
c_m		-.1314	-.1278	-.1236	-.1226	-.1177	-.1145	-.1129	-.1108	-.1084	-.1091	-.1096	-.1150	-.1152	-.1173
c_c		.0070	.0070	.0066											
c/p	Pressure coefficient, P														
Upper surface	θ	0.000	1.179	1.176	1.173	1.169	1.166	1.164	1.161	1.161	1.158	1.155	1.154	1.151	1.146
		.025	-.039	.012	.057	.090	.160	.206	.259	.363	.415	.455	.507	.550	.593
		.050	-.484	-.427	-.371	-.335	-.257	-.206	-.148	-.037	.021	.064	.125	.172	.225
		.100	-.509	-.486	-.454	-.429	-.367	-.281	-.188	-.139	-.105	-.050	-.011	.035	.103
		.200	-.599	-.581	-.574	-.568	-.512	-.477	-.437	-.359	-.319	-.288	-.239	-.205	-.165
		.300	-.682	-.653	-.640	-.631	-.604	-.592	-.557	-.483	-.441	-.413	-.364	-.331	-.296
		.400	-.762	-.729	-.695	-.671	-.628	-.598	-.583	-.534	-.499	-.473	-.428	-.401	-.368
		.500	-.815	-.794	-.777	-.769	-.726	-.694	-.659	-.620	-.586	-.555	-.507	-.481	-.448
		.600	-.931	-.910	-.889	-.865	-.793	-.787	-.771	-.674	-.596	-.573	-.533	-.513	-.485
		.700	-.782	-.825	-.827	-.813	-.793	-.696	-.623	-.602	-.599	-.592	-.565	-.556	-.508
Lower surface		.800	-.340	-.310	-.292	-.292	-.298	-.312	-.334	-.348	-.359	-.367	-.367	-.374	-.372
		.900	-.197	-.148	-.109	-.091	-.073	-.066	-.071	-.075	-.087	-.098	-.105	-.118	-.149
		.950	-.136	-.083	-.037	-.018	.002	.019	.033	.044	.050	.048	.053	.047	.034
		.0375	.145	.094	.036	-.003	-.082	-.139	-.210	-.302	-.352	-.360	-.975	-1.335	-1.722
		.075	.135	.097	.054	.024	-.032	-.070	-.119	-.201	-.235	-.252	-.293	-.439	-.634
		.150	.135	.108	.077	.056	.017	-.009	-.042	-.097	-.129	-.156	-.174	-.189	-.222
		.250	.090	.080	.060	.046	.022	.006	-.017	-.056	-.079	-.102	-.119	-.142	-.153
		.350	.085	.070	.053	.037	.016	.001	-.017	-.047	-.064	-.083	-.096	-.117	-.129
		.450	.024	.013	0	-.011	-.025	-.036	-.052	-.072	-.084	-.099	-.110	-.128	-.137
		.550	.048	.041	.031	.021	.010	.001	-.009	-.024	-.033	-.045	-.051	-.066	-.073
		.650	.013	.012	.005	-.001	-.010	-.013	-.020	-.029	-.033	-.042	-.044	-.055	-.061

*No orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(f) $M = 0.58$.

J	2.609	2.570	2.528	2.487	2.446	2.407	2.376	2.337	2.297	2.271	2.234	2.208	2.167	2.137
$M_{x'}$.768	.775	.781	.786	.792	.798	.805	.809	.813	.819	.826	.833	.838	.844
$\alpha_{x'}$	-2.87	-2.45	-1.98	-1.52	-1.04	-.58	-.21	.26	.75	1.08	1.55	1.88	2.42	2.82
$\Delta\theta$	-.64	-.55	-.45	-.38	-.31	-.27	-.26	-.23	-.16	-.09	.03	.12	.25	.35
α_1	-.11	-.01	.15	.30	.46	.58	.72	.86	.99	1.10	1.22	1.35	1.48	1.52
α_n	-.0394	-.0026	.0529	.1090	.1677	.2103	.2519	.3135	.3600	.3974	.4394	.4858	.5342	.5471
α_m	-.1163	-.1177	-.1154	-.1124	-.1121	-.1134	-.1108	-.1082	-.1075	-.1119	-.1173	-.1214	-.1272	-.1377
α_c							.0174	.0162	.0143	.0136	.0142	.0148	.0145	.0138
c/b	Pressure coefficient, P													
Upper surface	0.000	1.157	1.160	1.162	1.164	1.167	1.169	1.172	1.175	1.177	1.179	1.182	1.185	1.188
	.025	.654	.621	.588	.552	.507	.462	.421	.373	.321	.275	.233	.200	.125
	.050	.254	.216	.175	.130	.076	.022	-.145	-.085	-.201	-.249	-.285	-.389	-.444
	.100	.116	.083	.051	.014	-.029	-.071	-.108	-.153	-.197	-.234	-.267	-.293	-.349
	.200	-.097	-.126	-.156	-.189	-.229	-.267	-.299	-.338	-.376	-.412	-.449	-.476	-.522
	.300	-.225	-.254	-.280	-.312	-.348	-.384	-.415	-.453	-.490	-.507	-.525	-.540	-.593
	.400	-.319	-.346	-.373	-.402	-.437	-.467	-.489	-.506	-.519	-.533	-.569	-.598	-.633
	.500	-.409	-.436	-.466	-.497	-.537	-.553	-.576	-.609	-.629	-.650	-.670	-.680	-.713
	.600	-.463	-.488	-.516	-.546	-.614	-.687	-.712	-.715	-.741	-.743	-.785	-.801	-.848
	.700	-.462	-.471	-.484	-.505	-.530	-.579	-.619	-.633	-.642	-.632	-.691	-.709	-.710
	.800	-.365	-.361	-.357	-.347	-.342	-.327	-.308	-.300	-.299	-.313	-.341	-.359	-.366
Lower surface	.900	-.136	-.122	-.111	-.097	-.089	-.077	-.072	-.076	-.085	-.110	-.154	-.203	-.247
	.950	.046	.052	.055	.058	.052	.048	.036	.015	-.006	-.038	-.089	-.143	-.201
	.0375	-1.582	-1.460	-1.377	-1.306	-1.213	-1.066	-.740	-.420	-.309	-.222	-.164	-.106	-.022
	.075	-1.160	-1.144	-1.013	-.756	-.547	-.359	-.269	-.217	-.156	-.104	-.065	-.023	.036
	.150	-.505	-.423	-.358	-.263	-.213	-.162	-.137	-.104	-.062	-.026	-.001	.030	.067
	.250	-.305	-.235	-.204	-.162	-.142	-.114	-.092	-.063	-.032	-.004	.013	.035	.064
	.350	-.203	-.167	-.149	-.124	-.112	-.096	-.079	-.058	-.034	-.016	-.003	.015	.038
	.450	-.156	-.142	-.133	-.120	-.113	-.103	-.091	-.075	-.059	-.045	-.041	-.024	-.008
	.550	-.088	-.083	-.079	-.070	-.068	-.060	-.053	-.042	-.028	-.017	-.014	-.003	.007
	.650	-.063	-.064	-.063	-.057	-.058	-.055	-.052	-.046	-.038	-.031	-.031	-.026	-.020
	.750	-.010	-.011	-.012	-.008	-.012	-.012	-.012	-.011	-.006	-.002	-.008	-.007	-.008
	.850	.048	.047	.045	.047	.042	.040	.036	.034	.033	.031	.021	.017	.006
	.925	.112	.112	.110	.112	.106	.104	.098	.092	.088	.081	.065	.054	.035
	.975	.210	.210	.206	.207	.199	.195	.189	.187	.185	.184	.174	.173	.160
	1.000	.270	.270	.250	.250	.250	.250	.240	.250	.260	.255	.250	.265	.298

^aNo orifice.^bPaired value.

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $M = 0.60$.

	2.553	2.528	2.489	2.460	2.419	2.377	2.338	2.311	2.281	2.246	2.220	2.197	2.164	2.128	2.106
x	2.553	2.528	2.489	2.460	2.419	2.377	2.338	2.311	2.281	2.246	2.220	2.197	2.164	2.128	2.106
M_x	.796	.806	.811	.820	.826	.828	.830	.839	.849	.851	.856	.863	.870	.869	.873
α_x	-2.26	-1.98	-1.54	-1.20	-.73	-.23	.25	.58	.95	1.40	1.73	2.03	2.46	2.94	3.24
$\Delta\theta$	-.66	-.63	-.57	-.53	-.46	-.38	-.31	-.24	-.17	-.10	-.05	-.02	0	.04	.07
c_l	-.14	-.03	.11	.21	.32	.49	.59	.70	.82	.95	1.03	1.14	1.24	1.31	1.39
c_{D1}	-.0497	-.0103	.0406	.0768	.1174	.1774	.2155	.2535	.2955	.3439	.3710	.4097	.4465	.4735	.4994
c_{D2}	-.1132	-.1091	-.1118	-.1080	-.1091	-.1078	-.1096	-.1114	-.1108	-.1118	-.1118	-.1137	-.1147	-.1200	-.1249
c_c		.0241	.0233	.0222	.0247	.0204	.0210	.0216	.0220	.0212	.0208	.0210	.0211	.0208	.0203
c/b	Pressure coefficient, P														
Upper surface	0.000	1.169	1.173	1.175	1.180	1.182	1.183	1.184	1.188	1.193	1.194	1.196	1.200	1.203	1.205
	.025	.635	.607	.578	.554	.520	.474	.446	.417	.389	.337	.298	.261	.223	.184
	.050	.231	.199	.163	.134	.092	.036	-.001	-.034	-.070	-.132	-.177	-.225	-.278	-.320
	.100	.099	.073	.044	.022	-.012	-.055	-.083	-.107	-.132	-.177	-.209	-.237	-.267	-.296
	.200	-.117	-.138	-.166	-.184	-.213	-.252	-.279	-.298	-.322	-.367	-.404	-.419	-.429	-.438
	.300	-.249	-.268	-.295	-.311	-.339	-.374	-.403	-.421	-.429	-.458	-.477	-.487	-.509	-.528
	.400	-.350	-.368	-.392	-.406	-.427	-.446	-.452	-.460	-.482	-.513	-.540	-.559	-.573	-.599
	.500	-.455	-.475	-.498	-.501	-.522	-.553	-.570	-.575	-.587	-.611	-.627	-.642	-.658	-.674
	.600	-.529	-.566	-.625	-.644	-.663	-.670	-.697	-.690	-.697	-.737	-.746	-.775	-.774	-.790
	.700	-.558	-.575	-.628	-.663	-.690	-.725	-.732	-.738	-.752	-.774	-.786	-.804	-.823	-.829
	.800	-.550	-.540	-.533	-.516	-.520	-.523	-.544	-.556	-.561	-.556	-.552	-.554	-.572	-.591
Lower surface	.900	-.502	-.509	-.500	-.507	-.505	-.502	-.518	-.512	-.514	-.524	-.527	-.529	-.535	-.548
	.950	.053	.053	.047	.038	0	-.028	-.074	-.119	-.176	-.214	-.255	-.286	-.322	-.346
	.0375	-1.404	-1.327	-1.272	-1.223	-1.163	-1.106	-1.039	-.850	-.563	-.304	-.244	-.188	-.138	-.079
	.075	-1.336	-1.256	-1.181	-1.110	-.997	-.927	-.838	-.635	-.202	-.161	-.130	-.075	-.015	.014
	.150	-.888	-.684	-.539	-.368	-.239	-.173	-.156	-.127	-.095	-.058	-.040	0	.037	.060
	.250	-.217	-.170	-.145	-.133	-.129	-.113	-.099	-.076	-.055	-.028	-.013	.014	.040	.066
	.350	-.132	-.131	-.133	-.129	-.122	-.102	-.093	-.074	-.058	-.040	-.029	-.007	.018	.027
	.450	-.147	-.143	-.145	-.140	-.135	-.120	-.114	-.098	-.083	-.072	-.066	-.048	-.024	-.022
	.550	-.098	-.094	-.096	-.091	-.089	-.076	-.074	-.063	-.056	-.047	-.046	-.034	-.018	-.015
	.650	-.082	-.081	-.085	-.083	-.084	-.076	-.080	-.073	-.070	-.067	-.070	-.062	-.053	-.053
	.750	-.028	-.027	-.032	-.032	-.038	-.035	-.042	-.041	-.043	-.045	-.054	-.050	-.048	-.050
	.850	.031	.032	.026	.024	.014	.011	-.001	-.006	-.015	-.024	-.037	-.040	-.045	-.044
	.925	.101	.101	.095	.091	.077	.069	.052	.042	.025	.010	-.008	-.016	-.024	-.030
	.975	.199	.197	.193	.192	.185	.182	.175	.172	.163	.150	.133	.114	.086	.060
	1.000	.280	.265	.253	.270	.270	.270	.270	.288	.280	.278	.260	.263	.178	.140

^a% orifice.

NACA

TABLE 5.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-506.62 PROPELLER BLADE SECTION ($x = 0.70$; $\beta_x = 47.00^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

	J	2.124	2.152	2.183	2.219	2.259	2.286	2.326	2.364	2.397	2.434	2.456	2.098
M_x		.943	.932	.922	.917	.911	.903	.896	.889	.879	.874	.867	.948
α_x		3.00	2.62	2.21	1.74	1.23	.89	.39	-.07	-.47	-.90	-1.16	3.35
$\Delta\theta$		-.25	-.29	-.34	-.40	-.46	-.50	-.56	-.61	-.66	-.71	-.75	-.21
α_1		1.18	1.08	.93	.80	.67	.57	.42	.26	.12	.01	-.05	1.27
c_n		.4232	.3897	.3348	.2890	.2419	.2065	.1503	.0929	.0452	.0026	-.0181	.4574
c_m		-.1608	-.1576	-.1522	-.1501	-.1413	-.1360	-.1295	-.1254	-.1224	-.1222	-.1222	-.1593
c_c		.0428	.0434	.0426	.0418	.0406	.0388	.0381	.0366	.0358	.0347	.0335	.0420
c/b	Pressure coefficient, P												
Upper surface	a ^{0.000}	1.242	1.236	1.231	1.228	1.225	1.221	1.217	1.213	1.208	1.205	1.202	1.245
	.025	.410	.419	.453	.470	.495	.518	.552	.572	.587	.608	.627	.363
	.050	-.001	.011	.053	.077	.106	.130	.173	.206	.225	.248	.270	-.037
	.100	-.133	-.128	-.095	-.077	-.052	-.031	.005	.034	.047	.068	.085	-.156
	.200	-.299	-.294	-.281	-.273	-.246	-.221	-.187	-.163	-.152	-.133	-.116	-.297
	.300	-.352	-.356	-.342	-.337	-.328	-.322	-.318	-.310	-.305	-.285	-.270	-.363
	.400	-.448	-.450	-.435	-.426	-.412	-.394	-.366	-.344	-.346	-.341	-.340	-.462
	.500	-.522	-.533	-.523	-.518	-.507	-.494	-.478	-.466	-.474	-.461	-.456	-.524
	.600	-.637	-.650	-.641	-.637	-.627	-.626	-.596	-.597	-.604	-.594	-.588	-.635
	.700	-.749	-.762	-.752	-.748	-.739	-.731	-.735	-.733	-.744	-.729	-.720	-.742
	.800	-.849	-.863	-.863	-.859	-.823	-.705	-.621	-.520	-.442	-.386	-.376	-.839
Lower surface	.900	-.473	-.466	-.416	-.378	-.337	-.301	-.279	-.255	-.233	-.199	-.176	-.467
	.950	-.444	-.440	-.397	-.364	-.326	-.292	-.271	-.245	-.220	-.176	-.143	-.441
	.0375	-.157	-.235	-.455	-.568	-.653	-.737	-.829	-.890	-.969	-1.021	-1.077	-.068
	.075	-.066	-.121	-.231	-.371	-.520	-.622	-.720	-.786	-.863	-.910	-.963	-.008
	.150	.013	-.027	-.075	-.093	-.130	-.248	-.561	-.675	-.760	-.808	-.862	.056
	.250	.024	-.012	-.052	-.073	-.087	-.102	-.135	-.178	-.347	-.465	-.588	.058
	.350	.001	-.033	-.071	-.091	-.107	-.120	-.131	-.130	-.154	-.157	-.176	.031
	.450	-.054	-.087	-.123	-.140	-.153	-.163	-.174	-.172	-.183	-.167	-.161	-.030
	.550	-.031	-.063	-.091	-.106	-.116	-.122	-.134	-.133	-.148	-.135	-.126	-.009
	.650	-.076	-.107	-.130	-.142	-.145	-.143	-.151	-.150	-.161	-.143	-.129	-.056
	.750	-.060	-.087	-.104	-.110	-.111	-.108	-.113	-.109	-.114	-.096	-.083	-.043
	.850	-.035	-.057	-.070	-.076	-.077	-.074	-.078	-.071	-.072	-.052	-.038	-.018
	.925	.012	-.008	-.021	-.029	-.031	-.033	-.036	-.029	-.026	-.002	.014	.031
	.975	-.099	-.103	-.088	-.065	-.032	.012	.044	.084	.113	.151	.168	-.095
	a ^{1.000}	-.264	-.239	-.175	-.108	-.060	.101	.120	.195	.285	.290	.303	-.308

^aNo orifice.^bPaired value.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.05 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.78} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	J	M_x	α_x	$\Delta\delta$	c_l	c_m	c_c													
	1.606	1.689	1.816	1.928	2.052	2.169	2.300	2.423	2.549	2.649	2.601	2.492	2.367	2.258	2.106	1.982	1.876	1.774	1.652	
	.503	.509	.524	.534	.551	.566	.579	.593	.608	.624	.616	.600	.586	.573	.559	.544	.528	.520	.506	
	10.66	9.32	7.36	5.70	3.96	2.39	.71	-.78	-2.23	-3.33	-2.81	-1.58	-.11	1.24	3.22	4.93	6.46	8.00	9.91	
	.94	.85	.72	.59	.46	.33	.16	-.02	-.20	-.36	-.28	-.12	.06	.22	.41	.54	.65	.76	.89	
	3.11	3.05	2.77	2.35	1.99	1.57	1.15	.72	.31	-.01	.15	.54	.92	1.29	1.77	2.20	2.52	2.88	3.09	
	.9058	.9671	.8781	.7503	.6387	.5023	.3703	.2313	.0994	-.0019	.0471	.1761	.2965	.4158	.5658	.7039	.8026	.9123	.9755	
	-.0539	-.0542	-.0718	-.0831	-.0893	-.0932	-.0918	-.0919	-.0983	-.1031	-.1009	-.0932	-.0931	-.0921	-.0910	-.0846	-.0783	-.0674	-.0518	
c/b	Pressure coefficient, P																			
Upper surface	0.000	1.065	1.066	1.070	1.073	1.078	1.082	1.086	1.091	1.095	1.101	1.098	1.093	1.088	1.084	1.079	1.076	1.071	1.069	
	.025	-1.841	-2.126	-2.290	-1.161	-.788	-.345	.027	.328	.507	.605	.558	.424	.198	-.093	-.567	-1.005	-1.600	-2.285	
	.050	-1.846	-2.078	-1.655	-1.085	-.765	-.462	-.187	.054	.227	.325	.275	.147	-.055	-.279	-.613	-.934	-1.201	-2.026	
	.100	-1.780	-1.708	-1.085	-.903	-.696	-.490	-.295	-.120	.017	.101	.058	-.047	-.197	-.362	-.592	-.806	-.982	-1.327	
	.200	-1.153	-1.013	-.804	-.722	-.605	-.488	-.358	-.239	-.132	.070	-.103	-.181	-.291	-.403	-.547	-.669	-.751	-.791	
	.300	-.937	-.753	-.719	-.661	-.578	-.488	-.393	-.304	-.220	-.168	-.197	-.261	-.343	-.424	-.526	-.624	-.692	-.724	
	.400	-.682	-.620	-.626	-.583	-.520	-.454	-.380	-.315	-.247	-.208	-.229	-.279	-.343	-.405	-.483	-.555	-.605	-.630	
	.500	-.543	-.557	-.585	-.565	-.528	-.480	-.424	-.380	-.323	-.296	-.312	-.348	-.395	-.442	-.500	-.551	-.576	-.584	
	.600	-.432	-.469	-.508	-.504	-.480	-.450	-.408	-.380	-.338	-.318	-.330	-.395	-.388	-.422	-.463	-.495	-.510	-.502	
	.700	-.344	-.394	-.445	-.456	-.432	-.438	-.408	-.395	-.366	-.354	-.363	-.377	-.397	-.418	-.442	-.459	-.452	-.431	
	.800	-.261	-.285	-.327	-.352	-.362	-.365	-.351	-.350	-.334	-.333	-.337	-.339	-.346	-.354	-.360	-.360	-.337	-.314	
Lower surface	.900	-.172	-.141	-.131	-.133	-.151	-.164	-.162	-.172	-.167	-.175	-.174	-.167	-.161	-.160	-.154	-.146	-.129	-.131	
	.950	-.138	-.077	-.031	-.018	-.013	-.019	-.015	-.026	-.025	-.034	-.033	-.024	-.017	-.015	-.012	-.015	-.022	-.039	
	.0375	.744	.712	.638	.527	.377	.184	-.029	-.295	-.902	-1.074	-1.076	-.544	-.159	.032	.293	.459	.585	.667	
	.075	.618	.585	.518	.423	.300	.154	.006	-.180	-.460	-.790	-.679	-.254	-.080	.060	.235	.366	.470	.545	
	.150	.492	.462	.407	.333	.245	.142	.051	-.078	-.185	-.474	-.309	-.123	-.010	.083	.200	.291	.368	.431	
	.250	.399	.370	.330	.248	.186	.116	.045	-.048	-.107	-.194	-.132	-.078	0	.071	.172	.239	.286	.327	
	.350	.334	.313	.279	.231	.176	.116	.060	-.013	-.095	-.096	-.075	-.034	.028	.079	.151	.206	.255	.296	
	.450	.263	.249	.222	.181	.138	.090	.045	-.013	-.041	-.064	-.057	-.027	.020	.062	.118	.161	.204	.236	
	.550	.227	.221	.202	.168	.132	.092	.054	.011	-.011	-.029	-.024	.002	.036	.069	.116	.148	.182	.213	
	.650	.152	.155	.147	.120	.092	.062	.037	-.002	-.011	-.021	-.021	-.005	.020	.048	.081	.105	.133	.156	
	.750	.122	.131	.132	.111	.092	.070	.054	.028	.021	.014	.014	.025	.043	.062	.085	.103	.120	.137	
	.850	.096	.114	.127	.117	.109	.100	.089	.070	.067	.060	.062	.071	.083	.093	.107	.114	.120	.131	
	.925	.064	.095	.123	.120	.124	.122	.120	.108	.108	.100	.100	.111	.119	.122	.126	.120	.121	.109	
	b.975	.040	.081	.128	.126	.150	.138	.144	.142	.140	.125	.050	.140	.146	.143	.142	.128	.125	.116	
	a1.000	.025	.074	.130	.128	.164	.148	.157	.161	.155	.140	.130	.155	.160	.155	.150	.138	.128	.110	

No orifice.

b Paired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($x = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

	J	1.793	1.890	1.988	2.130	2.272	2.420	2.567	2.634	2.606	2.490	2.367	2.223	2.087	1.945	1.837
M_x		.630	.640	.652	.674	.696	.717	.740	.750	.744	.727	.705	.685	.665	.645	.632
α_x		7.71	6.26	4.85	2.90	1.06	-.74	-2.43	-3.17	-2.86	-1.56	-.11	1.69	3.48	5.46	7.04
$\Delta\theta$		1.12	.92	.71	.43	.16	-.13	-.46	-.62	-.55	-.27	-.03	.26	.51	.80	1.03
α_1		3.14	2.70	2.35	1.85	1.38	.80	.28	0	.07	.60	1.02	1.54	2.04	2.51	2.98
c_D		.9961	.8619	.7523	.5939	.4439	.2594	.0903	.0013	.0219	.1932	.3287	.4942	.6535	.8013	.9497
c_m		-.0688	-.0816	-.0906	-.0991	-.1023	-.1048	-.1150	-.1180	-.1219	-.1045	-.1031	-.0986	-.0967	-.0928	-.0777
c_c																
c/b	Pressure coefficient, P															
Upper surface	0.000	1.103	1.106	1.111	1.120	1.128	1.136	1.145	1.149	1.147	1.140	1.131	1.123	1.113	1.108	1.103
	.025	-.2537	-.2084	-.1227	-.488	-.041	.356	.574	.643	.609	.471	.231	-.220	-.733	-.1593	-.2374
	.050	-.2368	-.1864	-.1091	-.561	-.223	.103	.311	.380	.349	.209	-.005	-.371	-.748	-.1289	-.2181
	.100	-.2164	-.1008	-.919	-.584	-.350	-.094	.088	.153	.125	-.005	-.182	-.468	-.721	-.990	-.1803
	.200	-.687	-.728	-.712	-.556	-.421	-.245	-.103	-.048	-.073	-.173	-.307	-.503	-.631	-.736	-.720
	.300	-.746	-.748	-.689	-.547	-.460	-.332	-.221	-.174	-.194	-.274	-.376	-.529	-.618	-.719	-.756
	.400	-.656	-.654	-.615	-.508	-.451	-.361	-.275	-.238	-.254	-.316	-.392	-.511	-.567	-.635	-.660
	.500	-.622	-.624	-.599	-.522	-.494	-.433	-.371	-.346	-.357	-.400	-.452	-.546	-.571	-.610	-.625
	.600	-.536	-.541	-.531	-.475	-.470	-.435	-.398	-.384	-.392	-.414	-.446	-.514	-.518	-.537	-.537
	.700	-.465	-.480	-.485	-.452	-.466	-.453	-.447	-.447	-.446	-.445	-.455	-.502	-.485	-.484	-.478
	.800	-.328	-.340	-.358	-.340	-.370	-.373	-.382	-.388	-.385	-.372	-.372	-.403	-.371	-.354	-.332
	.900	-.106	-.103	-.117	-.100	-.136	-.145	-.161	-.170	-.166	-.148	-.143	-.168	-.130	-.111	-.102
	.950	-.003	.001	.005	.040	.013	.010	0	-.009	-.006	.009	.010	-.021	.005	.005	.001
Lower surface	.0375	.698	.605	.485	.299	.025	-.315	-1.370	-1.125	-1.722	-.657	-.190	.075	.349	.547	.697
	.075	.576	.495	.393	.254	.053	-.189	-.652	-.970	-.935	-.336	-.103	.079	.283	.443	.541
	.150	.470	.407	.329	.238	.090	-.071	-.267	-.656	-.554	-.134	-.013	.099	.251	.367	.441
	.250	.308	.238	.215	.192	.072	-.043	-.138	-.343	-.223	-.086	-.002	.067	.177	.231	.276
	.350	.323	.280	.227	.182	.084	-.003	-.073	-.137	-.096	-.039	.027	.075	.175	.252	.303
	.450	.267	.228	.184	.151	.066	-.003	-.053	-.067	-.055	-.028	.021	.052	.141	.205	.248
	.550	.239	.208	.168	.151	.075	.021	-.019	-.024	-.020	.003	.039	.058	.134	.188	.226
	.650	.183	.154	.123	.114	.048	.010	-.016	-.011	-.012	-.003	.021	.029	.093	.138	.172
	.750	.164	.141	.118	.120	.068	.039	.023	.027	.025	.031	.048	.041	.096	.130	.153
	.850	.158	.143	.129	.145	.103	.087	.075	.072	.072	.081	.091	.073	.117	.137	.151
	.925	.152	.141	.136	.164	.133	.124	.115	.107	.108	.121	.126	.099	.131	.140	.146
	.975	.250	.246	.245	.303	.267	.252	.260	.257	.258	.257	.258	.243	.247	.272	.270
	1.000	.387	.407	.430	.458	.395	.410	.417	.460	.428	.440	.414	.380	.453	.463	.445

*No orifice.

b Paired value.



TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $N = 1500$ rpm.

J	2.003	2.100	2.169	2.305	2.409	2.505	2.582	2.547	2.470	2.359	2.252	2.148	2.063	
M _x	.721	.736	.747	.768	.787	.802	.815	.808	.793	.774	.757	.737	.725	
α _x	4.64	3.30	2.39	.65	-.61	-1.73	-2.60	-2.21	-1.33	-.01	1.32	2.66	3.81	
Δh	.96	.67	.46	.02	-.27	-.56	-.82	-.70	-.45	-.13	.20	.53	.78	
c ₁	2.40	2.10	1.81	1.28	.87	.34	-.02	.13	.55	1.06	1.46	1.91	2.24	
c _n	.7671	.6742	.5819	.4126	.2803	.1084	-.0065	.0439	.1781	.3406	.4710	.6135	.7174	
c _m	-.0975	-.1037	-.1071	-.1154	-.1200	-.1324	-.1362	-.1331	-.1268	-.1147	-.1143	-.1064	-.0968	
c _c						.0265	.0298	.0287						
c/b	Pressure coefficient, P													
Upper surface	0.000	1.137	1.143	1.148	1.157	1.165	1.171	1.177	1.173	1.167	1.159	1.152	1.144	1.139
	.025	-.948	-.903	-.866	-.829	-.792	-.757	-.722	-.688	-.653	-.619	-.585	-.551	-.517
	.050	-1.003	-.970	-.938	-.903	-.868	-.834	-.800	-.766	-.732	-.698	-.664	-.630	-.596
	.100	-1.107	-.756	-.530	-.295	-.068	.067	.152	.117	.080	-.150	-.364	-.618	-.918
	.200	-.689	-.635	-.567	-.483	-.385	-.284	-.189	-.089	-.173	-.308	-.458	-.623	-.818
	.300	-.708	-.668	-.596	-.462	-.352	-.258	-.190	-.219	-.292	-.399	-.518	-.626	-.695
	.400	-.688	-.675	-.628	-.525	-.429	-.346	-.282	-.306	-.375	-.469	-.567	-.643	-.680
	.500	-.644	-.625	-.608	-.557	-.504	-.451	-.402	-.419	-.469	-.527	-.579	-.612	-.634
	.600	-.568	-.561	-.563	-.551	-.535	-.504	-.464	-.480	-.518	-.542	-.577	-.561	-.566
	.700	-.508	-.511	-.524	-.543	-.562	-.582	-.597	-.565	-.597	-.561	-.533	-.519	-.511
.800	-.359	-.366	-.378	-.384	-.387	-.386	-.381	-.380	-.390	-.386	-.386	-.376	-.365	
.900	-.101	-.103	-.111	-.114	-.114	-.116	-.103	-.110	-.117	-.115	-.116	-.112	-.104	
.950	.013	.020	.022	.027	.030	.031	.040	.038	.030	.031	.022	.021	.016	
Lower surface	.0375	.457	.319	.168	-.098	-.468	-1.293	-1.353	-1.351	-1.237	-.243	.013	.237	.376
	.075	.374	.265	.150	-.035	-.245	-1.181	-1.274	-1.260	-.694	-.129	.037	.201	.308
	.150	.310	.232	.154	.031	-.081	-.222	-.296	-.489	-.110	-.093	.085	.188	.262
	.250	.117	.140	.117	.029	-.047	-.079	-.225	-.103	-.079	-.010	.064	.126	.149
	.350	.225	.177	.128	.055	-.006	-.046	-.051	-.042	-.037	.022	.084	.149	.195
	.450	.180	.139	.099	.042	-.005	-.038	-.031	-.036	-.031	.017	.064	.115	.155
	.550	.168	.135	.102	.057	.022	-.007	-.004	-.006	0	.038	.072	.115	.146
	.650	.121	.097	.069	.036	.009	-.012	-.008	-.010	-.007	.021	.047	.081	.105
	.750	.117	.099	.079	.057	.039	.023	.028	.025	.028	.047	.063	.087	.105
	.850	.131	.121	.109	.098	.087	.078	.082	.080	.081	.093	.101	.115	.123
	.925	.141	.138	.133	.132	.125	.118	.123	.121	.119	.128	.130	.135	.137
	b .975	.255	.261	.245	.255	.260	.253	.270	.260	.255	.260	.242	.243	.260
	a 1.000	.380	.360	.358	.380	.393	.420	.405	.430	.405	.425	.375	.390	.440

^aNo orifice.^bReared value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($x = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $N = 1600$ rpm.

J	2.165	2.267	2.349	2.444	2.528	2.483	2.406	2.315	2.235	2.130
M_x	.796	.816	.831	.847	.864	.854	.838	.820	.804	.788
α_x	2.44	1.13	.11	-1.02	-1.99	-1.48	-.58	.53	1.53	2.90
$\Delta\delta$.54	.15	-.16	-.57	-.91	-.75	-.40	-.03	.28	.67
α_1	1.79	1.44	.99	.38	-.14	.16	.66	1.19	1.54	1.98
c_n	.5735	.4626	.3187	.1245	-.0445	.0535	.2123	.3826	.4942	.6374
c_m	-.1150	-.1265	-.1401	-.1422	-.1468	-.1475	-.1298	-.1232	-.1200	-.1167
c_c	.0021	.0137	.0243	.0328	.0385	.0343	.0258	.0192		
c/b	Pressure coefficient, P									
Upper surface	$\beta_{0.000}$	1.169	1.186	1.185	1.192	1.200	1.195	1.188	1.180	1.172
	.025	-.058	.220	.422	.565	.659	.608	.505	.342	.129
	.050	-.305	-.052	.137	.311	.390	.336	.224	.097	-.135
	.100	-.463	-.245	-.075	.069	.170	.116	.008	-.149	-.319
	.200	-.560	-.403	-.255	-.127	-.037	-.086	-.185	-.321	-.446
	.300	-.633	-.481	-.364	-.249	-.170	-.214	-.300	-.417	-.524
	.400	-.604	-.478	-.424	-.351	-.282	-.322	-.389	-.457	-.511
	.500	-.760	-.691	-.623	-.531	-.464	-.500	-.576	-.661	-.724
	.600	-.802	-.751	-.673	-.575	-.450	-.510	-.622	-.707	-.773
	.700	-.510	-.763	-.711	-.616	-.571	-.598	-.651	-.733	-.638
	.800	-.310	-.300	-.571	-.529	-.701	-.625	-.408	-.316	-.321
Lower surface	.900	-.074	-.070	-.075	-.090	-.114	-.100	-.076	-.075	-.077
	.950	.028	.024	.003	-.030	-.068	-.045	-.004	.020	.027
	.0375	.144	-.071	-.730	-1.082	-1.147	-1.121	-1.040	-.199	-.009
	.075	.136	-.013	-.132	-.922	-1.087	-1.048	-.890	-.111	.031
	.150	.149	.047	-.059	-.551	-.926	-.874	-.095	-.022	.079
	.250	.120	.047	-.038	-.073	-.811	-.213	-.060	-.005	.070
	.350	.127	.066	-.001	-.031	-.208	-.047	-.025	.025	.082
	.450	.097	.049	-.004	-.033	-.059	-.031	-.025	.015	.062
	.550	.100	.062	.014	-.003	-.007	-.006	.001	.033	.070
	.650	.065	.036	-.002	-.019	-.018	-.022	-.014	.011	.041
	.750	.078	.054	.021	.009	.007	.008	.015	.034	.059
	.850	.111	.094	.069	.056	.049	.054	.061	.078	.096
	.925	.132	.122	.099	.084	.072	.080	.093	.110	.126
	$\beta_{0.975}$.155	.155	.120	.115	.090	.100	.120	.139	.150
	$\beta_{1.000}$.165	.170	.132	.130	.105	.115	.133	.153	.162

^aNo orifice.^bPaired values.

NACA

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_T = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $M = 0.56$.

	J	2.114	2.146	2.192	2.229	2.278	2.326	2.371 ^a	2.417	2.469	2.542	2.578	2.620
M_x		.879	.868	.858	.847	.837	.828	.817	.805	.800	.789	.784	.778
$c_{x'}$		3.12	2.69	2.09	1.61	.99	.39	-.16	-.71	-1.55	-2.15	-2.56	-3.02
$\Delta\delta$.30	.17	.04	-.03	-.07	-.10	-.18	-.32	-.49	-.58	-.64	-.70
α_1		1.82	1.70	1.57	1.45	1.32	1.15	.93	.74	.45	.22	.12	-.05
c_n		.5826	.5445	.5045	.4665	.4239	.3690	.2987	.2400	.1471	.0710	.0374	-.0174
c_m		-.1434	-.1385	-.1350	-.1335	-.1309	-.1222	-.1257	-.1263	-.1273	-.1286	-.1286	-.1306
c_c		.0153	.0173	.0182	.0174	.0174	.0184	.0196	.0217	.0232			
c/b	Pressure coefficient, P												
Upper surface	θ , 0.000	1.208	1.203	1.198	1.192	1.187	1.183	1.178	1.172	1.170	1.166	1.163	1.161
	.025	.053	.098	.151	.207	.271	.338	.409	.482	.532	.590	.613	.650
	.050	-.138	-.105	-.062	-.018	.037	.095	.162	.201	.280	.337	.361	.396
	.100	-.319	-.289	-.253	-.216	-.169	-.116	-.054	-.018	.056	.110	.132	.167
	.200	-.444	-.430	-.381	-.374	-.338	-.290	-.235	-.206	-.138	-.090	-.070	-.040
	.300	-.553	-.521	-.511	-.468	-.434	-.404	-.352	-.326	-.264	-.193	-.202	-.173
	.400	-.583	-.554	-.510	-.491	-.452	-.407	-.402	-.400	-.344	-.297	-.281	-.252
	.500	-.708	-.697	-.679	-.663	-.628	-.627	-.606	-.548	-.453	-.406	-.389	-.361
	.600	-.756	-.743	-.736	-.722	-.706	-.666	-.584	-.542	-.511	-.464	-.447	-.416
	.700	-.848	-.838	-.827	-.798	-.788	-.735	-.642	-.640	-.524	-.470	-.459	-.433
	.800	-.336	-.310	-.304	-.298	-.307	-.307	-.337	-.371	-.284	-.389	-.393	-.391
Lower surface	.900	-.295	-.256	-.218	-.167	-.104	-.065	-.076	-.096	-.109	-.123	-.133	-.143
	.950	.293	-.247	-.196	-.130	-.052	.020	.043	.039	.040	.034	.025	.019
	.0375	.153	.093	.018	-.060	-.144	-.218	-.672	-1.075	-1.271	-1.430	-1.495	-1.591
	.075	.157	.112	.054	-.004	-.068	-.118	-.152	-.307	-.890	-1.269	-1.346	-1.440
	.150	.180	.148	.107	.066	.022	-.016	-.053	-.074	-.095	-.220	-.332	-.473
	.250	.133	.113	.084	.057	.026	-.002	-.033	-.057	-.070	-.081	-.093	-.108
	.350	.135	.116	.091	.068	.046	.027	.004	-.017	-.032	-.047	-.060	-.071
	.450	.098	.084	.066	.048	.033	.021	.004	-.013	-.024	-.037	-.049	-.057
	.550	.090	.080	.067	.054	.045	.038	.027	.014	.007	-.003	-.013	-.020
	.650	.036	.032	.025	.019	.017	.017	.013	.003	.002	-.005	-.013	-.017
	.750	.030	.032	.029	.030	.034	.042	.043	.036	.038	.034	.028	.025
	.850	.038	.044	.050	.059	.072	.085	.091	.086	.091	.088	.084	.081
	.925	.027	.038	.051	.071	.093	.118	.128	.126	.132	.130	.126	.123
	b.975	.250	.310	.340	.340	.280	.290	.280	.350	.360	.345	.360	.348
	a1.000	.500	.470	.512	.495	.550	.550	.500	.510	.570	.490	.570	.470

^aNo orifice.^bFaired value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78^\circ$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(r) $M = 0.58$.

	J	2.110	2.152	2.198	2.244	2.281	2.329	2.370	2.422	2.488	2.519	2.551	2.596
M_x		.907	.897	.887	.878	.867	.858	.847	.838	.830	.824	.819	.810
α_x		3.16	2.60	2.00	1.41	.95	.35	-.15	-.77	-1.64	-1.90	-2.26	-2.76
$\Delta\theta$.42	.24	.05	-.13	-.27	-.37	-.40	-.44	-.56	-.64	-.73	-.86
α_1		1.63	1.51	1.38	1.24	1.09	.96	.79	.59	.33	.17	.04	-.11
c_n		.5219	.4826	.4445	.3974	.3510	.3090	.2529	.1916	.1065	.0555	.0123	-.0348
c_m		-.1417	-.1350	-.1319	-.1244	-.1226	-.1272	-.1293	-.1309	-.1345	-.1352	-.1370	-.1395
c_c		.0251	.0252	.0250	.0249	.0258	.0255	.0253	.0258	.0279	.0292	.0305	.0323
c/b	Pressure coefficient, P												
Upper surface	^a 0.000	1.223	1.217	1.212	1.207	1.203	1.197	1.192	1.188	1.184	1.181	1.179	1.175
	.025	.165	.212	.254	.310	.358	.400	.438	.500	.558	.591	.616	.650
	.050	-.038	-.003	.033	.081	.122	.158	.193	.251	.309	.342	.367	.400
	.100	-.226	-.194	-.165	-.124	-.089	-.055	-.023	.032	.084	.116	.140	.172
	.200	-.379	-.350	-.308	-.296	-.270	-.239	-.212	-.163	-.117	-.088	-.067	-.037
	.300	-.475	-.446	-.437	-.394	-.365	-.356	-.334	-.290	-.250	-.222	-.203	-.176
	.400	-.513	-.486	-.445	-.422	-.402	-.371	-.355	-.350	-.335	-.315	-.295	-.268
	.500	-.638	-.628	-.611	-.597	-.584	-.563	-.576	-.555	-.509	-.448	-.419	-.389
	.600	-.684	-.679	-.667	-.657	-.644	-.641	-.620	-.572	-.527	-.482	-.474	-.466
	.700	-.786	-.775	-.767	-.745	-.736	-.726	-.706	-.657	-.623	-.616	-.596	-.537
	.800	-.430	-.388	-.348	-.328	-.331	-.343	-.382	-.384	-.381	-.364	-.374	-.394
Lower surface	.900	-.337	-.301	-.265	-.230	-.202	-.158	-.105	-.066	-.075	-.085	-.097	-.115
	.950	-.338	-.301	-.260	-.219	-.180	-.120	-.049	.025	.039	.047	.046	.040
	.0375	.089	.017	-.039	-.119	-.344	-.659	-.888	-1.058	-1.182	-1.263	-1.326	-1.423
	.075	.112	.056	.013	-.050	-.094	-.166	-.503	-.912	-1.069	-1.161	-1.220	-1.310
	.150	.150	.111	.083	.039	-.005	-.027	-.045	-.102	-.433	-.635	-.790	-.996
	.250	.118	.090	.071	.037	.002	-.019	-.043	-.052	-.059	-.072	-.107	-.150
	.350	.115	.093	.079	.055	.028	.012	-.009	-.019	-.029	-.029	-.032	-.040
	.450	.080	.063	.054	.036	.014	.004	-.012	-.019	-.029	-.029	-.030	-.037
	.550	.074	.061	.055	.043	.027	.020	.010	.009	.001	.001	0	-.006
	.650	.017	.009	.008	.002	-.008	-.007	-.009	-.005	-.009	-.005	-.005	-.009
	.750	.013	.008	.011	.010	.006	.013	.016	.027	.027	.032	.032	.030
	.850	.027	.024	.029	.034	.036	.050	.061	.079	.080	.087	.089	.086
	.925	.025	.019	.025	.036	.043	.065	.086	.113	.120	.128	.130	.129
	.975	.031	.010	.020	.037	.050	.072	.098	.140	.150	.159	.160	.160
	^b 1.000	.020	.002	.016	.037	.050	.078	.102	.160	.168	.178	.175	.175

^aNo orifices.^bFaired value.

TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.05 PROPELLER BLADE SECTION ($\alpha = 0.78$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(S) $M = 0.60$.

	J	2.103	2.142	2.174	2.206	2.244	2.275	2.323	2.362	2.407	2.443	2.486	2.534	2.566
M_x		.940	.933	.922	.915	.908	.898	.891	.883	.875	.865	.858	.850	.845
α_x		3.26	2.74	2.32	1.91	1.42	1.03	.43	-.05	-.59	-1.01	-1.51	-2.06	-2.42
$\Delta\theta$		-.06	-.11	-.14	-.17	-.23	-.31	-.45	-.55	-.66	-.73	-.81	-.89	-.94
α_1		1.64	1.52	1.47	1.29	1.11	.96	.74	.62	.42	.30	.19	.03	-.12
α_n		.5265	.4877	.4697	.4129	.3548	.3071	.2387	.1994	.1355	.0955	.0619	.0097	-.0374
α_m		-.1732	-.1719	-.1689	-.1590	-.1516	-.1467	-.1444	-.1426	-.1460	-.1478	-.1509	-.1544	-.1509
α_c		.0361	.0364	.0367	.0359	.0345	.0337	.0338	.0341	.0343	.0347	.0347	.0350	.0351
c/b	Pressure coefficient, P													
Upper surface	a.0000	1.241	1.237	1.231	1.227	1.223	1.218	1.214	1.210	1.206	1.201	1.198	1.194	1.191
	.025	.251	.297	.313	.347	.393	.417	.469	.498	.535	.561	.588	.624	.653
	.050	.041	.082	.091	.121	.161	.181	.231	.258	.293	.317	.344	.379	.408
	.100	-.148	-.113	-.107	-.084	-.048	-.029	.018	.042	.075	.095	.120	.154	.181
	.200	-.308	-.277	-.261	-.241	-.227	-.213	-.170	-.149	-.120	-.103	-.083	-.052	-.029
	.300	-.404	-.373	-.382	-.370	-.334	-.309	-.285	-.275	-.248	-.232	-.216	-.190	-.169
	b.400	-.490	-.465	-.483	-.470	-.434	-.408	-.400	-.390	-.373	-.362	-.351	-.319	-.293
	.500	-.569	-.560	-.562	-.551	-.535	-.528	-.502	-.498	-.500	-.498	-.495	-.455	-.418
	.600	-.662	-.611	-.615	-.609	-.595	-.593	-.569	-.570	-.546	-.534	-.514	-.484	-.461
	.700	-.718	-.706	-.713	-.711	-.691	-.682	-.664	-.659	-.639	-.625	-.614	-.592	-.581
	.800	-.838	-.828	-.837	-.790	-.708	-.619	-.574	-.532	-.554	-.571	-.606	-.636	-.581
Lower surface	.900	-.414	-.393	-.372	-.332	-.285	-.259	-.230	-.208	-.178	-.152	-.110	-.067	-.063
	.950	-.409	-.387	-.366	-.325	-.278	-.251	-.217	-.186	-.147	-.108	-.056	.014	.041
	.0375	.052	-.008	-.058	-.226	-.491	-.608	-.739	-.840	-.946	-1.035	-1.105	-1.194	-1.297
	.075	.086	.039	-.005	-.058	-.148	-.338	-.657	-.751	-.856	-.939	-1.012	-1.110	-1.171
	.150	.141	.109	.074	.028	.002	-.009	-.064	-.302	-.599	-.766	-.850	-.935	-.993
	.250	.111	.088	.059	.024	.002	-.013	-.031	-.047	-.072	-.124	-.210	-.355	-.490
	.350	.113	.095	.070	.043	.028	.016	-.002	-.018	-.023	-.030	-.035	-.053	-.093
	.450	.078	.063	.041	.020	.011	.002	-.011	-.025	-.029	-.031	-.030	-.023	-.017
	.550	.073	.060	.041	.024	.020	.013	.006	-.005	-.006	-.008	-.006	.003	.008
	.650	.015	.005	-.011	-.022	-.022	-.024	-.027	-.032	-.027	-.025	-.022	-.009	-.001
	.750	.016	.007	-.009	-.017	-.013	-.013	-.011	-.011	-.004	.001	.009	.024	.031
	.850	.041	.033	.017	.009	.013	.013	.020	.023	.036	.044	.057	.075	.085
	.925	.051	.041	.024	.013	.015	.016	.025	.033	.051	.065	.082	.107	.120
	b.975	.056	.040	.025	0	.015	.022	.022	.038	.056	.076	.096	.112	.130
	a.1.000	.060	.044	.025	0	.014	.023	.020	.039	.052	.080	.100	.111	.130

a. No orifice.

b. Paired value.

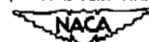


TABLE 6.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.85 PROPELLER BLADE SECTION ($\alpha = 0.78^\circ$; $\beta_x = 43.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Computed(h) $M = 0.65$.

J	2.089	2.102	2.132	2.160	2.179	2.213	2.243	2.268	2.299	2.326	2.359	2.386	2.418	2.451
M_x	1.026	1.015	1.007	.999	.989	.983	.977	.969	.962	.956	.949	.941	.934	.923
c_{D_e}	3.45	3.28	2.88	2.50	2.26	1.81	1.43	1.11	.73	.39	-.01	-.34	-.72	-1.11
$\Delta\delta$	-.49	-.41	-.47	-.52	-.56	-.63	-.69	-.73	-.79	-.82	-.89	-.93	-.98	-1.03
α_1	1.44	1.38	1.21	1.12	1.01	.87	.70	.58	.42	.27	.12	0	-.12	-.30
c_{D_i}	.4613	.4406	.3858	.3587	.3239	.2781	.2239	.1858	.1342	.0855	.0394	.0013	-.0381	-.0961
c_{D_B}	-.1922	-.1929	-.1875	-.1870	-.1829	-.1780	-.1696	-.1671	-.1516	-.1457	-.1383	-.1367	-.1327	-.1296
c_e	.0506	.0528	.0515	.0521	.0529	.0534	.0509	.0506	.0471	.0450	.0446	.0446	.0440	.0434
c/b	Pressure coefficient, P													
Upper surface	a	0.000	1.291	1.284	1.279	1.274	1.268	1.265	1.261	1.257	1.253	1.250	1.245	1.241
	b	.025	.399	.419	.451	.463	.471	.491	.513	.524	.545	.559	.589	.602
	c	.050	.199	.214	.240	.251	.257	.273	.292	.298	.318	.330	.361	.371
	d	.100	.008	.021	.045	.052	.056	.071	.088	.093	.110	.120	.150	.159
	e	.200	-.156	-.145	-.118	-.100	-.097	-.093	-.090	-.092	-.076	-.067	-.039	-.031
	f	.300	-.255	-.243	-.220	-.223	-.230	-.220	-.195	-.197	-.175	-.171	-.158	-.157
	g	.400	-.335	-.320	-.308	-.317	-.324	-.316	-.297	-.290	-.281	-.273	-.270	-.264
	h	.500	-.415	-.410	-.404	-.404	-.407	-.402	-.394	-.401	-.391	-.390	-.375	-.373
	i	.600	-.467	-.467	-.453	-.454	-.461	-.454	-.458	-.454	-.456	-.442	-.448	-.453
	j	.700	-.554	-.554	-.550	-.545	-.559	-.555	-.561	-.556	-.578	-.586	-.573	-.579
Lower surface	k	.800	-.669	-.669	-.664	-.672	-.683	-.681	-.679	-.687	-.693	-.692	-.700	-.707
	l	.900	-.810	-.814	-.817	-.830	-.843	-.843	-.837	-.817	-.539	-.412	-.349	-.329
	m	.950	-.860	-.865	-.835	-.836	-.822	-.638	-.517	-.455	-.395	-.356	-.317	-.303
	n	.0375	-.050	-.139	-.260	-.314	-.368	-.418	-.486	-.536	-.604	-.654	-.726	-.784
	o	.075	.032	-.026	-.188	-.266	-.331	-.382	-.447	-.522	-.592	-.660	-.661	-.711
	p	.150	.129	.115	.090	.055	-.060	-.204	-.305	-.357	-.424	-.474	-.534	-.580
	q	.250	.099	.085	.055	.036	.007	-.021	-.093	-.200	-.359	-.438	-.497	-.540
	r	.350	.115	.103	.073	.055	.021	0	-.021	-.045	-.103	-.188	-.345	-.420
	s	.450	.080	.068	.041	.023	-.015	-.038	-.057	-.074	-.089	-.101	-.125	-.152
	t	.550	.086	.071	.050	.054	-.001	-.021	-.041	-.057	-.069	-.075	-.069	-.075

^aNo orifice.^bPaired value.

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $P_x = 41.10^\circ$; $\beta_{0.725} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

r	2.709	2.541	2.376	2.183	2.178	2.030	1.879	1.710	1.551	1.629	1.799	1.959	2.086	2.267	2.426	2.614
M_x	.690	.668	.612	.587	.589	.573	.554	.536	.520	.530	.548	.563	.580	.604	.620	.643
α_x	4.31	4.48	4.56	4.83	4.90	5.86	5.97	8.46	10.95	9.72	7.13	4.84	3.11	.77	-1.16	-3.29
$\Delta\theta$	-.63	-.32	-.04	.30	.30	.50	.72	.96	1.18	1.08	.84	.60	.43	.16	-.13	-.45
α_1	-.21	.47	1.06	1.75	1.70	2.37	2.86	3.42	3.60	3.51	3.17	2.61	2.10	1.40	.88	.15
c_m	-.0581	.1277	.2890	.4735	.4613	.6387	.7697	.9248	.9568	.9387	.8477	.6994	.5652	.3787	.2387	.0400
c_m	-.1019	-.1006	-.0929	-.0950	-.0954	-.0891	-.0823	-.0600	-.0760	-.0580	-.0744	-.0887	-.0928	-.0985	-.0954	-.1049
c_o																
a/b	Pressure coefficient, P															
Upper surface	a/b	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.000	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.025	.695	.691	.690	.687	.689	.684	.679	.673	.669	.672	.677	.681	.687	.686	.699
	.050	.393	.397	.397	.394	.396	.391	.386	.380	.376	.379	.384	.388	.394	.393	.406
	.100	.179	.185	.184	.181	.183	.178	.173	.167	.163	.166	.171	.175	.174	.176	.189
	.200	-.009	-.112	-.243	-.429	-.437	-.584	-.705	-.940	-.1.052	-.1.052	-.720	-.671	-.494	-.326	-.199
	.300	-.119	-.202	-.299	-.438	-.433	-.546	-.633	-.695	-.986	-.870	-.664	-.641	-.502	-.365	-.268
	.400	-.179	-.242	-.317	-.431	-.426	-.498	-.557	-.599	-.729	-.620	-.583	-.584	-.463	-.367	-.295
	.500	-.249	-.311	-.354	-.434	-.429	-.484	-.517	-.486	-.547	-.482	-.527	-.557	-.457	-.389	-.337
	.600	-.301	-.331	-.372	-.423	-.420	-.462	-.472	-.424	-.423	-.393	-.475	-.525	-.445	-.398	-.362
	.700	-.338	-.356	-.381	-.413	-.410	-.430	-.422	-.350	-.322	-.316	-.407	-.422	-.420	-.393	-.370
	.800	-.302	-.304	-.314	-.331	-.326	-.326	-.299	-.243	-.254	-.234	-.291	-.374	-.326	-.321	-.310
Lower surface	a/b	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.000	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.025	.695	.691	.690	.687	.689	.684	.679	.673	.669	.672	.677	.681	.687	.686	.699
	.050	.393	.397	.397	.394	.396	.391	.386	.380	.376	.379	.384	.388	.394	.393	.406
	.100	.179	.185	.184	.181	.183	.178	.173	.167	.163	.166	.171	.175	.174	.176	.189
	.200	-.009	-.112	-.243	-.429	-.437	-.584	-.705	-.940	-.1.052	-.1.052	-.720	-.671	-.494	-.326	-.199
	.300	-.119	-.202	-.299	-.438	-.433	-.546	-.633	-.695	-.986	-.870	-.664	-.641	-.502	-.365	-.268
	.400	-.179	-.242	-.317	-.431	-.426	-.498	-.557	-.599	-.729	-.620	-.583	-.584	-.463	-.367	-.295
	.500	-.249	-.311	-.354	-.434	-.429	-.484	-.517	-.486	-.547	-.482	-.527	-.557	-.457	-.389	-.337
	.600	-.301	-.331	-.372	-.423	-.420	-.462	-.472	-.424	-.423	-.393	-.475	-.525	-.445	-.398	-.362
	.700	-.338	-.356	-.381	-.413	-.410	-.430	-.422	-.350	-.322	-.316	-.407	-.422	-.420	-.393	-.370
	.800	-.302	-.304	-.314	-.331	-.326	-.326	-.299	-.243	-.254	-.234	-.291	-.374	-.326	-.321	-.310
	.900	-.188	-.176	-.169	-.174	-.171	-.149	-.115	-.121	-.187	-.152	-.130	-.192	-.157	-.168	-.171
	.950	-.080	-.005	-.002	-.005	-.001	-.001	.001	-.047	-.149	-.107	-.016	-.054	.004	.001	0
Lower surface	a/b	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.000	1.110	1.102	1.097	1.088	1.089	1.084	1.079	1.073	1.069	1.072	1.077	1.081	1.087	1.086	1.099
	.025	.695	.691	.690	.687	.689	.684	.679	.673	.669	.672	.677	.681	.687	.686	.699
	.050	.393	.397	.397	.394	.396	.391	.386	.380	.376	.379	.384	.388	.394	.393	.406
	.100	.179	.185	.184	.181	.183	.178	.173	.167	.163	.166	.171	.175	.174	.176	.189
	.200	-.009	-.112	-.243	-.429	-.437	-.584	-.705	-.940	-.1.052	-.1.052	-.720	-.671	-.494	-.326	-.199
	.300	-.119	-.202	-.299	-.438	-.433	-.546	-.633	-.695	-.986	-.870	-.664	-.641	-.502	-.365	-.268
	.400	-.179	-.242	-.317	-.431	-.426	-.498	-.557	-.599	-.729	-.620	-.583	-.584	-.463	-.367	-.295
	.500	-.249	-.311	-.354	-.434	-.429	-.484	-.517	-.486	-.547	-.482	-.527	-.557	-.457	-.389	-.337
	.600	-.301	-.331	-.372	-.423	-.420	-.462	-.472	-.424	-.423	-.393	-.475	-.525	-.445	-.398	-.362
	.700	-.338	-.356	-.381	-.413	-.410	-.430	-.422	-.350	-.322	-.316	-.407	-.422	-.420	-.393	-.370
	.800	-.302	-.304	-.314	-.331	-.326	-.326	-.299	-.243	-.254	-.234	-.291	-.374	-.326	-.321	-.310
	.900	-.188	-.176	-.169	-.174	-.171	-.149	-.115	-.121	-.187	-.152	-.130	-.192	-.157	-.168	-.171
	.950	-.080	-.005	-.002	-.005	-.001	-.001	.001	-.047	-.149	-.107	-.016	-.054	.004	.001	0

*No orifice.

*Paired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.7R} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	1.762	1.887	2.053	2.186	2.344	2.464	2.610	2.700	2.694	2.538	2.413	2.276	2.126	1.972	1.856
M_x	.649	.662	.682	.697	.723	.743	.763	.776	.769	.750	.729	.707	.690	.670	.655
α_x	7.68	5.85	3.55	1.80	-.18	-1.60	-3.25	-4.22	-3.72	-2.44	-1.00	.66	2.58	4.66	6.30
$\Delta\beta$	1.33	1.01	.61	.31	-.05	-.33	-.79	-1.02	-.92	-.54	-.21	.10	.44	.80	1.09
α_1	3.63	3.13	2.46	1.88	1.22	.79	.15	-.27	-.06	.42	1.03	1.50	2.10	2.74	3.30
α_n	.9716	.8413	.6639	.5097	.3332	.2142	.0400	-.0723	-.0174	.1135	.2800	.4058	.5681	.7355	.8890
α_m	-.0655	-.0814	-.0944	-.1029	-.1064	-.1082	-.1240	-.1209	-.1240	-.1196	-.1081	-.1048	-.1001	-.0890	-.0762
α_o															
a/b	Pressure coefficient, P														
Upper surface	$a_0.000$	1.109	1.114	1.122	1.128	1.138	1.146	1.154	1.160	1.157	1.149	1.140	1.131	1.125	1.117
	.025	-.2374	-.1848	-.1799	-.202	-.249	-.484	-.634	-.702	-.668	-.566	-.385	-.069	-.433	-.1246
	.050	-.2244	-.1721	-.1688	-.1834	-.209	-.207	-.365	-.438	-.401	-.292	-.113	-.164	-.566	-.1875
	.100	-.2040	-.1222	-.1708	-.436	-.171	.002	-.141	-.209	-.174	-.076	-.074	-.284	-.554	-.825
	.200	-.620	-.635	-.604	-.432	-.292	-.172	-.061	-.005	-.034	-.113	-.223	-.370	-.533	-.643
	.300	-.648	-.672	-.584	-.482	-.361	-.271	-.183	-.137	-.161	-.227	-.307	-.416	-.527	-.626
	.400	-.601	-.600	-.537	-.474	-.394	-.330	-.262	-.229	-.246	-.297	-.352	-.434	-.500	-.565
	.500	-.560	-.562	-.529	-.477	-.424	-.375	-.330	-.310	-.319	-.353	-.390	-.448	-.501	-.541
	.600	-.509	-.515	-.500	-.471	-.441	-.411	-.385	-.379	-.383	-.401	-.415	-.456	-.486	-.502
	.700	-.444	-.458	-.462	-.454	-.442	-.435	-.425	-.440	-.437	-.433	-.427	-.449	-.460	-.457
	.800	-.309	-.318	-.335	-.342	-.347	-.348	-.356	-.377	-.367	-.355	-.335	-.347	-.345	-.324
	.900	-.123	-.114	-.128	-.144	-.155	-.162	-.176	-.199	-.189	-.174	-.147	-.154	-.144	-.116
	.950	-.006	-.004	.004	.015	.014	.015	.008	-.010	-.001	.008	-.027	.011	.008	.004
Lower surface	$a_0.0375$.689	.588	.388	.154	-.161	-.511	-.985	-1.006	-1.005	-1.008	-.271	-.018	.257	.489
	.075	.569	.481	.321	.152	-.042	-.186	-.860	-.949	-.924	-.702	-.113	.058	.225	.400
	.150	.448	.376	.255	.137	-.003	-.106	-.548	-.763	-.682	-.280	-.046	.061	.185	.312
	.250	.288	.242	.210	.129	.035	-.035	-.212	-.465	-.349	-.075	.013	.082	.172	.232
	.350	.311	.263	.189	.127	.046	-.007	-.070	-.239	-.150	-.031	.030	.078	.151	.224
	.450	.270	.231	.187	.135	.069	.030	0	-.092	-.038	.007	.059	.093	.154	.221
	.550	.229	.197	.149	.109	.059	.028	.014	-.032	-.005	.012	.055	.077	.123	.174
	.650	.186	.158	.119	.087	.051	.031	.029	.009	.019	.021	.052	.064	.098	.137
	.750	.183	.159	.131	.109	.082	.068	.063	.047	.056	.057	.086	.090	.116	.144
	.850	.165	.151	.134	.124	.107	.101	.095	.080	.094	.115	.111	.126	.141	.159
	.925	.161	.153	.148	.148	.140	.135	.127	.109	.116	.124	.149	.140	.146	.161
	$b_0.975$.165	.185	.160	.166	.170	.160	.150	.130	.143	.174	.164	.161	.154	.189
	$a_1.000$.170	.210	.165	.178	.185	.173	.159	.140	.157	.167	.187	.175	.169	.210

^aNo orifice.^bFaired value.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85^\circ$; $\beta_x = 41.10^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(c) $N = 1500$ rpm.

	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$	$\frac{r}{M}$
	2.038	2.104	2.233	2.313	2.436	2.640	2.611	2.578	2.497	2.385	2.273	2.177	2.062	1.968	
	.753	.763	.766	.799	.819	.837	.848	.841	.827	.806	.790	.776	.756	.744	
	3.75	2.86	1.20	.20	-1.27	-2.47	-3.26	-2.89	-1.96	-.67	.70	1.91	3.43	4.71	
	.88	.65	.20	-.10	-.78	-.96	-1.22	-1.11	-.76	-.35	.05	.40	.80	1.12	
	2.60	2.33	1.79	1.38	.78	.20	-.08	.01	.54	1.11	1.61	1.97	2.48	2.93	
	.7032	.6303	.4852	.3768	.2123	.0542	-.0219	.0026	.1471	.3039	.4381	.5348	.6703	.7871	
	-.1000	-.1052	-.1124	-.1170	-.1308	-.1447	-.1573	-.1524	-.1383	-.1209	-.1141	-.1114	-.1029	-.0898	
	.0310					.0310	.0358	.0329	.0275						
	Pressure coefficient, P														
	0.000	1.151	1.155	1.164	1.170	1.179	1.188	1.193	1.189	1.183	1.173	1.166	1.160	1.152	1.147
	.025	-.693	-.389	.035	.283	.509	.643	.775	.739	.632	.433	.182	-.116	-.577	-1.070
	.050	-.860	-.596	-.209	.013	.233	.374	.505	.464	.371	.156	-.078	-.342	-.766	-1.100
	.100	-.980	-.619	-.332	-.159	.027	.152	.275	.237	.153	-.041	-.232	-.437	-.796	-1.137
	.200	-.655	-.610	-.438	-.315	-.164	-.056	.053	.019	-.056	-.219	-.410	-.605	-.840	-1.077
	.300	-.615	-.598	-.495	-.406	-.286	-.193	-.096	-.123	-.188	-.328	-.442	-.541	-.698	-0.923
	.400	-.595	-.571	-.502	-.444	-.358	-.262	-.195	-.219	-.273	-.390	-.470	-.539	-.695	-.924
	.500	-.607	-.613	-.580	-.551	-.487	-.426	-.351	-.370	-.415	-.511	-.565	-.595	-.699	-.974
	.600	-.548	-.548	-.529	-.508	-.462	-.419	-.363	-.366	-.398	-.480	-.521	-.537	-.647	-.936
	.700	-.495	-.502	-.498	-.517	-.660	-.622	-.599	-.608	-.639	-.680	-.687	-.695	-.799	-.982
	.800	-.332	-.343	-.339	-.345	-.335	-.332	-.409	-.316	-.287	-.341	-.344	-.343	-.336	-.324
	.900	-.109	-.117	-.114	-.116	-.113	-.098	-.036	-.045	-.060	-.111	-.114	-.116	-.110	-.105
	.950	.021	.026	.034	.034	.038	.046	.095	.095	.092	.041	.035	.032	.026	.020
	.0375	.403	.282	.054	-.154	-1.054	-1.238	-1.281	-1.258	-1.196	-.626	-.056	.149	.358	.513
	.075	.340	.249	.107	-.033	-.573	-1.125	-1.179	-1.152	-1.062	-.082	.038	.154	.304	.424
	.150	.273	.207	.107	.007	-.046	-.907	-1.059	-1.023	-.135	-.051	.052	.142	.248	.338
	.250	.222	.163	.117	.049	-.009	-.043	-.353	-.143	.049	.009	.079	.130	.194	.272
	.350	.204	.164	.108	.056	.008	.021	-.057	.062	.058	.026	.080	.132	.190	.246
	.450	.193	.167	.121	.080	.041	.047	.105	.104	.090	.057	.099	.141	.185	.223
	.550	.162	.135	.099	.066	.036	.040	.108	.095	.084	.049	.081	.114	.154	.192
	.650	.127	.105	.082	.057	.036	.036	.103	.092	.081	.046	.067	.091	.122	.151
	.750	.140	.123	.105	.086	.071	.073	.132	.127	.122	.080	.095	.112	.136	.158
	.850	.142	.133	.126	.114	.105	.108	.161	.161	.158	.111	.119	.129	.141	.157
	.925	.156	.153	.152	.145	.141	.143	.193	.195	.195	.145	.147	.153	.157	.165
	.975	.170	.172	.180	.172	.171	.175	.220	.219	.226	.166	.175	.180	.167	.178
	1.000	.177	.182	.192	.188	.186	.189	.235	.230	.240	.178	.190	.193	.172	.183

^aNo orifice.

^bPaired values.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

	J	M_x	C_{Dx}	ΔC_{Dx}	C_{L1}	C_{D1}	C_{D2}	C_{D3}	C_{D4}	C_{D5}	C_{D6}	C_{D7}	C_{D8}	C_{D9}	C_{D10}
	2.545	2.493	2.438	2.360	2.302	2.240	2.151	2.080	2.115	2.191	2.269	2.337	2.396	2.469	2.529
	.903	.886	.876	.861	.852	.840	.826	.815	.817	.831	.843	.858	.867	.881	.894
	-2.52	-1.93	-1.30	-.37	.34	1.11	2.25	3.18	2.72	1.73	.75	-.09	-.80	-1.66	-2.34
	-1.13	-.94	-.67	-.31	-.05	.22	.62	.95	.79	.44	.09	-.21	-.47	-.81	-1.08
	-.38	.07	.53	.93	1.35	1.74	2.22	2.52	2.32	1.98	1.56	1.12	.77	.36	-.10
	-.1019	.0194	.1445	.2523	.3665	.4723	.6013	.6800	.6277	.5361	.4245	.3045	.2103	.0981	-.0277
	-.1516	-.1622	-.1472	-.1368	-.1257	-.1235	-.1226	-.1141	-.1173	-.1235	-.1259	-.1311	-.1386	-.1560	-.1598
	.0425	.0393	.0327	.0253	.0193	.0121	.0017			.0069	.0155	.0226	.0280	.0363	.0411
o/b		Pressure coefficient, P													
Upper surface	.000	1.221	1.211	1.206	1.199	1.195	1.190	1.182	1.177	1.178	1.185	1.191	1.197	1.202	1.209
	.025	.715	.699	.685	.682	.663	.657	.644	.632	.622	.605	.596	.586	.574	.563
	.050	.460	.438	.418	.401	.382	.363	.344	.323	.306	.286	.276	.264	.254	.244
	.100	.245	.184	.110	.009	-.096	-.236	-.427	-.636	-.849	-.1030	-.167	-.043	.041	.148
	.200	.032	-.026	-.096	-.184	-.274	-.379	-.536	-.748	-.944	-.1164	-.331	-.227	-.159	-.061
	.300	-.109	-.165	-.227	-.307	-.378	-.491	-.649	-.862	-.1074	-.365	-.454	-.348	-.287	-.198
	.400	-.188	-.230	-.279	-.363	-.441	-.530	-.670	-.818	-.1071	-.599	-.497	-.406	-.334	-.255
	.500	-.328	-.377	-.423	-.474	-.520	-.589	-.675	-.791	-.914	-.640	-.556	-.499	-.466	-.403
	.600	-.431	-.484	-.535	-.588	-.627	-.664	-.730	-.843	-.933	-.694	-.650	-.612	-.579	-.512
	.700	-.577	-.625	-.667	-.699	-.743	-.776	-.835	-.945	-.1043	-.751	-.765	-.730	-.701	-.648
	.800	-.678	-.718	-.757	-.787	-.808	-.829	-.876	-.984	-.1084	-.862	-.886	-.846	-.828	-.605
Lower surface	.900	-.155	-.145	-.124	-.102	-.088	-.071	-.074	-.082	-.073	-.070	-.078	-.103	-.120	-.145
	.950	-.093	-.082	-.061	-.040	-.026	-.002	.023	.040	.040	.009	-.014	-.043	-.060	-.087
	.0375	-1.083	-1.052	-.986	-.865	-.716	-.529	.172	.302	.235	.071	-.123	-.749	-.932	-1.080
	.075	-.997	-.962	-.893	-.640	-.492	-.260	.172	.268	.220	.113	-.006	-.186	-.827	-.993
	.150	-.903	-.864	-.776	-.415	-.219	.065	.155	.224	.192	.114	.022	-.034	-.210	-.892
	.250	-.790	-.720	-.607	.017	.032	.081	.122	.131	.131	.115	.055	.009	.012	-.331
	.350	-.737	-.667	.037	.026	.040	.082	.137	.180	.163	.109	.061	.023	.015	.026
	.450	-.130	.065	.059	.053	.063	.096	.143	.178	.168	.117	.080	.049	.040	.069
	.550	.029	.064	.042	.039	.048	.075	.113	.149	.136	.092	.061	.034	.025	.051
	.650	.075	.048	.028	.028	.035	.060	.088	.117	.108	.073	.048	.025	.014	.036
	.750	.069	.066	.056	.060	.064	.085	.110	.134	.127	.095	.075	.055	.045	.060
	.850	.091	.080	.078	.084	.089	.106	.124	.144	.141	.097	.079	.068	.078	.086
	.925	.093	.092	.096	.106	.112	.127	.146	.166	.163	.135	.121	.101	.091	.093
	.975	.099	.110	.110	.125	.130	.147	.168	.180	.178	.156	.140	.120	.119	.108
	1.000	.100	.118	.118	.134	.141	.155	.179	.190	.185	.166	.150	.126	.132	.111

^aNo orifice.^bPaired value.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $M = 0.56$.

γ	2.128	2.152	2.192	2.235	2.276	2.323	2.367	2.414	2.453	2.514	2.564	2.602	2.659	2.460	
M_{∞}	.918	.903	.894	.885	.876	.868	.859	.850	.840	.832	.823	.814	.805	.838	
$C_{p,i}$	2.55	2.24	1.72	1.17	.66	.08	-.45	-1.01	-1.47	-2.17	-2.74	-3.16	-3.78	-1.55	
Δp	.18	.08	-.03	-.12	-.17	-.21	-.30	-.45	-.58	-.74	-.86	-.94	-1.06	-.60	
$C_{p,e}$	1.98	1.86	1.74	1.57	1.46	1.21	1.08	.90	.73	.39	.21	.02	-.16	.69	
$C_{p,t}$.5361	.5026	.4729	.4258	.3968	.3290	.2942	.2452	.1994	.1071	.0568	.0065	-.0439	.1890	
$C_{p,b}$	-.1385	-.1350	-.1299	-.1247	-.1245	-.1257	-.1316	-.1342	-.1321	-.1372	-.1417	-.1419	-.1347	-.1314	
ϕ_o	.0202	.0203	.0205	.0213	.0213	.0222	.0231	.0249	.0262	.0289					
o/b		Pressure coefficients, P													
Upper surface	θ .000	1.228	1.221	1.216	1.211	1.207	1.202	1.198	1.194	1.189	1.185	1.181	1.177	1.173	1.188
	.025	.210	.219	.253	.303	.338	.425	.464	.513	.553	.610	.677	.678	.708	.537
	.050	-.050	-.043	-.015	.031	.063	.148	.188	.238	.281	.338	.437	.409	.444	.265
	.100	-.212	-.207	-.186	-.152	-.128	-.051	-.014	.032	.070	.122	.167	.185	.217	.055
	.200	-.359	-.367	-.358	-.324	-.308	-.238	-.205	-.167	-.133	-.086	-.044	-.029	-.001	-.145
	.300	-.462	-.469	-.455	-.430	-.406	-.347	-.324	-.290	-.260	-.220	-.180	-.166	-.139	-.272
	.400	-.544	-.546	-.532	-.507	-.491	-.436	-.400	-.381	-.356	-.314	-.271	-.256	-.229	-.369
	.500	-.610	-.617	-.607	-.588	-.586	-.526	-.498	-.471	-.439	-.427	-.374	-.354	-.327	-.454
	.600	-.668	-.683	-.680	-.670	-.697	-.594	-.583	-.547	-.513	-.453	-.442	-.434	-.410	-.522
	.700	-.794	-.815	-.815	-.802	-.793	-.723	-.702	-.679	-.639	-.623	-.588	-.551	-.507	-.634
Lower surface	.800	-.324	-.317	-.293	-.284	-.280	-.319	-.380	-.406	-.362	-.340	-.355	-.373	-.383	-.384
	.900	-.280	-.269	-.243	-.222	-.180	-.113	-.072	-.068	-.092	-.113	-.136	-.130	-.180	-.110
	.950	-.274	-.261	-.233	-.206	-.155	-.070	-.001	-.036	-.049	-.047	-.043	-.031	-.010	-.029
	.0375	.096	.022	-.039	-.116	-.191	-.266	-.311	-.375	-.409	-.429	-.432	-.443	-.449	-.117
	.075	.157	.105	-.057	-.107	-.132	-.161	-.232	-.281	-.363	-.409	-.420	-.428	-.429	-.992
	.150	.144	.096	.061	.016	-.006	-.018	-.019	-.015	-.065	-.145	-.179	-.188	-.161	-.110
	.250	.152	.111	.086	.053	.039	.032	.022	.013	.008	.007	-.033	-.083	-.215	-.009
	.350	.130	.095	.074	.049	.040	.040	.020	.021	.014	.012	.006	-.007	-.105	-.005
	.450	.132	.100	.084	.063	.060	.065	.062	.053	.046	.018	.035	.024	-.034	.027
	.550	.093	.063	.052	.036	.036	.047	.048	.042	.038	.011	.032	.021	-.008	.019
.650	.055	.030	.021	.011	.014	.033	.039	.038	.037	.011	.034	.026	.014	.017	
.750	.064	.041	.035	.029	.037	.061	.072	.074	.076	.076	.074	.066	.057	.057	
.850	.058	.036	.034	.032	.046	.078	.097	.105	.108	.107	.107	.100	.090	.087	
.925	.056	.034	.034	.036	.055	.095	.123	.137	.145	.147	.146	.140	.125	.125	
.975	.059	.037	.039	.035	.059	.110	.145	.164	.175	.185	.178	.170	.160	.156	
1.000	.062	.038	.040	.035	.060	.120	.157	.180	.190	.217	.195	.188	.180	.173	

*No airfoil.

*Paired value.

NACA

TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(r) $M = 0.58$.

J	2.163	2.177	2.216	2.240	2.270	2.324	2.350	2.387	2.414	2.449	2.481	2.526	2.563	2.601	2.636
M_x	.934	.923	.915	.906	.899	.897	.884	.881	.871	.869	.858	.854	.843	.837	.831
α_x	2.09	1.91	1.41	1.11	.73	.07	-.25	-.69	-1.01	-1.42	-1.80	-2.31	-2.73	-3.15	-3.53
α_1	.09	.02	-.16	-.26	-.38	-.50	-.53	-.56	-.59	-.65	-.73	-.86	-.99	-1.11	-1.22
α_2	1.79	1.62	1.50	1.39	1.32	1.08	.93	.84	.72	.65	.53	.34	.09	-.04	-.21
α_n	.4839	.4374	.4058	.3768	.3594	.2948	.2535	.2284	.1974	.1761	.1439	.0916	.0252	-.0103	-.0581
α_m	-.1553	-.1414	-.1416	-.1354	-.1331	-.1390	-.1421	-.1434	-.1481	-.1527	-.1552	-.1596	-.1540	-.1499	-.1496
α_c	.0283	.0269	.0262	.0262	.0262	.0290	.0295	.0296	.0308	.0319	.0319	.0338	.0343	.0343	.0356
Pressure coefficient, P															
Upper surface	α/b	1.237	1.231	1.227	1.222	1.218	1.217	1.210	1.209	1.204	1.203	1.197	1.195	1.190	1.184
	0.000	.317	.345	.375	.394	.413	.479	.502	.530	.549	.577	.608	.645	.676	.723
	.025	.055	.080	.108	.125	.143	.209	.231	.258	.278	.307	.337	.377	.410	.460
	.050	-.120	-.102	-.079	-.067	-.054	.005	.024	.048	.065	.092	.118	.155	.184	.230
	.100	-.270	-.265	-.244	-.241	-.233	-.184	-.169	-.149	-.135	-.112	-.089	-.057	-.032	.009
	.200	-.386	-.376	-.363	-.354	-.351	-.304	-.289	-.275	-.265	-.244	-.222	-.194	-.172	-.133
	.300	-.472	-.462	-.441	-.433	-.420	-.381	-.370	-.351	-.335	-.328	-.322	-.300	-.275	-.239
	.400	-.487	-.479	-.465	-.470	-.471	-.437	-.432	-.424	-.429	-.422	-.411	-.410	-.406	-.368
	.500	-.608	-.607	-.599	-.606	-.608	-.576	-.571	-.562	-.577	-.538	-.506	-.487	-.416	-.401
	.600	-.706	-.715	-.707	-.717	-.725	-.702	-.708	-.697	-.692	-.670	-.668	-.642	-.643	-.625
	.700	-.598	-.478	-.411	-.383	-.371	-.434	-.441	-.435	-.465	-.506	-.539	-.576	-.581	-.359
Lower surface	.800	-.315	-.285	-.251	-.235	-.214	-.200	-.175	-.151	-.142	-.113	-.068	-.064	-.080	-.103
	.900	-.297	-.266	-.234	-.214	-.184	-.160	-.123	-.083	-.063	-.041	-.001	.022	-.040	.041
	.950	0	-.093	-.215	-.356	-.487	-.720	-.805	-.876	-.948	-1.011	-1.083	-1.165	-1.250	-1.380
	.0375	.102	.053	.017	0	-.046	-.294	-.702	-.779	-.855	-.917	-.987	-1.068	-1.148	-1.272
	.150	.104	.067	.040	.017	.002	-.009	-.078	-.246	-.459	-.675	-.785	-.941	-1.026	-1.138
	.250	.117	.092	.076	.059	.048	.033	.029	.032	.027	.017	.008	-.090	-.207	-.302
	.350	.116	.092	.080	.066	.055	.040	.032	.035	.031	.036	.042	.043	.028	-.077
	.450	.120	.100	.091	.079	.073	.060	.056	.058	.054	.057	.061	.066	.064	.060
	.550	.085	.069	.063	.054	.049	.040	.036	.041	.038	.044	.051	.052	.052	.048
	.650	.048	.034	.032	.026	.025	.017	.017	.025	.024	.033	.043	.048	.047	.044
	.750	.061	.049	.069	.044	.044	.041	.044	.054	.056	.065	.079	.082	.083	.079
	.850	.063	.054	.076	.050	.054	.054	.060	.075	.080	.092	.108	.113	.116	.111
	.925	.065	.054	.076	.054	.059	.062	.074	.093	.102	.118	.138	.143	.146	.144
	b.975	.069	.052	.074	.057	.058	.069	.086	.109	.120	.135	.161	.173	.175	.175
	a1.000	.071	.051	.077	.055	.055	.070	.092	.117	.129	.145	.177	.190	.189	.189

a No orifice.

b Paired value.



TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($\alpha = 0.85^\circ$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(2) $M = 0.60$.

	2.135	2.158	2.173	2.220	2.240	2.265	2.290	2.314	2.346	2.370	2.392	2.429	2.464	2.496	2.522	2.560
γ	.977	.970	.958	.939	.951	.945	.939	.933	.926	.921	.911	.908	.901	.898	.890	.883
M_x	2.46	2.16	1.96	1.36	1.11	.80	.48	.19	-.20	-.49	-.75	-1.19	-1.60	-1.97	-2.26	-2.69
α_2	-.25	-.27	-.28	-.33	-.37	-.44	-.51	-.60	-.72	-.79	-.85	-.94	-1.01	-1.07	-1.11	-1.16
α_1	1.69	1.55	1.49	1.29	1.18	1.10	.98	.90	.71	.59	.49	.28	.13	.02	-.04	-.20
c_n	.4574	.4200	.4026	.3497	.3200	.2974	.2665	.2452	.1929	.1594	.1323	.0774	.0348	.0052	-.0123	-.0542
c_m	-.1794	-.1726	-.1680	-.1639	-.1601	-.1624	-.1614	-.1650	-.1622	-.1621	-.1626	-.1590	-.1576	-.1573	-.1599	-.1588
c_o	.0407	.0379	.0370	.0373	.0370	.0375	.0378	.0380	.0384	.0387	.0387	.0397	.0399	.0399	.0396	.0400
c/b	Pressure coefficient, P															
Upper surface	.0000	1.261	1.257	1.250	1.251	1.247	1.244	1.240	1.237	1.233	1.230	1.225	1.223	1.220	1.218	1.214
	.025	.406	.418	.420	.465	.479	.499	.529	.555	.565	.579	.595	.619	.642	.661	.671
	.050	.154	.163	.161	.206	.218	.238	.268	.291	.303	.316	.332	.359	.380	.403	.412
	.100	-.015	-.010	-.014	.024	.032	.050	.075	.094	.105	.116	.130	.153	.171	.189	.196
	.200	-.209	-.196	-.197	-.156	-.152	-.140	-.118	-.101	-.090	-.082	-.070	-.051	-.035	-.019	-.013
	.300	-.312	-.296	-.300	-.271	-.263	-.252	-.240	-.224	-.210	-.208	-.201	-.185	-.174	-.160	-.155
	.400	-.383	-.382	-.390	-.356	-.348	-.332	-.314	-.303	-.294	-.282	-.270	-.240	-.228	-.222	-.221
	.500	-.437	-.443	-.447	-.414	-.410	-.405	-.393	-.385	-.380	-.378	-.373	-.370	-.373	-.368	-.369
	.600	-.539	-.541	-.548	-.524	-.525	-.520	-.513	-.507	-.505	-.502	-.498	-.494	-.488	-.477	-.471
	.700	-.642	-.632	-.663	-.636	-.638	-.636	-.634	-.631	-.634	-.635	-.634	-.629	-.628	-.620	-.617
	.800	-.732	-.736	-.767	-.751	-.757	-.753	-.747	-.742	-.737	-.739	-.730	-.727	-.715	-.699	-.692
	.900	-.667	-.687	-.708	-.711	-.749	-.713	-.682	-.677	-.684	-.683	-.686	-.687	-.677	-.655	-.636
	.950	-.455	-.411	-.371	-.339	-.320	-.283	-.254	-.229	-.215	-.198	-.169	-.155	-.129	-.102	-.077
Lower surface	.0375	-.154	-.252	-.318	-.446	-.511	-.569	-.629	-.672	-.751	-.807	-.854	-.921	-.982	-1.031	-1.084
	.075	.047	-.044	-.114	-.332	-.441	-.498	-.556	-.597	-.675	-.729	-.774	-.838	-.899	-.947	-.997
	.150	.069	.036	.020	-.012	-.094	-.228	-.379	-.472	-.578	-.634	-.678	-.745	-.804	-.851	-.898
	.250	.107	.065	.071	.054	.040	.038	.031	-.124	-.235	-.235	-.340	-.372	-.471	-.523	-.571
	.350	.100	.083	.071	.061	.051	.051	.055	.061	.040	.035	.030	-.024	-.104	-.163	-.215
	.450	.109	.095	.083	.079	.072	.073	.077	.085	.070	.070	.073	.068	.054	.042	.033
	.550	.069	.058	.049	.048	.042	.045	.050	.058	.046	.045	.051	.055	.057	.063	.062
	.650	.089	.020	.013	.015	.010	.014	.019	.028	.018	.019	.026	.032	.038	.048	.051
	.750	.046	.039	.031	.033	.028	.033	.038	.044	.035	.035	.043	.047	.052	.062	.066
	.850	.066	.058	.047	.049	.043	.043	.047	.054	.043	.043	.052	.055	.060	.072	.080
	.925	.085	.074	.061	.061	.052	.051	.052	.059	.046	.046	.056	.059	.067	.079	.091
	.975	.100	.082	.070	.070	.069	.065	.076	.067	.044	.047	.057	.066	.074	.088	.106
	1.000	.110	.085	.077	.077	.075	.067	.058	.070	.044	.047	.057	.070	.080	.093	.110

No crifices.

Dashed values.

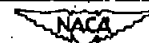


TABLE 7.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-505.30 PROPELLER BLADE SECTION ($x = 0.85$; $\beta_x = 41.10^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

		2.472	2.446	2.411	2.374	2.351	2.317	2.280	2.264	2.233	2.205	2.170	2.147	2.117
$\frac{J}{M}$.947	.956	.964	.972	.983	.989	.995	1.007	1.015	1.023	1.031	1.037	1.046
$c_{x'}$		-1.69	-1.39	-.98	-.54	-.26	.15	.61	.81	1.20	1.55	2.00	2.30	2.69
$\Delta\theta$		-1.37	-1.33	-1.28	-1.21	-1.17	-1.11	-1.03	-1.00	-.93	-.87	-.79	-.74	-.66
c_1		-.52	-.38	-.15	.06	.24	.43	.58	.73	.90	1.03	1.17	1.31	1.41
c_n		-.1426	-.1045	-.0413	.0168	.0658	.1174	.1568	.1974	.2426	.2787	.3174	.3529	.3794
c_m		-.1281	-.1336	-.1416	-.1580	-.1706	-.1742	-.1785	-.1898	-.1939	-.1925	-.1894	-.1917	-.1904
c_c		.0449	.0449	.0457	.0499	.0518	.0514	.0508	.0539	.0543	.0520	.0508	.0499	.0490
c/b		Pressure coefficient, P												
Upper surface	θ°	0.000	1.244	1.249	1.254	1.258	1.266	1.268	1.272	1.279	1.284	1.285	1.294	1.301
		.025	.712	.694	.655	.644	.637	.619	.597	.586	.568	.554	.535	.513
		.050	.461	.445	.414	.394	.386	.371	.348	.336	.319	.303	.286	.265
		.100	.255	.243	.215	.197	.194	.181	.160	.151	.137	.123	.112	.098
		.200	.050	.040	.016	0	.001	-.011	-.030	-.037	-.044	-.054	-.069	-.084
		.300	-.085	-.093	-.109	-.115	-.114	-.133	-.143	-.145	-.162	-.169	-.171	-.183
		.400	-.143	-.157	-.184	-.205	-.203	-.211	-.226	-.234	-.246	-.258	-.266	-.275
		.500	-.277	-.274	-.282	-.290	-.286	-.292	-.299	-.300	-.307	-.317	-.324	-.332
		.600	-.396	-.395	-.406	-.414	-.406	-.409	-.414	-.414	-.416	-.420	-.423	-.431
		.700	-.508	-.526	-.533	-.532	-.521	-.522	-.524	-.519	-.520	-.524	-.525	-.527
		.800	-.643	-.640	-.643	-.650	-.643	-.640	-.641	-.637	-.635	-.635	-.638	-.627
Lower surface		.900	-.849	-.895	-.849	-.683	-.795	-.795	-.758	-.793	-.788	-.784	-.778	-.775
		.950	-.801	-.832	-.886	-.744	-.821	-.877	-.855	-.805	-.828	-.822	-.815	-.812
		.0375	-.889	-.835	-.775	-.723	-.662	-.617	-.560	-.501	-.442	-.380	-.321	-.253
		.075	-.813	-.762	-.704	-.654	-.597	-.553	-.500	-.446	-.391	-.333	-.276	-.214
		.150	-.731	-.681	-.624	-.577	-.519	-.475	-.425	-.373	-.315	-.256	-.202	-.133
		.250	-.628	-.577	-.520	-.475	-.419	-.379	-.334	-.282	-.234	-.183	-.133	-.051
		.350	-.612	-.566	-.517	-.475	-.419	-.370	-.325	-.269	-.217	0	-.034	.060
		.450	-.545	-.496	-.440	-.346	-.220	-.076	-.016	-.018	-.017	.044	.073	.091
		.550	-.218	-.172	-.100	-.065	.002	.037	.037	.018	.025	.039	.052	.060
		.650	.033	.045	.042	.037	.040	.045	.037	.022	.010	.005	.009	.013
		.750	.085	.085	.072	.061	.063	.064	.060	.051	.043	.037	.035	.033
		.850	.086	.085	.074	.068	.072	.077	.078	.081	.081	.084	.087	.090
		.925	.073	.072	.066	.066	.077	.085	.093	.102	.109	.118	.127	.133
		.975	.074	.070	.068	.070	.077	.095	.110	.120	.127	.142	.154	.165
		1.000	.075	.071	.070	.076	.077	.100	.115	.130	.140	.160	.169	.182

^aNo crifice.^bPaired values.

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	1.579	1.739	1.876	1.983	2.114	2.255	2.379	2.505	2.635	2.712	2.667	2.578	2.445	2.313	2.170	2.053	1.913	1.806	1.649
J	1.579	1.739	1.876	1.983	2.114	2.255	2.379	2.505	2.635	2.712	2.667	2.578	2.445	2.313	2.170	2.053	1.913	1.806	1.649
M_x	.558	.571	.588	.596	.611	.627	.640	.653	.667	.679	.675	.662	.645	.628	.616	.602	.589	.579	.568
α_x	10.32	7.90	5.93	4.45	2.71	.92	-.58	-2.04	-3.49	-4.31	-3.83	-2.86	-1.36	.21	1.99	3.51	5.41	6.93	9.24
$\Delta\theta$	1.26	.99	.76	.56	.40	.12	-.12	-.36	-.61	-.76	-.68	-.50	-.24	.01	.29	.47	.70	.88	1.14
α_1	3.97	3.68	3.14	2.67	2.18	1.65	1.19	.66	.12	-.19	-.05	.35	.94	1.47	1.98	2.44	2.93	3.45	3.79
c_n	.8716	.8239	.6948	.6000	.4916	.3632	.2577	.1432	.0213	-.0510	-.0116	.0839	.2084	.3219	.4361	.5387	.6471	.7458	.8329
c_m	-.0513	-.0629	-.0801	-.0852	-.0878	-.0902	-.0918	-.0993	-.1057	-.1042	-.1073	-.1044	-.0955	-.0916	-.0890	-.0852	-.0814	-.0771	-.0523
c_c																			
a/b	Pressure coefficient, P																		
Upper surface	$a_0.000$	1.080	1.084	1.089	1.091	1.096	1.102	1.106	1.111	1.116	1.121	1.119	1.114	1.108	1.102	1.098	1.093	1.089	1.086
	.025	-1.770	-1.979	-1.183	-1.766	-1.364	-1.042	-1.311	-.491	-.617	-.677	-.649	-.562	-.416	-.170	-.170	-.554	-.923	-1.916
	.050	-1.715	-1.793	-.982	-.738	-.474	-.171	-.044	-.215	-.341	-.404	-.374	-.284	-.140	-.070	-.294	-.595	-.883	-1.302
	.100	-1.513	-1.283	-.822	-.662	-.483	-.284	-.131	-.002	-.109	-.166	-.138	-.061	-.058	-.216	-.393	-.547	-.751	-1.494
	.200	-.913	-.672	-.604	-.514	-.423	-.295	-.182	-.118	-.040	-.001	-.020	-.075	-.159	-.263	-.380	-.458	-.560	-.631
	.300	-.746	-.589	-.557	-.499	-.430	-.339	-.271	-.202	-.142	-.108	-.126	-.169	-.231	-.308	-.391	-.447	-.526	-.576
	.400	-.567	-.482	-.506	-.465	-.405	-.347	-.300	-.248	-.202	-.174	-.190	-.221	-.269	-.326	-.377	-.428	-.485	-.517
	.500	-.457	-.482	-.479	-.454	-.408	-.365	-.332	-.296	-.263	-.239	-.250	-.273	-.308	-.350	-.386	-.425	-.461	-.478
	.600	-.379	-.434	-.444	-.431	-.403	-.369	-.346	-.323	-.301	-.286	-.294	-.308	-.330	-.359	-.384	-.410	-.432	-.437
	.700	-.309	-.369	-.395	-.393	-.375	-.353	-.340	-.327	-.314	-.306	-.313	-.316	-.330	-.346	-.364	-.378	-.388	-.381
	.800	-.233	-.288	-.315	-.328	-.324	-.309	-.308	-.305	-.306	-.302	-.304	-.300	-.303	-.310	-.316	-.319	-.315	-.299
Lower surface	.900	-.153	-.138	-.149	-.165	-.172	-.169	-.176	-.179	-.190	-.194	-.192	-.179	-.172	-.173	-.170	-.164	-.151	-.143
	.950	-.109	-.037	-.026	-.027	-.027	-.023	-.031	-.036	-.047	-.055	-.051	-.037	-.028	-.028	-.024	-.023	-.021	-.029
	.0375	.707	.638	.525	.398	.229	.016	-.164	-.783	-.838	-.841	-.838	-.858	-.500	-.074	.113	.300	.475	.582
	.075	.580	.517	.419	.320	.198	.060	-.079	-.458	-.806	-.805	-.824	-.719	-.147	.008	.135	.258	.383	.469
	.150	.459	.410	.333	.259	.178	.114	.012	-.072	-.509	-.645	-.610	-.276	-.026	.067	.142	.217	.307	.371
	.250	.248	.297	.244	.187	.130	.084	.023	-.020	-.164	-.345	-.247	-.046	.003	.064	.120	.169	.221	.260
	.350	.299	.266	.216	.172	.128	.079	.027	-.011	-.050	-.155	-.081	-.016	.011	.055	.106	.151	.202	.240
	.450	.248	.230	.189	.153	.119	.084	.044	.011	-.005	-.048	-.017	.009	.031	.064	.102	.138	.177	.209
	.550	.217	.203	.169	.146	.121	.090	.057	.033	.020	.007	.018	.030	.050	.074	.110	.134	.164	.185
	.650	.162	.161	.134	.110	.090	.065	.040	.026	.022	.022	.023	.028	.038	.053	.077	.101	.126	.144
	.750	.139	.149	.130	.113	.101	.084	.066	.056	.049	.050	.050	.056	.065	.074	.093	.110	.128	.141
	.850	.117	.143	.130	.123	.119	.111	.098	.087	.080	.079	.078	.088	.097	.104	.115	.123	.131	.139
	.925	.113	.161	.156	.153	.156	.149	.139	.133	.122	.116	.119	.132	.142	.143	.153	.156	.158	.158
	.975	.119	.180	.180	.184	.185	.182	.163	.185	.160	.142	.150	.170	.184	.180	.185	.185	.180	.155
	a1.000	.125	.190	.197	.200	.200	.200	.180	.215	.180	.158	.169	.190	.210	.199	.210	.200	.197	.170

^aNo orifice.^bPaired values.

NACA

TABLE 8.—PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504,80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) — Continued(b) $N = 1350$ rpm.

$\frac{h}{h_0}$ $\frac{M_x}{M_0}$ $\frac{\Delta h}{\Delta h_0}$ α α_D α_M α_C	2.711 .798 -4.30 -1.27 -.31 -.0710 -.1147	2.635 .785 -3.48 -1.06 -.03 -.0058 -.1232	2.501 .765 -3.99 -.59 -.29 -.1692 -.1141	2.402 .749 -3.85 -.08 -.17 -.2619 -.1050	2.300 .737 -3.71 -.21 1.60 -.3568 -.1036	2.211 .724 -3.57 -.21 1.98 -.3768 -.1037	2.111 .712 -3.43 -.46 2.40 -.3955 -.0977	2.022 .700 -3.29 -.70 2.80 -.4146 -.0937	1.926 .691 -3.15 -.95 3.27 -.4332 -.0905	1.830 .679 -3.01 -1.20 3.76 -.4520 -.0775	1.733 .666 -2.87 -1.45 4.00 -.4708 -.0729	1.633 .658 -2.73 -1.66 4.08 -.4896 -.0754	1.533 .648 -2.59 -1.86 4.12 -.5084 -.0634	1.433 .637 -2.45 -2.06 3.94 -.5272 -.0724	1.333 .626 -2.31 -2.26 3.62 -.5460 -.0756	1.233 .616 -2.17 -2.46 3.02 -.5648 -.0870	1.133 .606 -2.03 -2.66 2.62 -.5836 -.0967	1.033 .596 -1.89 -2.86 2.16 -.6024 -.1035	.933 .586 -1.75 -3.06 1.60 -.6212 -.1023	.833 .576 -1.61 -3.26 1.19 -.6400 -.1032	.733 .566 -1.47 -3.46 .95 -.6588 -.1037	.633 .556 -1.33 -3.66 .75 -.6776 -.1201	.533 .546 -1.19 -3.86 .55 -.6964 -.1211	.433 .536 -1.05 -4.06 .35 -.7152 -.1245	.333 .526 -.91 -4.26 .15 -.7340 -.1245	.233 .516 -.77 -4.46 -.05 -.7528 -.1245	.133 .506 -.63 -4.66 -.25 -.7716 -.1245	.033 .496 -.49 -4.86 -.45 -.7904 -.1245	.000 .486 -.35 -5.06 -.65 -.8092 -.1245																																																																																											
o/b	Pressure coefficient, P																																																																																																																							
Upper surface	.00,000 .0025 .0050 .0100 .0200 .0300 .0400 .0500 .0600 .0700 .0800 .0900 .950	1.169 .737 .682 .195 .015 -.113 -.198 -.282 -.349 -.395 -.375 -.213 -.046	1.161 .682 .605 .195 -.027 -.149 -.227 -.299 -.354 -.389 -.336 -.192 -.026	1.155 .665 .565 .182 -.087 -.216 -.272 -.335 -.381 -.408 -.344 -.175 -.011	1.148 .644 .524 .167 -.102 -.235 -.298 -.353 -.398 -.426 -.361 -.161 0	1.144 .624 .494 .154 -.083 -.220 -.286 -.341 -.386 -.414 -.349 -.154 -.003	1.138 .604 .464 .144 -.072 -.211 -.277 -.332 -.377 -.405 -.340 -.146 -.006	1.134 .584 .434 .134 -.062 -.201 -.267 -.322 -.367 -.395 -.330 -.136 -.004	1.129 .564 .414 .114 -.052 -.191 -.257 -.312 -.357 -.385 -.320 -.126 -.004	1.125 .544 .394 .104 -.042 -.181 -.247 -.302 -.347 -.375 -.310 -.116 -.004	1.121 .524 .374 .094 -.032 -.171 -.237 -.292 -.337 -.365 -.300 -.106 -.014	1.116 .504 .354 .084 -.022 -.161 -.227 -.282 -.327 -.355 -.290 -.096 -.018	1.114 .484 .334 .074 -.012 -.151 -.217 -.272 -.317 -.345 -.280 -.086 -.065	1.116 .464 .314 .064 -.002 -.141 -.207 -.262 -.307 -.335 -.270 -.076 -.090	1.119 .444 .294 .054 -.002 -.121 -.187 -.242 -.287 -.315 -.250 -.056 -.011	1.123 .424 .274 .044 -.002 -.101 -.167 -.222 -.267 -.295 -.230 -.042 -.004	1.128 .404 .254 .034 -.002 -.081 -.147 -.202 -.247 -.275 -.210 -.038 -.005	1.132 .384 .234 .024 -.002 -.061 -.127 -.182 -.227 -.255 -.190 -.034 -.005	1.137 .364 .214 .014 -.002 -.041 -.107 -.162 -.207 -.235 -.170 -.028 -.007	1.142 .344 .194 .004 -.002 -.021 -.087 -.142 -.187 -.215 -.150 -.024 -.003	1.146 .324 .174 -.002 -.002 -.001 -.067 -.122 -.167 -.195 -.130 -.020 -.004	1.153 .304 .154 -.002 -.002 -.002 -.047 -.102 -.147 -.175 -.110 -.018 -.006	1.160 .284 .134 -.002 -.002 -.002 -.027 -.082 -.127 -.155 -.090 -.014 -.006	1.164 .264 .114 -.002 -.002 -.002 -.007 -.062 -.107 -.135 -.070 -.010 -.014	1.168 .244 .094 -.002 -.002 -.002 -.001 -.042 -.087 -.115 -.050 -.008 -.027																																																																																															
Lower surface	.0375 .075 .150 .250 .350 .450 .550 .650 .750 .850 .925 .975 1.000	.049 .093 .160 .246 .336 .424 .509 .589 .664 .734 .794 .844 .884	.054 .098 .165 .251 .341 .429 .514 .594 .669 .739 .799 .849 .889	.061 .105 .172 .258 .348 .436 .521 .601 .676 .746 .806 .856 .896	.068 .112 .179 .265 .355 .443 .528 .608 .683 .753 .813 .863 .903	.075 .119 .186 .272 .362 .450 .535 .615 .690 .760 .820 .870 .910	.082 .126 .193 .279 .369 .457 .542 .622 .697 .767 .827 .877 .917	.089 .133 .200 .286 .376 .464 .549 .629 .704 .774 .834 .884 .924	.096 .140 .207 .293 .383 .471 .556 .636 .711 .781 .841 .891 .931	.103 .147 .214 .300 .390 .478 .563 .643 .718 .788 .848 .898 .938	.110 .154 .221 .307 .397 .485 .570 .650 .725 .795 .855 .905 .945	.117 .161 .228 .314 .404 .492 .577 .657 .732 .802 .862 .912 .952	.124 .168 .235 .321 .411 .499 .584 .664 .739 .809 .869 .919 .959	.131 .175 .242 .328 .418 .506 .591 .671 .746 .816 .876 .926 .966	.138 .182 .249 .335 .425 .513 .598 .678 .753 .823 .883 .933 .973	.145 .189 .256 .342 .432 .520 .605 .685 .760 .830 .890 .940 .980	.152 .196 .263 .349 .439 .527 .612 .692 .767 .837 .897 .947 .987	.159 .203 .270 .356 .446 .534 .619 .699 .774 .844 .904 .954 .994	.166 .210 .277 .363 .453 .541 .626 .706 .781 .851 .911 .961 1.001	.173 .217 .284 .370 .460 .548 .633 .713 .788 .858 .918 .968 1.008	.180 .224 .291 .377 .467 .555 .640 .720 .795 .865 .925 .975 1.015	.187 .231 .298 .384 .474 .562 .647 .727 .802 .872 .932 .982 1.022	.194 .238 .305 .391 .481 .569 .654 .734 .809 .879 .939 .989 1.029	.201 .245 .312 .398 .488 .576 .661 .741 .816 .886 .946 .996 1.036	.208 .252 .319 .405 .495 .583 .668 .748 .823 .893 .953 1.003 1.043	.215 .259 .326 .412 .502 .590 .675 .755 .830 .900 .960 1.010 1.050	.222 .266 .333 .419 .509 .597 .682 .762 .837 .907 .967 1.017 1.057	.229 .273 .340 .426 .516 .604 .689 .769 .844 .914 .974 1.024 1.064	.236 .280 .347 .433 .523 .611 .696 .776 .851 .921 .981 1.031 1.071	.243 .287 .354 .440 .530 .618 .703 .783 .858 .928 .988 1.038 1.078	.250 .294 .361 .447 .537 .625 .710 .790 .865 .935 .995 1.045 1.085	.257 .301 .368 .454 .544 .632 .717 .797 .872 .942 1.002 1.052 1.092	.264 .308 .375 .461 .551 .639 .724 .804 .879 .949 1.009 1.059 1.099	.271 .315 .382 .468 .558 .646 .731 .811 .886 .956 1.016 1.066 1.106	.278 .322 .389 .475 .565 .653 .738 .818 .893 .963 1.023 1.073 1.113	.285 .329 .396 .482 .572 .660 .745 .825 .900 .970 1.030 1.080 1.120	.292 .336 .403 .489 .579 .667 .752 .832 .907 .977 1.037 1.087 1.127	.299 .343 .410 .496 .586 .674 .759 .839 .914 .984 1.044 1.094 1.134	.306 .350 .417 .503 .593 .681 .766 .846 .921 .991 1.051 1.101 1.141	.313 .357 .424 .510 .600 .688 .773 .853 .928 .998 1.058 1.108 1.148	.320 .364 .431 .517 .607 .695 .780 .860 .935 1.005 1.065 1.105	.327 .371 .438 .524 .614 .702 .787 .867 .942 1.012 1.072 1.112	.334 .378 .445 .531 .621 .709 .794 .874 .949 1.019 1.079 1.119	.341 .385 .452 .538 .628 .716 .801 .881 .956 1.026 1.086 1.126	.348 .392 .459 .545 .635 .723 .808 .888 .963 1.033 1.093 1.133	.355 .399 .466 .552 .642 .730 .815 .895 .970 1.040 1.100 1.140	.362 .406 .473 .559 .649 .737 .822 .902 .977 1.047 1.107 1.147	.369 .413 .480 .566 .656 .744 .829 .909 .984 1.054 1.114 1.154	.376 .420 .487 .573 .663 .751 .836 .916 .991 1.061 1.121 1.161	.383 .427 .494 .580 .670 .758 .843 .923 .998 1.068 1.128 1.168	.390 .434 .501 .587 .677 .765 .850 .930 .1.005 1.075 1.115 1.155	.397 .441 .508 .594 .684 .772 .857 .937 1.012 1.082 1.122 1.162	.404 .448 .515 .601 .691 .779 .864 .944 1.019 1.089 1.129 1.169	.411 .455 .522 .608 .698 .786 .871 .951 1.026 1.096 1.136 1.176	.418 .462 .529 .615 .705 .793 .878 .958 1.033 1.103 1.143 1.183	.425 .469 .536 .622 .712 .800 .885 .965 1.040 1.110 1.150 1.190	.432 .476 .543 .629 .719 .807 .892 .972 1.047 1.117 1.157 1.197	.439 .483 .550 .636 .726 .814 .900 .980 1.055 1.125 1.165 1.205	.446 .490 .557 .643 .733 .821 .906 .986 1.061 1.131 1.171 1.211	.453 .497 .564 .650 .740 .828 .913 .993 1.068 1.138 1.178 1.218	.460 .504 .571 .657 .747 .835 .920 .1.000 1.075 1.115 1.155	.467 .511 .578 .664 .754 .842 .927 1.007 1.082 1.122 1.162	.474 .518 .585 .671 .761 .849 .934 1.014 1.089 1.129 1.169	.481 .525 .592 .678 .768 .856 .941 1.021 1.096 1.136 1.176	.488 .532 .599 .685 .775 .863 .948 1.028 1.103 1.143 1.183	.495 .539 .606 .692 .782 .870 .955 1.035 1.110 1.150 1.190	.502 .546 .613 .700 .790 .878 .963 1.043 1.118 1.158 1.198	.509 .553 .620 .706 .796 .884 .969 1.049 1.124 1.164 1.204	.516 .560 .627 .713 .803 .891 .976 1.056 1.131 1.171 1.211	.523 .567 .634 .720 .810 .898 .983 1.063 1.138 1.178 1.218	.530 .574 .641 .727 .817 .905 .990 1.070 1.145 1.185 1.225	.537 .581 .648 .734 .824 .912 .997 1.077 1.147 1.187 1.227	.544 .588 .655 .741 .831 .919 .1.004 1.084 1.124 1.164	.551 .595 .662 .748 .838 .926 1.011 1.091 1.131 1.171	.558 .602 .669 .755 .845 .933 1.018 1.098 1.138 1.178	.565 .609 .676 .762 .852 .940 1.025 1.105 1.145 1.185	.572 .616 .683 .769 .859 .947 1.032 1.112 1.152 1.192	.579 .623 .690 .776 .866 .954 1.039 1.119 1.159 1.199	.586 .630 .697 .783 .873 .961 1.046 1.126 1.166 1.206	.593 .637 .704 .790 .880 .968 1.053 1.133 1.173 1.213	.600 .644 .711 .797 .887 .975 1.060 1.140 1.180 1.220	.607 .651 .718 .804 .894 .982 1.067 1.147 1.187 1.227	.614 .658 .725 .811 .901 .989 1.074 1.154 1.194 1.234	.621 .665 .732 .818 .908 .996 1.081 1.161 1.201 1.241	.628 .672 .739 .825 .915 .1.003 1.088 1.168 1.208 1.248	.635 .679 .746 .832 .922 1.010 1.095 1.175 1.215 1.255	.642 .686 .753 .839 .929 1.017 1.102 1.182 1.222 1.262	.649 .693 .760 .846 .936 1.024 1.109 1.189 1.229 1.269	.656 .700 .767 .853 .943 1.031 1.116 1.196 1.236 1.276	.663 .707 .774 .860 .950 1.038 1.123 1.203 1.243 1.283	.670 .714 .781 .867 .957 1.045 1.130 1.210 1.250 1.290	.677 .721 .788 .874 .964 1.052 1.137 1.217 1.257 1.297	.684 .728 .795 .881 .971 1.058 1.144 1.224 1.264 1.304	.691 .735 .802 .888 .978 1.065 1.151 1.231 1.271 1.311	.698 .742 .809 .895 .985 1.072 1.157 1.237 1.277 1.317	.705 .749 .816 .902 .992 1.079 1.164 1.244 1.284 1.324	.712 .756 .823 .909 .999 1.086 1.172 1.252 1.292 1.332	.719 .763 .830 .916 .1.006 1.092 1.178 1.258 1.298 1.338	.726 .770 .837 .923 1.013 1.100 1.186 1.266 1.306 1.346	.733 .777 .844 .930 1.020 1.106 1.192 1.272 1.312 1.352	.740 .784 .851 .937 1.027 1.113 1.200 1.280 1.320 1.360	.747 .791 .858 .944 1.034 1.120 1.206 1.286 1.326 1.366	.754 .798 .865 .951 1.041 1.127 1.213 1.293 1.333 1.373	.761 .805 .872 .958 1.048 1.134 1.220 1.300 1.340 1.380	.768 .812 .879 .965 1.055 1.141 1.227 1.307 1.347 1.387	.775 .819 .886 .972 1.062 1.148 1.234 1.314 1.354 1.394	.782 .826 .893 .979 1.069 1.155 1.241 1.321 1.361 1.401	.789 .833 .900 .986 1.076 1.162 1.248 1.328 1.368 1.408	.796 .840 .907 .993 1.083 1.169 1.255 1.335 1.375 1.415	.803 .847 .914 .1.000 1.090 1.176 1.262 1.342 1.382 1.422	.810 .854 .921 1.007 1.097 1.183 1.269 1.349 1.389 1.429	.817 .861 .928 1.014 1.104 1.190 1.276 1.356 1.396 1.436	.824 .868 .935 1.021 1.111 1.197 1.283 1.363 1.403 1.443	.831 .875 .942 1.028 1.118 1.204 1.290 1.370 1.410 1.450	.838 .882 .949 1.035 1.125 1.211 1.297 1.377 1.417 1.457	.845 .889 .956 1.042 1.132 1.218 1.304 1.384 1.424 1.464	.852 .896 .963 1.049 1.139 1.225 1.311 1.391 1.431 1.471	.859 .903 .970 1.056 1.146 1.232 1.318 1.398 1.438 1.478	.866 .910 .977 1.063 1.153 1.239 1.325 1.405 1.445 1.485	.873 .917 .984 1.07

$\beta_{0.75R} = 45^\circ$; B = 2) - Continued.

(c) $N = 1500$ rpm.

J	2.004	2.059	2.153	2.218	2.304	2.392	2.476	2.563	2.634	2.596	2.523	2.438	2.352	2.261	2.186	2.106	2.048	
M _x	.783	.793	.807	.817	.828	.842	.858	.874	.885	.877	.867	.851	.837	.821	.813	.798	.791	
α ₁	4.17	3.44	2.21	1.39	.32	-.73	-1.71	-2.69	-3.47	-3.03	-2.24	-1.27	-.26	.85	1.79	2.82	3.43	
Δθ	1.02	.81	.46	.21	-.11	-.45	-.81	-1.22	-1.58	-1.39	-1.03	-.64	-.29	.05	.33	.64	.85	
α ₂	3.01	2.72	2.41	2.03	1.63	1.23	.78	.34	-.31	-.07	.51	.98	1.38	1.93	2.24	2.59	2.83	
α ₃	.6697	.6065	.5384	.4555	.3642	.2768	.1742	.0768	-.0690	-.0161	.1148	.2200	.3090	.4310	.5000	.5790	.6290	
α ₄	-.1000	-.1037	-.1104	-.1112	-.1155	-.1229	-.1434	-.1619	-.1632	-.1598	-.1555	-.1298	-.1184	-.1139	-.1084	-.1077	-.1016	
α ₅							.0288	.0343	.0391	.0369	.0320	.0247						
α/b	Pressure coefficient, P																	
Upper surface	0.000	1.163	1.167	1.173	1.178	1.183	1.189	1.197	1.205	1.211	1.207	1.202	1.194	1.187	1.180	1.176	1.169	1.166
	.025	-.505	-.317	-.045	.146	.353	.497	.604	.691	.760	.729	.650	.559	.434	.252	.043	-.192	-.375
	.050	-.743	-.547	-.301	-.130	.064	.205	.319	.413	.488	.454	.367	.271	.142	-.031	-.221	-.430	-.611
	.100	-.842	-.710	-.448	-.306	-.149	-.022	.084	.168	.239	.205	.128	.033	-.082	-.229	-.380	-.591	-.759
	.200	-.714	-.667	-.537	-.370	-.268	-.172	-.089	-.018	.045	.014	-.052	-.127	-.217	-.320	-.424	-.605	-.677
	.300	-.552	-.450	-.484	-.447	-.372	-.294	-.225	-.168	-.110	-.138	-.192	-.275	-.331	-.410	-.472	-.606	-.427
	.400	-.479	-.524	-.491	-.464	-.423	-.371	-.312	-.265	-.219	-.242	-.285	-.340	-.397	-.445	-.481	-.510	.516
	.500	-.533	-.545	-.527	-.516	-.486	-.438	-.400	-.368	-.337	-.356	-.380	-.416	-.459	-.496	-.522	-.534	-.546
	.600	-.515	-.524	-.512	-.499	-.503	-.500	-.473	-.443	-.441	-.442	-.456	-.487	-.507	-.489	-.508	-.520	-.522
	.700	-.463	-.473	-.482	-.498	-.534	-.523	-.512	-.493	-.503	-.488	-.498	-.519	-.523	-.523	-.492	-.478	-.472
Lower surface	.800	-.344	-.350	-.346	-.348	-.342	-.334	-.315	-.288	-.267	-.262	-.280	-.387	-.334	-.347	-.349	-.349	-.348
	.900	-.128	-.130	-.123	-.125	-.124	-.115	-.101	-.080	-.067	-.076	-.086	-.107	-.118	-.123	-.126	-.128	-.129
	.950	.013	.012	.020	.022	.023	.032	.038	.041	.046	.044	.045	.038	.031	.025	.018	.017	.012
	.0375	.397	.308	.164	.033	-.098	-.283	-1.045	-1.093	-1.154	-1.164	-1.100	-1.021	-.544	-.050	.099	.237	.334
	.075	.363	.264	.164	.086	-.025	-.268	-.965	-1.026	-1.080	-1.070	-1.004	-.883	-.032	.044	.121	.223	.291
	.150	.287	.235	.194	.145	.055	.037	-.292	-.822	-.924	-.914	-.780	.026	.038	.104	.175	.207	.254
	.250	.046	.085	.159	.121	.062	.035	.067	-.213	-.814	-.631	.027	.045	.047	.095	.138	.120	.053
	.350	.200	.167	.133	.100	.056	.035	.044	.095	-.234	-.091	.070	.034	.046	.083	.116	.154	.179
	.450	.185	.158	.129	.102	.069	.051	.051	.091	-.005	.088	.068	.049	.056	.090	.114	.146	.169
	.550	.174	.151	.129	.107	.081	.068	.063	.090	.112	.109	.076	.066	.076	.098	.117	.144	.161
b	.650	.131	.109	.093	.078	.057	.049	.045	.062	.103	.079	.055	.049	.055	.071	.084	.103	.118
	.750	.137	.121	.110	.102	.085	.080	.077	.085	.111	.093	.084	.080	.084	.095	.104	.119	.128
	.850	.151	.140	.134	.127	.118	.118	.114	.117	.130	.120	.121	.119	.119	.127	.129	.139	.145
	.925	.185	.177	.174	.169	.164	.166	.161	.161	.163	.162	.167	.166	.166	.169	.170	.177	.180
	a, 1.000	.213	.206	.206	.197	.198	.207	.201	.204	.196	.207	.200	.208	.205	.204	.210	.211	.214
a	.228	.223	.224	.213	.217	.230	.223	.226	.212	.228	.219	.230	.227	.223	.232	.229	.232	

^aNo orifice.^b Paired value.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(d) $N = 1600$ rpm.

	J	2.103	2.170	2.240	2.295	2.352	2.410	2.457	2.509	2.561	2.554	2.499	2.439	2.389	2.337	2.275	2.224	2.161
M_x		.856	.866	.876	.885	.896	.908	.916	.924	.934	.933	.923	.908	.902	.892	.881	.873	.860
α_T		2.86	1.99	1.11	.43	-.26	-.94	-1.49	-2.08	-2.67	-2.99	-1.97	-1.28	-.70	-.08	.68	1.31	2.11
$\Delta\theta$.86	.52	.17	-.11	-.40	-.70	-.93	-1.17	-1.33	-1.31	-1.13	-.84	-.59	-.33	-.01	.25	.57
α_1		2.69	2.30	1.98	1.64	1.30	.89	.56	-.06	-.51	-.53	.09	.65	.99	1.37	1.79	1.98	2.32
c_m		.6003	.5142	.4426	.3687	.2910	.1994	.1251	-.0148	-.1155	-.1194	.0194	.1465	.2226	.3077	.4006	.4432	.5194
c_{m0}		-.1209	-.1211	-.1237	-.1355	-.1481	-.1542	-.1588	-.1504	-.1393	-.1404	-.1581	-.1586	-.1547	-.1424	-.1288	-.1216	-.1180
c_o		.0009	.0083	.0144	.0214	.0274	.0321	.0362	.0397	.0420	.0414	.0394	.0344	.0308	.0263	.0191	.0124	.0058
c/b	Pressure coefficient, P																	
Upper surface	0.000	1.196	1.201	1.206	1.211	1.217	1.223	1.227	1.231	1.237	1.237	1.231	1.223	1.220	1.215	1.209	1.204	1.198
	.025	-.008	.178	.317	.428	.516	.593	.610	.716	.761	.757	.705	.632	.566	.500	.395	.276	.121
	.050	-.261	-.098	.070	.139	.230	.311	.334	.445	.494	.491	.432	.352	.282	.215	.107	-.007	-.149
	.100	-.451	-.288	-.174	-.081	.002	.077	.099	.208	.254	.252	.194	.118	.051	-.014	-.111	-.208	-.334
	.200	-.543	-.447	-.354	-.219	-.154	-.091	-.081	.023	.065	.064	.010	-.057	-.113	-.165	-.245	-.385	-.464
	.300	-.612	-.495	-.407	-.347	-.287	-.230	-.228	-.129	-.088	-.089	-.139	-.202	-.249	-.295	-.363	-.424	-.520
	.400	-.647	-.571	-.496	-.431	-.387	-.334	-.328	-.231	-.195	-.197	-.242	-.303	-.355	-.388	-.439	-.511	-.594
	.500	-.663	-.579	-.524	-.503	-.463	-.438	-.444	-.359	-.323	-.324	-.368	-.413	-.448	-.466	-.514	-.555	-.577
	.600	-.663	-.616	-.582	-.561	-.520	-.516	-.537	-.451	-.416	-.416	-.458	-.506	-.503	-.524	-.566	-.597	-.615
	.700	-.675	-.658	-.641	-.620	-.591	-.569	-.617	-.540	-.507	-.505	-.544	-.581	-.573	-.598	-.625	-.650	-.659
	.800	-.240	-.307	-.380	-.524	-.644	-.655	-.711	-.699	-.633	-.632	-.666	-.647	-.671	-.627	-.473	-.355	-.275
	.900	-.062	-.064	-.073	-.091	-.103	-.105	-.164	-.133	-.139	-.132	-.124	-.105	-.103	-.093	-.077	-.065	-.063
	.950	.026	.002	-.018	-.042	-.061	-.062	-.134	-.104	-.108	-.102	-.096	-.065	-.059	-.044	0	0	.021
Lower surface	.0375	.202	.081	-.023	-.402	-.654	-.804	-.908	-.916	-.941	-.962	-.948	-.902	-.847	-.771	-.638	-.534	.103
	.075	.205	.113	.057	.006	-.613	-.765	-.862	-.864	-.888	-.893	-.870	-.823	-.767	-.618	.015	.072	.135
	.150	.226	.173	.119	.073	.051	-.535	-.713	-.727	-.754	-.765	-.739	-.689	-.648	.076	.076	.128	.189
	.250	.141	.122	.095	.062	.073	.068	-.471	-.638	-.676	-.684	-.650	-.603	.088	.042	.074	.099	.121
	.350	.153	.116	.091	.056	.054	.086	.002	-.509	-.648	-.664	-.614	.096	.066	.049	.065	.071	.124
	.450	.146	.115	.095	.065	.060	.077	.067	-.008	-.400	-.332	.061	.097	.064	.058	.074	.096	.120
	.550	.141	.116	.101	.074	.064	.075	.058	-.108	-.002	-.007	.123	.088	.066	.066	.081	.101	.121
	.650	.101	.080	.067	.042	.033	.037	.011	.099	.082	.088	.089	.048	.033	.033	.051	.067	.084
	.750	.116	.098	.087	.065	.055	.057	.020	.092	.112	.115	.084	.063	.054	.060	.074	.089	.103
	.850	.138	.122	.112	.092	.082	.082	.035	.089	.107	.107	.089	.085	.081	.087	.099	.115	.127
	.925	.174	.156	.145	.122	.114	.112	.057	.099	.103	.106	.103	.110	.111	.118	.134	.150	.165
	.975	.202	.183	.173	.154	.139	.137	.077	.105	.096	.106	.120	.130	.138	.141	.167	.178	.197
	1.000	.218	.198	.187	.169	.152	.153	.089	.110	.093	.107	.130	.140	.150	.155	.184	.192	.215

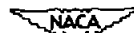
^aNo orifices.^bPaired values.

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $M = 0.56$.

J	2.677	2.641	2.588	2.547	2.512	2.482	2.429	2.398	2.346	2.316	2.281	2.254	2.221	2.185	2.159	2.127
M_x	.826	.832	.837	.849	.855	.864	.872	.878	.885	.896	.900	.911	.920	.927	.938	.946
α_x	-3.93	-3.55	-2.97	-2.51	-2.12	-1.78	-1.16	-1.80	-1.18	.18	.61	.94	1.35	1.80	2.13	2.55
$\Delta\beta$	-1.32	-1.26	-1.13	-1.01	-.90	-.81	-.63	-.50	-.34	-.29	-.25	-.22	-.16	-.08	0	.14
α_1	-.29	-.08	.11	.37	.55	.70	1.00	1.12	1.37	1.45	1.57	1.76	1.82	1.98	2.08	2.28
c_n	-.0645	-.0174	.0258	.0839	.1226	.1574	.2245	.2516	.3058	.3239	.3503	.3942	.4055	.4423	.4655	.5090
c_m	-.1262	-.1427	-.1442	-.1462	-.1491	-.1542	-.1442	-.1501	-.1490	-.1436	-.1424	-.1427	-.1408	-.1431	-.1463	-.1496
c_o				.0323	.0321	.0308	.0284	.0272	.0265	.0263	.0260	.0252	.0245	.0244	.0243	.0236
o/b	Pressure coefficient, P															
Upper surface	$\alpha_0.000$	1.182	1.185	1.187	1.193	1.196	1.200	1.204	1.207	1.211	1.217	1.219	1.225	1.230	1.234	1.239
	.025	.752	.738	.711	.677	.653	.628	.579	.555	.512	.493	.466	.444	.419	.390	.374
	.050	.481	.462	.432	.398	.372	.347	.297	.273	.228	.211	.185	.164	.142	.116	.103
	.100	.227	.207	.176	.147	.124	.104	.056	.036	-.007	-.022	-.046	-.062	-.081	-.102	-.114
	.200	.028	.010	-.011	-.035	-.055	-.072	-.110	-.128	-.163	-.175	-.194	-.240	-.280	-.301	-.308
	.300	-.105	-.123	-.143	-.170	-.191	-.206	-.241	-.259	-.286	-.297	-.313	-.322	-.329	-.346	-.356
	.400	-.204	-.221	-.237	-.259	-.277	-.297	-.317	-.330	-.366	-.387	-.411	-.420	-.432	-.439	-.445
	.500	-.296	-.314	-.337	-.364	-.376	-.385	-.419	-.431	-.451	-.454	-.480	-.513	-.528	-.535	-.539
	.600	-.367	-.384	-.406	-.404	-.437	-.454	-.486	-.514	-.523	-.526	-.538	-.537	-.556	-.576	-.599
	.700	-.445	-.467	-.498	-.508	-.518	-.518	-.549	-.561	-.556	-.591	-.604	-.604	-.613	-.622	-.631
	.800	-.492	-.510	-.535	-.563	-.571	-.610	-.643	-.663	-.675	-.674	-.682	-.686	-.681	-.660	-.664
	.900	-.501	-.512	-.555	-.527	-.513	-.085	-.063	-.059	-.075	-.101	-.127	-.145	-.168	-.188	-.218
	.950	-.026	.007	.019	.034	.037	.050	.049	.032	-.010	-.051	-.087	-.112	-.139	-.165	-.199
Lower surface	.0375	-1.041	-1.348	-1.284	-1.200	-1.142	-1.063	-.973	-.915	-.819	-.717	-.633	-.503	-.362	-.158	-.061
	.075	-.910	-1.218	-1.174	-1.091	-1.040	-.966	-.862	-.798	-.668	-.504	-.311	-.037	.066	.078	.094
	.150	-.647	-.755	-.770	-.719	-.640	-.529	-.404	-.283	-.035	.021	.042	.101	.109	.137	.154
	.250	-.413	-.302	-.259	-.005	.051	.083	.084	.079	.070	.079	.077	.088	.098	.121	.132
	.350	-.246	.005	.056	.060	.059	.063	.059	.057	.054	.063	.063	.074	.081	.102	.109
	.450	-.116	.046	.058	.060	.059	.065	.065	.064	.063	.070	.068	.079	.083	.100	.107
	.550	-.028	.059	.066	.069	.068	.074	.076	.075	.072	.078	.074	.082	.084	.099	.103
	.650	.020	.051	.053	.055	.051	.055	.056	.051	.045	.045	.038	.042	.044	.052	.054
	.750	.062	.080	.083	.085	.083	.086	.086	.081	.072	.068	.058	.059	.057	.065	.069
	.850	.098	.119	.121	.126	.124	.127	.125	.118	.105	.097	.083	.082	.077	.082	.081
	.925	.135	.162	.168	.171	.170	.171	.169	.159	.142	.129	.111	.106	.098	.102	.096
	.975	.215	.211	.220	.216	.209	.216	.195	.199	.174	.150	.120	.125	.111	.121	.108
	1.000	.298	.245	.250	.248	.230	.240	.210	.225	.189	.162	.130	.140	.118	.134	.115

^aNo orifice.^bPaired value.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(r) $M = 0.58$.

J	2.637	2.585	2.544	2.512	2.476	2.424	2.391	2.354	2.319	2.280	2.249	2.220	2.185	2.149
M_x	.863	.870	.877	.887	.894	.905	.912	.920	.929	.935	.946	.954	.961	.972
α_x	-3.50	-2.94	-2.48	-2.12	-1.71	-1.11	-.72	-.28	.14	.62	1.00	1.36	1.80	2.26
$\Delta\theta$	-1.42	-1.24	-1.09	-.97	-.86	-.73	-.68	-.64	-.61	-.52	-.41	-.29	-.11	.10
α_1	-.21	0	.16	.30	.47	.69	.85	.97	1.10	1.26	1.44	1.58	1.77	1.99
α_n	-.0465	0	.0348	.0665	.1065	.1542	.1890	.2168	.2452	.2816	.3219	.3542	.3945	.4413
α_m	-.1558	-.1552	-.1540	-.1557	-.1562	-.1540	-.1513	-.1534	-.1534	-.1526	-.1533	-.1513	-.1541	-.1560
c_c	.0383	.0363	.0350	.0341	.0336	.0326	.0322	.0320	.0318	.0305	.0308	.0294	.0294	.0286
c/d	Pressure coefficient, P													
Upper surface	α_0	1.200	1.203	1.207	1.212	1.216	1.222	1.225	1.230	1.235	1.238	1.244	1.249	1.252
	.025	.757	.727	.703	.678	.661	.617	.594	.580	.561	.530	.518	.487	.430
	.050	.485	.452	.426	.399	.380	.335	.314	.298	.282	.250	.239	.211	.160
	.100	.236	.208	.186	.162	.146	.105	.084	.073	.059	.030	.022	0	-.046
	.200	.039	.015	-.006	-.025	-.038	-.071	-.085	-.092	-.101	-.122	-.148	-.204	-.247
	.300	-.113	-.137	-.155	-.172	-.186	-.214	-.223	-.228	-.235	-.251	-.255	-.265	-.304
	.400	-.220	-.241	-.260	-.279	-.286	-.313	-.329	-.336	-.342	-.360	-.361	-.373	-.397
	.500	-.335	-.352	-.363	-.390	-.407	-.424	-.434	-.446	-.454	-.467	-.468	-.476	-.492
	.600	-.437	-.425	-.437	-.461	-.487	-.508	-.518	-.524	-.529	-.543	-.547	-.560	-.574
	.700	-.490	-.481	-.493	-.509	-.534	-.562	-.573	-.576	-.583	-.584	-.585	-.589	-.603
	.800	-.598	-.603	-.621	-.630	-.626	-.646	-.647	-.648	-.655	-.664	-.664	-.667	-.683
	.900	-.104	-.085	-.067	-.060	-.067	-.092	-.114	-.133	-.154	-.179	-.210	-.231	-.267
	.950	.039	.045	.046	.026	.001	-.042	-.075	-.100	-.127	-.153	-.183	-.204	-.236
Lower surface	α_0	-.0375	-1.235	-1.182	-1.116	-1.042	-.988	-.908	-.841	-.766	-.632	-.561	-.474	-.359
	.075	-1.142	-1.084	-1.021	-.951	-.902	-.827	-.764	-.694	-.635	-.548	-.479	-.312	-.076
	.150	-.992	-.928	-.866	-.799	-.733	-.679	-.610	-.506	-.375	-.049	.081	.126	.136
	.250	-.390	-.345	-.286	-.253	-.214	0	.060	.099	.106	.103	.105	.106	.117
	.350	-.159	-.065	.019	.064	.083	.093	.090	.090	.087	.082	.083	.087	.098
	.450	.042	.080	.099	.103	.102	.087	.080	.081	.080	.079	.082	.087	.097
	.550	.096	.098	.100	.099	.095	.080	.075	.079	.078	.078	.083	.086	.094
	.650	.057	.076	.074	.070	.062	.044	.037	.037	.034	.032	.034	.037	.044
	.750	.097	.093	.093	.088	.080	.063	.054	.053	.050	.049	.049	.054	.059
	.850	.124	.123	.122	.115	.107	.089	.078	.075	.069	.069	.068	.076	.082
	.925	.162	.160	.160	.149	.138	.118	.104	.101	.093	.091	.090	.097	.105
	.975	.189	.180	.188	.178	.162	.140	.124	.128	.117	.108	.108	.112	.137
	$\alpha_{1.000}$.202	.192	.202	.191	.178	.150	.134	.138	.129	.117	.116	.120	.147

^aNo orifice.^bPaired value.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN
NACA 16-504.80 PROPELLER BLADE SECTION ($\alpha = 0.90$; $\beta_x = 39.50^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued

(g) $M = 0.60$.

	2.611	2.563	2.522	2.485	2.445	2.405	2.374	2.344	2.303	2.271	2.253	2.209	2.167	2.150	2.131
J	.901	.905	.913	.921	.929	.939	.945	.957	.963	.971	.984	.986	.993	1.003	1.009
M_x	-3.22	-2.69	-2.23	-1.81	-1.35	-.88	-.52	-.16	.34	.73	.95	1.50	2.03	2.25	2.49
Δp	-1.43	-1.35	-1.29	-1.24	-1.18	-1.07	-.97	-.86	-.69	-.58	-.52	-.41	-.38	-.37	-.37
α_1	-.38	-.21	-.08	.14	.27	.44	.54	.74	.99	1.08	1.29	1.60	1.78	1.95	2.05
c_n	-.0845	-.0477	-.0174	.0310	.0613	.0981	.1213	.1645	.2206	.2419	.2890	.3568	.3961	.4355	.4568
c_m	-.1496	-.1542	-.1531	-.1583	-.1647	-.1568	-.1563	-.1594	-.1570	-.1601	-.1668	-.1703	-.1799	-.1953	-.1981
c_d	.0400	.0393	.0393	.0387	.0385	.0377	.0377	.0379	.0362	.0366	.0375	.0377	.0403	.0424	.0423
a/b	Pressure coefficient, P														
Upper surface	0.000	1.220	1.222	1.226	1.230	1.235	1.240	1.244	1.250	1.254	1.258	1.265	1.264	1.275	1.280
	.025	.775	.748	.726	.700	.662	.646	.630	.597	.582	.567	.546	.520	.506	.504
	.050	.506	.476	.454	.431	.401	.388	.371	.356	.323	.309	.296	.275	.251	.239
	.100	.262	.234	.216	.209	.243	.157	.145	.131	.102	.092	.082	.062	.042	.035
	.200	.063	.043	.027	.069	.059	-.015	-.023	-.032	-.051	-.061	-.102	-.141	-.165	-.107
	.300	-.091	-.112	-.124	-.082	-.090	-.155	-.161	-.167	-.184	-.190	-.192	-.204	-.225	-.170
	.400	-.202	-.228	-.231	-.187	-.195	-.263	-.271	-.276	-.295	-.297	-.300	-.311	-.325	-.271
	.500	-.320	-.344	-.356	-.316	-.315	-.378	-.385	-.391	-.404	-.404	-.404	-.413	-.425	-.370
	.600	-.423	-.434	-.448	-.408	-.412	-.464	-.470	-.474	-.489	-.490	-.492	-.504	-.515	-.461
	.700	-.521	-.532	-.533	-.499	-.499	-.549	-.549	-.550	-.561	-.560	-.558	-.570	-.583	-.535
	.800	-.640	-.653	-.657	-.618	-.621	-.667	-.663	-.659	-.664	-.658	-.652	-.656	-.661	-.613
Lower surface	.900	-.057	-.076	-.099	-.060	-.083	-.164	-.196	-.224	-.250	-.310	-.403	-.516	-.736	-.702
	.950	.009	-.026	-.064	-.029	-.059	-.141	-.171	-.195	-.217	-.248	-.278	-.305	-.378	-.485
	.0375	-1.079	-1.049	-.986	-.889	-.829	-.812	-.764	-.709	-.631	-.569	-.507	-.440	-.367	-.262
	.075	-1.020	-.969	-.909	-.817	-.758	-.747	-.699	-.643	-.568	-.513	-.450	-.380	-.306	-.189
	.150	-.875	-.829	-.773	-.679	-.622	-.622	-.575	-.518	-.430	-.365	-.291	-.213	-.133	-.074
	.250	-.792	-.743	-.690	-.597	-.538	-.528	-.473	-.390	-.303	-.236	-.161	-.127	-.127	.204
	.350	-.320	-.322	-.360	-.130	-.017	.017	.053	.089	.118	.118	.116	.112	.106	.182
	.450	-.108	-.028	.018	.146	.180	.126	.125	.125	.110	.109	.108	.107	.103	.179
	.550	.051	.100	.118	.192	.192	.121	.115	.113	.100	.100	.102	.102	.099	.173
	.650	.118	.112	.104	.153	.144	.069	.061	.057	.043	.044	.045	.044	.039	.108
	.750	.128	.112	.099	.150	.142	.069	.063	.062	.056	.056	.061	.063	.058	.128
	.850	.134	.117	.102	.155	.149	.079	.072	.076	.075	.080	.088	.095	.095	.170
	.925	.149	.131	.115	.168	.161	.093	.088	.093	.099	.106	.120	.119	.132	.212
	.975	.154	.148	.120	.178	.182	.102	.100	.119	.118	.120	.142	.128	.168	.250
	1.000	.160	.158	.129	.182	.199	.110	.110	.128	.129	.130	.158	.130	.182	.270

^aNo orifice.

^bReaired value.

NACA

TABLE 8.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.80 PROPELLER BLADE SECTION ($x = 0.90$; $\beta_x = 39.50^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

J	2.110	2.142	2.161	2.194	2.213	2.255	2.284	2.312	2.336	2.371	2.405	2.439	2.471	2.501
M_x	1.095	1.088	1.074	1.064	1.055	1.047	1.039	1.031	1.022	1.013	1.005	.997	.985	.978
$C_{x'}$	2.77	2.35	2.11	1.69	1.45	.93	.57	.23	-.06	-.48	-.88	-1.28	-1.65	-1.99
$\Delta\beta$	-.79	-.89	-.94	-1.03	-1.08	-1.20	-1.26	-1.33	-1.38	-1.45	-1.50	-1.55	-1.59	-1.62
C_{Li}	1.54	1.38	1.29	1.09	.96	.80	.68	.54	.38	.14	-.08	-.29	-.50	-.73
c_m	.3413	.3071	.2871	.2429	.2132	.1761	.1516	.1213	.0852	.0316	-.0181	-.0639	-.1123	-.1639
c_m	-.1803	-.1858	-.1847	-.1857	-.1817	-.1820	-.1821	-.1819	-.1799	-.1735	-.1580	-.1480	-.1368	-.1206
c_o	.0432	.0458	.0467	.0478	.0478	.0485	.0503	.0514	.0522	.0533	.0515	.0505	.0476	.0456
a/b	Pressure coefficient, P													
Upper surface	$a_{0.000}$	1.336	1.331	1.322	1.315	1.310	1.304	1.300	1.294	1.288	1.283	1.276	1.273	1.266
	.025	.606	.626	.629	.631	.644	.654	.669	.684	.712	.720	.737	.749	.764
	.050	.348	.367	.369	.373	.383	.394	.407	.424	.451	.458	.473	.486	.501
	.100	.144	.161	.161	.164	.172	.181	.192	.206	.230	.234	.248	.258	.272
	.200	-.045	-.037	-.041	-.039	-.030	-.005	.031	.050	.067	.067	.076	.082	.092
	.300	-.113	-.104	-.107	-.103	-.100	-.095	-.089	-.078	-.065	-.066	-.059	-.056	-.052
	.400	-.202	-.196	-.202	-.204	-.203	-.199	-.195	-.186	-.172	-.174	-.168	-.164	-.155
	.500	-.297	-.294	-.301	-.305	-.308	-.306	-.302	-.295	-.286	-.291	-.287	-.284	-.274
	.600	-.377	-.379	-.389	-.395	-.398	-.396	-.393	-.387	-.379	-.382	-.379	-.378	-.373
	.700	-.449	-.460	-.473	-.479	-.484	-.480	-.478	-.470	-.463	-.468	-.467	-.467	-.463
	.800	-.543	-.549	-.562	-.568	-.575	-.575	-.575	-.571	-.567	-.576	-.576	-.580	-.582
Lower surface	.900	-.631	-.643	-.659	-.669	-.679	-.683	-.687	-.686	-.687	-.701	-.706	-.698	-.511
	.950	-.654	-.672	-.690	-.704	-.715	-.722	-.730	-.732	-.737	-.742	-.743	-.739	-.731
	.0375	-.179	-.217	-.264	-.326	-.371	-.419	-.471	-.534	-.577	-.630	-.670	-.711	-.768
	.075	-.130	-.190	-.237	-.298	-.341	-.387	-.440	-.497	-.537	-.589	-.628	-.668	-.721
	.150	-.007	-.068	-.120	-.178	-.223	-.266	-.315	-.368	-.407	-.461	-.511	-.558	-.606
	.250	.124	.008	-.070	-.141	-.188	-.231	-.279	-.329	-.365	-.416	-.456	-.494	-.544
	.350	.153	.102	.004	-.101	-.170	-.221	-.271	-.319	-.354	-.408	-.446	-.484	-.532
	.450	.160	.148	.120	.064	-.018	-.112	-.205	-.266	-.313	-.374	-.415	-.454	-.501
	.550	.168	.136	.139	.122	.112	.092	.047	-.022	-.024	-.180	-.250	-.304	-.359
	.650	.078	.067	.054	.046	.049	.064	.080	.117	.105	.053	.034	.014	-.005
	.750	.093	.081	.070	.064	.069	.083	.098	.113	.121	.105	.109	.107	.100
	.850	.128	.115	.113	.112	.117	.122	.126	.129	.131	.116	.119	.117	.112
	.925	.224	.210	.199	.181	.176	.169	.163	.155	.153	.132	.127	.118	.109
	b .975	.297	.308	.278	.250	.224	.203	.193	.177	.170	.149	.138	.129	.123
	a 1.000	.330	.370	.322	.290	.248	.222	.212	.189	.180	.157	.140	.142	.133

^aNo orifices.^bPaired values.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504 HO PROPELLER INLINE SECTION ($x = 0.95$;

$$\beta_x = 38.35^\circ; \beta_{0.75R} = 45^\circ$$

(a) $N = 1140$ rpm; $B = 2$.

	2.793	2.616	2.419	2.224	2.039	1.875	1.682	1.598	1.777	1.939	2.135	2.311	2.523	2.704
$\frac{J}{M_\infty}$.707	.683	.662	.639	.619	.603	.589	.585	.598	.611	.632	.650	.675	.697
$\frac{c_d}{c_l}$	-4.75	-2.89	-.68	1.66	4.01	6.21	8.95	10.18	7.58	5.34	2.77	.60	-1.86	-3.83
$\Delta \delta$	-.92	-.66	-.25	.06	.49	.78	1.14	1.29	.96	.66	.33	-.02	-.46	-.84
$\frac{c_l}{c_d}$	-.53	.33	1.26	2.05	2.86	3.65	4.64	4.83	4.19	3.30	2.41	1.72	.02	-.04
c_n	-.0852	.0542	.2039	.3316	.4597	.5658	.7445	.7755	.6697	.5323	.3890	.2787	.1329	-.0071
c_m	-.1121	-.0983	-.0885	-.0885	-.0821	-.0800	-.0675	-.0623	-.0749	-.0811	-.0864	-.0899	-.0928	-.1014
c_e														
c/b	Pressure coefficient, P													
Upper surface	b.000	1.132	1.123	1.115	1.106	1.099	1.094	1.089	1.088	1.092	1.096	1.104	1.110	1.119
	.025	b.680	.625	.428	.068	-.412	-.916	-1.823	-1.665	-1.717	-.684	-.153	.252	.541
	.050	.434	.322	.132	-.153	-.483	-.815	-1.600	-1.579	-1.087	-.675	-.308	-.015	.237
	.100	.178	.081	-.072	-.267	-.443	-.646	-1.118	-1.348	-.760	-.561	-.359	-.177	.011
	.200	-.020	-.088	-.187	-.299	-.406	-.513	-.604	-.755	-.559	-.458	-.352	-.249	-.134
	.300	-.106	-.173	-.223	-.299	-.364	-.438	-.505	-.532	-.487	-.406	-.333	-.268	-.187
	.400	-.193	-.226	-.274	-.324	-.391	-.442	-.471	-.478	-.418	-.354	-.301	-.246	-.210
	.500	-.191	-.215	-.232	-.292	-.343	-.389	-.425	-.419	-.416	-.368	-.318	-.277	-.230
	.600	-.228	-.273	-.300	-.327	-.362	-.394	-.421	-.405	-.416	-.379	-.345	-.319	-.282
	.700	-.263	-.273	-.290	-.314	-.341	-.367	-.381	-.363	-.381	-.354	-.328	-.308	-.275
	.800	-.265	-.264	-.269	-.285	-.299	-.314	-.318	-.298	-.325	-.306	-.294	-.281	-.264
	.900	-.248	-.230	-.225	-.232	-.214	-.210	-.216	-.205	-.217	-.213	-.229	-.234	-.221
	.950	-.087	-.069	-.064	-.065	-.058	-.065	-.086	-.094	-.076	-.079	-.062	-.065	-.060
Lower surface	.0375	-.763	-.889	-.305	.019	.261	.449	.584	.619	.530	.376	.135	-.105	-.745
	.075	-.714	-.673	-.125	.069	.215	.355	.462	.492	.416	.301	.128	-.013	-.316
	.150	-.646	-.337	-.048	.074	.168	.265	.344	.368	.310	.228	.113	.020	-.099
	.250	-.421	-.082	.006	.089	.140	.209	.261	.267	.229	.176	.103	.051	-.017
	.350	-.206	-.069	.009	.068	.119	.172	.219	.230	.197	.151	.091	.039	-.004
	.450	-.090	0	.027	.073	.107	.149	.182	.191	.167	.132	.088	.051	.017
	.550	-.033	.011	.027	.061	.088	.123	.150	.156	.138	.109	.072	.046	.022
	.650	.012	.037	.051	.081	.100	.129	.146	.139	.119	.089	.067	.048	.035
	.750	.029	.044	.051	.071	.079	.100	.112	.108	.094	.074	.062	.053	.044
	.850	.061	.075	.079	.093	.089	.100	.104	.102	.100	.089	.088	.082	.072
	.925	.099	.117	.127	.139	.126	.127	.123	.126	.130	.134	.136	.129	.113
	.975	.124	.147	.170	.177	.162	.150	.148	.132	.149	.159	.178	.182	.164
	b1.000	.140	.161	.195	.198	.182	.165	.160	.140	.160	.170	.205	.206	.182

^aNo orifice.
^bReaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(b) $N = 1350$ rpm; $B = 2$.

J	2.038	2.179	2.296	2.427	2.563	2.673	2.603	2.493	2.352	2.229	2.110
M_x	.738	.756	.771	.788	.810	.823	.814	.799	.776	.760	.746
α_x	4.02	2.22	.78	-.77	-2.30	-3.50	-2.74	-1.52	.11	1.58	3.07
$\Delta\delta$.67	.27	-.07	-.45	-.91	-1.29	-1.06	-.67	-.23	.12	.47
c_d	3.03	2.32	1.73	1.09	.36	-.19	.09	.78	1.44	2.02	2.64
c_n	.4887	.3732	.2781	.1768	.0581	-.0316	.0142	.1298	.2335	.3258	.4245
c_m	-.0870	-.0872	-.0880	-.0930	-.1073	-.1149	-.1121	-.1016	-.0891	-.0874	-.0866
c_c											
c/b	Pressure coefficient, P										
Upper surface	0.000	1.144	1.151	1.158	1.165	1.175	1.181	1.176	1.170	1.160	1.153
	.025	-.377	.031	.312	.515	.650	.732	.690	.584	.412	.174
	.050	-.526	-.226	.009	.196	.334	.423	.376	.263	.098	-.112
	.100	-.510	-.311	-.153	-.010	.104	.178	.141	.045	-.087	-.235
	.200	-.453	-.355	-.268	-.181	-.105	-.051	-.082	-.145	-.229	-.313
	.300	-.401	-.336	-.278	-.219	-.166	-.133	-.150	-.193	-.250	-.308
	.400	-.421	-.369	-.327	-.284	-.245	-.219	-.232	-.265	-.305	-.346
	.500	-.378	-.340	-.307	-.278	-.257	-.244	-.250	-.266	-.293	-.325
	.600	-.399	-.367	-.343	-.322	-.311	-.307	-.307	-.315	-.331	-.357
	.700	-.383	-.356	-.336	-.322	-.320	-.322	-.321	-.319	-.330	-.349
	.800	-.334	-.313	-.300	-.292	-.295	-.307	-.298	-.291	-.295	-.308
	.900	-.217	-.205	-.198	-.197	-.207	-.223	-.212	-.200	-.197	-.202
	.950	-.051	-.036	-.028	-.022	-.025	-.032	-.028	-.021	-.024	-.032
Lower surface	.0375	.273	.071	-.120	-.565	-1.319	-1.335	-1.371	-1.241	-.187	-.016
	.075	.229	.105	-.019	-.107	-.816	-1.183	-1.126	-.276	-.074	.092
	.150	.181	.102	.019	-.046	-.099	-.513	-.309	-.050	-.016	.062
	.250	.149	.103	.049	.002	-.009	-.133	-.013	-.010	.026	.078
	.350	.126	.079	.041	.009	-.011	-.027	-.016	-.002	.026	.062
	.450	.113	.078	.048	.024	.003	-.011	-.003	.014	.036	.062
	.550	.087	.061	.036	.019	.005	-.006	-.001	.013	.029	.047
	.650	.101	.079	.061	.048	.035	.025	.030	.043	.053	.068
	.750	.057	.042	.032	.028	.021	.016	.019	.027	.029	.035
	.850	.093	.086	.079	.078	.073	.067	.070	.078	.078	.080
	.925	.122	.121	.119	.119	.114	.106	.111	.118	.117	.119
	.975	.138	.142	.145	.151	.140	.137	.150	.150	.150	.150
	1.000	.145	.156	.160	.171	.161	.159	.170	.170	.175	.171

^aNo orifice.
^bPaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-904.40 PROPELLER BLADE SECTION ($\alpha = 0.95^\circ$) $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$ - Continued(a) $M = 1500$ rpm; $B = 2$.

	2.028	2.188	2.198	2.294	2.389	2.474	2.564	2.614	2.520	2.434	2.343	2.247	2.168	2.093
J	.822	.833	.845	.858	.875	.885	.904	.912	.894	.880	.863	.851	.837	.826
M_x	4.15	2.86	1.98	.80	-.33	-1.31	-2.32	-2.86	-1.83	-.85	.22	1.37	2.36	3.31
$\Delta\theta$.93	.53	.26	-.10	-.48	-.87	-1.34	-1.61	-1.11	-.68	-.29	.07	.38	.68
α_1	3.31	2.84	2.35	1.91	1.38	.86	.18	-.36	.43	1.10	1.60	2.10	2.58	3.05
α_2	.5332	.4561	.3794	.3087	.2239	.1394	.0897	-.0574	.0703	.1794	.2581	.3387	.4145	.4906
α_m	-.0914	-.0969	-.0977	-.0984	-.1101	-.1240	-.1288	-.1367	-.1296	-.1159	-.1041	-.0973	-.0950	-.0952
c_c							.0336	.0374						
c/b	Pressure coefficient, P													
Upper surface	0.000	1.180	1.185	1.191	1.197	1.206	1.211	1.221	1.225	1.216	1.208	1.200	1.194	1.187
	.025	-.280	.038	.221	.399	.589	.689	.721	.769	.680	.586	.482	.324	.131
	.050	-.433	-.243	-.085	.082	.210	.313	.412	.465	.366	.267	.162	.009	-.065
	.100	-.691	-.426	-.258	-.122	-.012	.081	.170	.220	.129	.040	-.053	-.182	-.320
	.200	-.775	-.490	-.305	-.283	-.211	-.146	-.081	-.037	-.109	-.172	-.237	-.317	-.400
	.300	-.807	-.475	-.347	-.297	-.254	-.209	-.182	-.149	-.189	-.227	-.269	-.318	-.361
	.400	-.848	-.488	-.405	-.368	-.336	-.299	-.274	-.260	-.280	-.317	-.349	-.383	-.413
	.500	-.813	-.490	-.378	-.352	-.331	-.305	-.285	-.332	-.288	-.314	-.335	-.359	-.380
	.600	-.845	-.488	-.422	-.415	-.410	-.387	-.362	-.375	-.377	-.398	-.408	-.411	-.418
	.700	-.841	-.486	-.428	-.417	-.417	-.408	-.396	-.386	-.399	-.413	-.420	-.424	-.423
	.800	-.870	-.452	-.445	-.438	-.438	-.442	-.447	-.440	-.443	-.441	-.444	-.440	-.436
Lower surface	.900	-.804	-.352	-.345	-.338	-.378	-.442	-.447	-.440	-.443	-.441	-.444	-.440	-.436
	.950	-.804	-.352	-.345	-.338	-.378	-.442	-.447	-.440	-.443	-.441	-.444	-.440	-.436
	.975	-.804	-.352	-.345	-.338	-.378	-.442	-.447	-.440	-.443	-.441	-.444	-.440	-.436
	1.000	-.804	-.352	-.345	-.338	-.378	-.442	-.447	-.440	-.443	-.441	-.444	-.440	-.436
	.0375	.279	.138	.011	-.108	-.251	-.398	-.501	-.564	-.600	-.622	-.647	-.668	-.677
	.075	.242	.155	.080	-.006	-.128	-.258	-.388	-.491	-.553	-.591	-.613	-.623	-.619
	.150	.193	.141	.086	.028	.045	-.335	-.485	-.583	-.643	-.680	-.703	-.715	-.713
	.250	.153	.136	.094	.055	.040	-.086	-.268	-.412	-.509	-.561	-.600	-.623	-.619
	.350	.137	.105	.076	.050	.030	-.058	-.230	-.363	-.459	-.511	-.549	-.572	-.587
	.450	.123	.098	.076	.055	.038	-.046	-.201	-.328	-.425	-.477	-.515	-.538	-.553
	.550	.096	.076	.059	.042	.026	-.030	-.168	-.286	-.383	-.435	-.473	-.496	-.511
	.650	.110	.095	.079	.067	.055	.032	-.074	-.194	-.291	-.343	-.381	-.404	-.419

^aNo orifice.
^bRevised value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(d) $N = 1600$ rpm; $B = 2$.

	J	2.097	2.185	2.269	2.343	2.435	2.521	2.549	2.479	2.392	2.322	2.240	2.151
M_x		.891	.904	.919	.928	.946	.961	.965	.951	.934	.920	.906	.893
α_x'		3.26	2.14	1.10	.22	-.86	-1.84	-2.15	-1.36	-.36	.47	1.46	2.57
$\Delta\delta$.90	.43	-.03	-.44	-.91	-1.32	-1.40	-1.14	-.69	-.32	.12	.61
α_1		3.04	2.45	1.84	1.32	.53	-.19	-.53	.19	.93	1.46	2.02	2.76
c_n		.4903	.3939	.2977	.2142	.0852	-.0303	-.0852	.0316	.1497	.2361	.3261	.4429
c_m		-.1163	-.1110	-.1113	-.1173	-.1327	-.1290	-.1196	-.1334	-.1239	-.1145	-.1103	-.1129
c_c			.0154	.0219	.0275	.0338	.0391	.0408	.0369	.0306	.0252	.0190	
c/b	Pressure coefficient, P												
Upper surface	θ , 0.000	1.214	1.222	1.229	1.234	1.244	1.219	1.254	1.247	1.237	1.230	1.222	1.215
	.025	.139	.329	.465	.570	.670	.749	.773	.714	.620	.530	.418	.226
	.050	-.136	.020	.151	.253	.363	.451	.478	.409	.309	.214	.103	-.069
	.100	-.413	-.189	-.067	.025	.130	.215	.241	.175	.078	-.007	-.109	-.325
	.200	-.472	-.389	-.303	-.213	-.114	-.036	-.010	-.071	-.159	-.255	-.338	-.432
	.300	-.504	-.422	-.320	-.205	-.146	-.121	-.176	-.275	-.295	-.282	-.331	-.453
	.400	-.477	-.390	-.298	-.222	-.312	-.255	-.236	-.280	-.337	-.333	-.366	-.450
	.500	-.446	-.390	-.364	-.338	-.355	-.312	-.294	-.332	-.338	-.348	-.376	-.409
	.600	-.495	-.463	-.438	-.408	-.402	-.394	-.380	-.409	-.381	-.414	-.450	-.487
	.700	-.535	-.508	-.479	-.455	-.425	-.442	-.432	-.451	-.427	-.457	-.488	-.525
	.800	-.582	-.569	-.537	-.515	-.484	-.513	-.508	-.494	-.493	-.517	-.545	-.576
Lower surface	.900	-.107	-.111	-.126	-.163	-.194	-.196	-.213	-.192	-.168	-.133	-.110	-.105
	.950	-.028	-.035	-.043	-.050	-.051	-.084	-.092	-.056	-.040	-.037	-.026	-.019
	.0375	.144	-.010	-.541	-.727	-.799	-.853	-.868	-.853	-.791	-.704	-.237	.073
	.075	.168	.071	-.041	-.606	-.709	-.764	-.782	-.761	-.690	-.562	.035	.123
	.150	.151	.082	.052	-.163	-.597	-.668	-.685	-.664	-.575	.064	.046	.118
	.250	.140	.091	.058	.101	-.375	-.553	-.576	-.524	.055	.073	.065	.118
	.350	.108	.074	.046	.061	.072	-.419	-.460	-.193	.095	.047	.055	.091
	.450	.099	.072	.048	.049	.103	-.146	-.316	.071	.074	.044	.056	.087
	.550	.074	.050	.026	.020	.064	.049	-.070	.079	.036	.021	.037	.064
	.650	.090	.069	.047	.040	.064	.086	.069	.082	.049	.044	.058	.082
	.750	.042	.025	.006	-.006	.010	.049	.056	.029	.004	.002	.016	.035
	.850	.088	.073	.055	.047	.054	.072	.077	.062	.053	.053	.067	.084
	.925	.119	.108	.093	.087	.088	.088	.087	.090	.091	.092	.105	.121
	.975	.142	.135	.119	.115	.100	.100	.095	.112	.125	.122	.130	.144
	a1.000	.156	.151	.135	.130	.110	.111	.102	.129	.148	.140	.145	.157

*No orifice.
 bPaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75x} = 45^\circ$) - Continued(e) $M = 0.56$; $\beta = 2$.

J	2.122	2.162	2.195	2.236	2.270	2.314	2.363	2.416	2.465	2.517	2.549	2.612	2.653
M_x	.982	.970	.960	.951	.938	.927	.918	.906	.895	.884	.875	.863	.850
α_x	2.94	2.43	2.02	1.51	1.09	.56	-.02	-.64	-1.20	-1.79	-2.15	-2.84	-3.28
$\Delta\delta$.12	-.04	-.15	-.22	-.28	-.35	-.46	-.65	-.85	-1.03	-1.13	-1.32	-1.44
α_1	2.46	2.32	2.10	1.91	1.69	1.42	1.29	.96	.68	.48	.28	.03	-.24
α_n	.3965	.3713	.3384	.3074	.2716	.2297	.2090	.1555	.1103	.0787	.0432	.0045	-.0387
c_m	-.1379	-.1363	-.1240	-.1216	-.1154	-.1154	-.1150	-.1221	-.1250	-.1270	-.1263	-.1229	-.1208
c_c	.0266	.0278	.0255	.0251	.0243	.0251	.0256	.0280	.0303	.0319	.0322	.0344	.0357
c/b	Pressure coefficient, P												
Upper surface	θ	0.000	1.254	1.257	1.251	1.246	1.239	1.233	1.228	1.221	1.217	1.210	1.206
		.025	.433	.451	.467	.484	.502	.514	.560	.609	.644	.672	.694
		.050	.143	.150	.161	.177	.193	.221	.244	.293	.330	.359	.381
		.100	-.125	-.080	-.056	-.042	-.027	-.001	.019	.064	.097	.124	.141
		.200	-.265	-.268	-.270	-.272	-.267	-.232	-.213	-.170	-.138	-.113	-.095
		.300	-.352	-.357	-.358	-.355	-.333	-.298	-.267	-.231	-.206	-.187	-.174
		.400	-.391	-.384	-.368	-.348	-.336	-.327	-.317	-.300	-.288	-.275	-.264
		.500	-.363	-.362	-.353	-.352	-.348	-.344	-.345	-.327	-.305	-.291	-.284
		.600	-.412	-.420	-.421	-.419	-.420	-.415	-.405	-.397	-.384	-.377	-.360
		.700	-.448	-.462	-.463	-.463	-.464	-.461	-.454	-.439	-.416	-.400	-.396
Lower surface	θ	.800	-.512	-.519	-.484	-.521	-.523	-.515	-.510	-.492	-.475	-.449	-.437
		.900	-.616	-.562	-.404	-.290	-.188	-.139	-.110	-.101	-.124	-.151	-.189
		.950	-.254	-.212	-.167	-.130	-.082	-.040	-.004	.026	.030	.010	.003
		.0375	-.025	-.155	-.335	-.464	-.571	-.675	-.749	-.858	-.948	-1.015	-1.095
		.075	.113	.104	.066	-.101	-.310	-.534	-.631	-.753	-.842	-.909	-.990
		.150	.115	.099	.084	.085	.090	.082	.023	-.332	-.554	-.647	-.732
		.250	.112	.098	.083	.074	.071	.078	.087	.101	.077	.030	-.045
		.350	.096	.085	.070	.061	.053	.051	.054	.068	.075	.080	.074
		.450	.092	.081	.069	.062	.053	.047	.047	.053	.058	.058	.052
		.550	.056	.049	.039	.032	.028	.023	.025	.031	.033	.037	.029
		.650	.071	.064	.055	.050	.047	.044	.049	.053	.059	.059	.055
		.750	.016	.011	.004	.001	.002	.005	.013	.025	.033	.037	.033
		.850	.066	.057	.049	.046	.047	.053	.067	.081	.090	.093	.088
		.925	.108	.097	.085	.079	.082	.093	.111	.128	.136	.140	.133
		.975	.138	.125	.115	.110	.108	.122	.138	.156	.170	.171	.172
		1.000	.153	.141	.130	.127	.121	.137	.151	.170	.185	.188	.192

No orifice.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued $(r) M = 0.98$; $B = 2$.

	2.129	2.161	2.197	2.229	2.264	2.296	2.337	2.388	2.426	2.471	2.520	2.573	2.637
J	2.129	2.161	2.197	2.229	2.264	2.296	2.337	2.388	2.426	2.471	2.520	2.573	2.637
M_x	1.019	1.009	.999	.988	.975	.963	.952	.943	.931	.920	.910	.899	.882
α_x	2.85	2.44	1.99	1.60	1.17	.78	.29	-.31	-.76	-1.27	-1.83	-2.41	-3.11
$\Delta\theta$.18	-.04	-.26	-.42	-.56	-.65	-.71	-.76	-.82	-.85	-1.12	-1.32	-1.55
α_1	2.41	2.19	1.95	1.65	1.62	1.47	1.25	.97	.84	.60	.46	.22	-.20
c_n	.3884	.3532	.3142	.2681	.2610	.2374	.2019	.1555	.1368	.0981	.0748	.0348	-.0329
c_m	-.1610	-.1326	-.1439	-.1392	-.1386	-.1322	-.1281	-.1259	-.1272	-.1281	-.1322	-.1288	-.1281
c_c	.0341	.0332	.0325	.0328	.0340	.0310	.0306	.0304	.0308	.0310	.0317		
c/b	Pressure coefficient, P												
Upper surface	∞	1.286	1.280	1.274	1.268	1.260	1.253	1.248	1.242	1.236	1.230	1.224	1.219
	.025	.502	.522	.538	.552	.563	.577	.584	.596	.604	.612	.620	.628
	.050	.207	.225	.238	.250	.268	.281	.296	.328	.346	.364	.393	.423
	.100	-.040	.009	.025	.036	.051	.061	.073	.100	.115	.149	.155	.178
	.200	-.211	-.205	-.201	-.203	-.195	-.179	-.166	-.144	-.132	-.099	-.095	-.073
	.300	-.299	-.293	-.277	-.292	-.274	-.272	-.269	-.249	-.232	-.199	-.196	-.175
	.400	-.368	-.358	-.347	-.348	-.348	-.346	-.343	-.331	-.329	-.294	-.280	-.271
	.500	-.338	-.324	-.318	-.329	-.330	-.330	-.346	-.351	-.345	-.306	-.299	-.272
	.600	-.389	-.381	-.378	-.384	-.383	-.381	-.386	-.377	-.369	-.360	-.358	-.364
	.700	-.422	-.417	-.414	-.420	-.420	-.420	-.425	-.419	-.424	-.405	-.403	-.395
	.800	-.478	-.470	-.470	-.478	-.480	-.482	-.485	-.480	-.484	-.459	-.456	-.430
Lower surface	.900	-.588	-.585	-.589	-.595	-.577	-.401	-.381	-.188	-.145	-.101	-.110	-.139
	.950	-.645	-.691	-.621	-.643	-.184	-.125	-.091	-.047	-.019	.036	.035	.088
	.0375	-.209	-.308	-.383	-.457	-.540	-.607	-.679	-.758	-.833	-.911	-1.060	-1.162
	.075	.009	-.165	-.269	-.353	-.438	-.507	-.584	-.668	-.744	-.816	-.968	-1.073
	.150	.135	.137	.121	-.002	-.178	-.318	-.459	-.594	-.632	-.707	-.761	-.845
	.250	.124	.124	.125	.127	.131	.129	.096	-.005	-.083	-.142	-.175	-.250
	.350	.098	.096	.093	.089	.094	.099	.123	.112	.106	.102	.079	.002
	.450	.098	.093	.087	.078	.077	.077	.077	.089	.092	.108	.102	.099
	.550	.060	.057	.052	.043	.041	.041	.038	.049	.052	.071	.067	.068
	.650	.071	.069	.065	.055	.051	.052	.047	.054	.057	.077	.074	.073
	.750	.037	.036	.033	.026	.029	.022	.019	.029	.035	.061	.061	.062
	.850	.079	.074	.067	.056	.049	.046	.043	.054	.063	.093	.094	.095
	.925	.150	.141	.127	.115	.102	.096	.092	.104	.114	.146	.148	.144
	.975	.227	.216	.186	.171	.166	.140	.130	.150	.156	.186	.200	.189
	1.000	.280	.265	.225	.205	.205	.166	.150	.170	.177	.210	.225	.210

^aNo orifice.
^bPaired value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.72R} = 45^\circ$) - Continued(a) $M = 0.60$; $B = 2$.

	J	2.132	2.161	2.189	2.222	2.253	2.287	2.312	2.333	2.381	2.412	2.451	2.490	2.527	2.568	2.599
M_x		1.050	1.040	1.031	1.023	1.014	1.005	.993	.987	.975	.967	.958	.949	.941	.932	.921
α_x		2.81	2.44	2.09	1.68	1.30	.89	.59	.10	-.23	-.79	-1.04	-1.49	-1.91	-2.36	-2.70
$\Delta\theta$		-.45	-.46	-.48	-.53	-.61	-.72	-.81	-.99	-1.10	-1.20	-1.30	-1.37	-1.42	-1.47	-1.51
α_1		2.09	1.97	1.85	1.70	1.55	1.25	1.11	.85	.73	.53	.25	.13	-.09	-.22	-.40
c_n		.3371	.3181	.2971	.2745	.2481	.2003	.1790	.1381	.1177	.0868	.0406	.0206	-.0155	-.0348	-.0658
c_m		-.1565	-.1604	-.1615	-.1631	-.1592	-.1540	-.1525	-.1531	-.1490	-.1460	-.1399	-.1388	-.1355	-.1360	-.1368
c_o		.0355	.0371	.0377	.0391	.0386	.0384	.0389	.0397	.0392	.0378	.0365	.0368	.0365	.0367	.0376
c/b		Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.306	1.300	1.294	1.289	1.283	1.277	1.271	1.267	1.260	1.256	1.251	1.246	1.241	1.236	1.230
	$a_{0.025}$.564	.576	.581	.583	.586	.590	.592	.595	.597	.598	.599	.600	.601	.602	.603
	$a_{0.050}$.872	.880	.884	.886	.888	.890	.891	.892	.893	.894	.895	.896	.897	.898	.899
	$a_{0.100}$.041	.061	.070	.081	.096	.120	.122	.142	.151	.159	.172	.186	.201	.217	.233
	$a_{0.200}$	-.154	-.154	-.156	-.153	-.147	-.125	-.117	-.099	-.094	-.088	-.077	-.064	-.051	-.038	-.023
	$a_{0.300}$	-.241	-.245	-.248	-.244	-.229	-.213	-.217	-.204	-.203	-.198	-.185	-.174	-.164	-.153	-.142
	$a_{0.400}$	-.331	-.334	-.328	-.315	-.311	-.299	-.302	-.289	-.290	-.290	-.285	-.279	-.272	-.261	-.250
	$a_{0.500}$	-.315	-.331	-.331	-.335	-.335	-.327	-.336	-.332	-.337	-.338	-.334	-.333	-.331	-.329	-.324
	$a_{0.600}$	-.359	-.371	-.374	-.378	-.382	-.389	-.402	-.402	-.406	-.409	-.408	-.411	-.413	-.412	-.404
	$a_{0.700}$	-.385	-.395	-.398	-.400	-.401	-.402	-.414	-.417	-.428	-.432	-.438	-.449	-.449	-.444	-.423
	$a_{0.800}$	-.444	-.449	-.451	-.453	-.454	-.455	-.465	-.467	-.474	-.477	-.481	-.491	-.484	-.471	-.453
	$a_{0.900}$	-.550	-.559	-.563	-.564	-.566	-.567	-.577	-.571	-.511	-.375	-.231	-.172	-.120	-.099	-.096
	$a_{0.950}$	-.648	-.661	-.665	-.637	-.501	-.370	-.265	-.188	-.141	-.107	-.068	-.048	-.008	.023	.042
Lower surface	$b_{0.0375}$	-.245	-.309	-.363	-.418	-.474	-.539	-.587	-.644	-.696	-.745	-.798	-.859	-.920	-.970	-1.030
	$b_{0.075}$	-.164	-.221	-.270	-.324	-.383	-.453	-.503	-.565	-.617	-.663	-.715	-.773	-.831	-.881	-.946
	$b_{0.150}$.085	-.072	-.139	-.218	-.279	-.351	-.402	-.463	-.517	-.563	-.616	-.675	-.729	-.774	-.830
	$b_{0.250}$.153	.143	.134	.095	.028	-.140	-.223	-.320	-.376	-.425	-.483	-.549	-.608	-.657	-.714
	$b_{0.350}$.116	.116	.116	.122	.128	.121	.108	.055	.016	-.016	-.094	-.199	-.293	-.353	-.423
	$b_{0.450}$.112	.106	.103	.105	.110	.120	.117	.122	.115	.110	.100	.071	.050	.035	.033
	$b_{0.550}$.064	.096	.054	.058	.064	.074	.072	.084	.085	.086	.090	.086	.087	.087	.085
	$b_{0.650}$.070	.063	.061	.062	.067	.072	.068	.078	.079	.080	.085	.086	.092	.097	.100
	$b_{0.750}$.030	.022	.020	.018	.027	.031	.029	.039	.039	.042	.050	.053	.066	.076	.084
	$b_{0.850}$.078	.073	.069	.068	.065	.061	.054	.057	.054	.054	.063	.066	.083	.096	.106
	$b_{0.925}$.172	.161	.150	.141	.132	.123	.111	.107	.100	.096	.103	.106	.124	.140	.153
	$b_{0.975}$.259	.248	.218	.195	.188	.172	.162	.147	.153	.133	.137	.140	.161	.180	.188
	$b_{1.000}$.305	.298	.255	.222	.218	.195	.188	.168	.183	.151	.154	.160	.180	.200	.202

^aNo orifice.
^bPaired value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(h) $M = 0.65$; $B = 2$.

	γ	M_{∞}	α_x	$\Delta\theta$	α_1	c_n	c_m	c_c									
	2.104	2.132	2.157	2.189	2.212	2.243	2.266	2.304	2.326	2.356	2.390	2.413	2.455	2.483			
	1.136	1.127	1.117	1.108	1.095	1.087	1.076	1.069	1.060	1.045	1.037	1.028	1.020	1.009			
	3.17	2.81	2.49	2.09	1.81	1.42	1.14	.68	.42	.06	-.34	-.61	-1.09	-1.41			
	-.90	-.98	-1.06	-1.16	-1.23	-1.31	-1.37	-1.46	-1.51	-1.57	-1.63	-1.67	-1.73	-1.76			
	1.77	1.55	1.39	1.29	1.08	.89	.80	.63	.47	.27	.12	-.09	-.34	-.64			
	.2839	.2481	.2235	.2077	.1748	.1432	.1297	.1019	.0768	.0432	.0187	-.0155	-.0552	-.1032			
	-.1467	-.1483	-.1482	-.1526	-.1515	-.1511	-.1513	-.1480	-.1501	-.1462	-.1420	-.1406	-.1268	-.1163			
	.0342	.0376	.0390	.0412	.0418	.0429	.0442	.0445	.0460	.0471	.0493	.0482	.0469	.0391			
c/b	Pressure coefficient, P																
Upper surface	$a_{0.000}$	1.364	1.358	1.351	1.344	1.336	1.331	1.323	1.319	1.312	1.303	1.298	1.292	1.287	1.280		
	.025	.659	.671	.674	.687	.698	.710	.717	.729	.738	.746	.757	.763	.780	.795		
	.050	.378	.390	.389	.400	.409	.421	.428	.440	.450	.455	.466	.473	.489	.504		
	.100	.121	.161	.167	.184	.193	.204	.212	.223	.232	.234	.243	.247	.262	.273		
	.200	-.038	-.036	-.043	-.038	-.038	-.035	-.032	-.017	-.004	-.003	.003	.004	.016	.025		
	.300	-.124	-.124	-.134	-.129	-.130	-.125	-.115	-.111	-.109	-.113	-.110	-.112	-.100	-.090		
	.400	-.227	-.223	-.234	-.222	-.217	-.213	-.214	-.207	-.203	-.208	-.208	-.211	-.205	-.202		
	.500	-.241	-.240	-.255	-.251	-.256	-.259	-.258	-.252	-.252	-.259	-.262	-.267	-.260	-.256		
	.600	-.291	-.297	-.316	-.316	-.325	-.329	-.331	-.327	-.329	-.340	-.342	-.347	-.341	-.340		
	.700	-.310	-.320	-.339	-.341	-.350	-.356	-.358	-.356	-.360	-.372	-.376	-.383	-.381	-.384		
	.800	-.358	-.370	-.392	-.395	-.407	-.414	-.420	-.418	-.427	-.442	-.447	-.455	-.454	-.460		
Lower surface	.900	-.453	-.465	-.487	-.494	-.509	-.517	-.525	-.524	-.535	-.559	-.570	-.570	-.570	-.579		
	.950	-.540	-.552	-.575	-.583	-.599	-.610	-.618	-.620	-.634	-.651	-.658	-.640	-.609	-.588		
	.0375	-.124	-.186	-.234	-.280	-.330	-.376	-.424	-.466	-.512	-.554	-.600	-.644	-.686	-.741		
	.075	-.058	-.112	-.177	-.203	-.256	-.305	-.356	-.398	-.443	-.487	-.532	-.574	-.615	-.666		
	.150	.023	-.035	-.086	-.129	-.181	-.228	-.276	-.318	-.362	-.405	-.450	-.491	-.533	-.583		
	.250	.091	.028	-.020	-.059	-.107	-.150	-.192	-.228	-.265	-.307	-.354	-.393	-.436	-.488		
	.350	.146	.067	-.001	-.036	-.077	-.113	-.147	-.175	-.203	-.240	-.282	-.313	-.344	-.387		
	.450	.169	.155	.088	.031	-.033	-.067	-.096	-.116	-.139	-.171	-.205	-.230	-.254	-.288		
	.550	.131	.125	.104	.087	.025	-.035	-.078	-.102	-.123	-.167	-.200	-.221	-.242	-.269		
	.650	.131	.125	.109	.107	.096	.074	.049	.040	.029	-.045	-.113	-.131	-.146	-.194		
	.750	.076	.068	.055	.058	.056	.061	.067	.078	.072	.044	.010	.008	.002	-.026		
	.850	.063	.055	.043	.059	.076	.098	.113	.122	.113	.098	.091	.085	.084	.074		
	.925	.220	.207	.194	.199	.195	.193	.187	.181	.168	.149	.138	.126	.120	.106		
	.975	.392	.370	.304	.352	.301	.284	.252	.230	.210	.175	.149	.148	.138	.117		
	1.000	.485	.450	.446	.440	.356	.335	.288	.255	.232	.187	.157	.156	.146	.123		

*No orifice.

bPaired value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(1) $N = 1500$ rpm; $B = 1$.

r M_x α_1 α_2 α_3 c_m c_n c_o	2.592 .883 -2.62 -1.48 .25 .0477 -1.504	2.512 .871 -1.74 -1.06 .75 .1439 -1.386	2.399 .851 -1.44 -.52 1.24 .2368 -1.227	2.288 .833 -.88 -.08 1.70 .3268 -1.133	2.185 .821 2.14 .30 2.23 .4313 -1.050	2.092 .805 3.32 .68 2.72 .5835 -1.045	2.009 .799 3.75 .82 2.90 .5945 -1.031	2.033 .798 4.09 .92 3.06 .6026 -1.019	1.990 .791 4.66 1.08 3.35 .6323 -1.073	1.965 .789 4.99 1.17 3.47 .6548 -1.021	1.930 .784 5.46 1.29 3.72 .6955 -0.995	1.897 .781 5.91 1.40 3.93 .7316 -1.014	1.849 .777 6.57 1.54 4.23 .7897 -0.968	1.812 .771 7.09 1.64 4.46 .8355 -0.968	1.785 .770 7.47 1.70 4.57 .8594 -0.950	1.751 .765 7.95 1.77 4.76 .9000 -0.944
c/b	Pressure coefficient, P															
Upper surface	$a_0.000$	1.210	1.204	1.194	1.185	1.180	1.173	1.169	1.166	1.166	1.163	1.162	1.160	1.158	1.158	1.155
	$a_0.025$.698	.671	.630	.628	-.060	-.354	-.408	-.628	-.747	-.829	-.860	-.963	-1.177	-1.282	-1.454
	$a_0.050$.423	.345	.225	.064	-.148	-.340	-.420	-.519	-.659	-.754	-.835	-.905	-1.059	-1.175	-1.326
	$a_0.100$.136	.062	-.044	-.176	-.352	-.603	-.699	-.774	-.829	-.883	-.983	-1.072	-1.178	-1.232	-1.362
	$b_0.200$	-.209	-.270	-.314	-.380	-.440	-.597	-.695	-.668	-.660	-.669	-.683	-.708	-.780	-.827	-.896
	$b_0.300$	-.305	-.332	-.371	-.416	-.467	-.496	-.496	-.501	-.505	-.500	-.495	-.496	-.533	-.568	-.640
	$b_0.400$	-.236	-.256	-.293	-.330	-.372	-.403	-.414	-.423	-.432	-.435	-.436	-.439	-.453	-.455	-.453
	$b_0.500$	-.290	-.305	-.330	-.356	-.388	-.413	-.424	-.434	-.445	-.449	-.452	-.455	-.469	-.472	-.473
	$b_0.600$	-.304	-.313	-.324	-.341	-.367	-.385	-.391	-.399	-.409	-.412	-.417	-.422	-.433	-.435	-.432
	$b_0.700$	-.373	-.378	-.367	-.373	-.393	-.404	-.408	-.415	-.425	-.430	-.435	-.440	-.453	-.455	-.459
	$b_0.800$	-.395	-.398	-.327	-.328	-.340	-.343	-.343	-.350	-.357	-.360	-.365	-.373	-.383	-.390	-.391
	$b_0.900$	-.146	-.151	-.154	-.156	-.165	-.169	-.171	-.174	-.180	-.183	-.188	-.193	-.202	-.203	-.213
	$b_0.950$.088	.021	.012	.004	-.006	-.015	-.019	-.022	-.028	-.031	-.034	-.039	-.046	-.050	-.058
Lower surface	$a_0.035$	-1.071	-1.022	-.895	-.074	.094	.224	.272	.318	.363	.397	.436	.474	.517	.548	.569
	$a_0.075$	-.967	-.916	-.101	-.020	.102	.198	.229	.262	.295	.321	.353	.380	.414	.438	.454
	$a_0.150$	-.881	-.188	-.020	0	.073	.149	.169	.190	.213	.232	.254	.276	.297	.317	.333
	$a_0.250$	-.205	.070	.022	.057	.107	.141	.156	.173	.189	.200	.218	.236	.254	.270	.280
	$b_0.350$.065	.021	.007	.041	.073	.114	.124	.135	.146	.157	.169	.183	.197	.209	.217
	$b_0.450$.084	.052	.049	.072	.100	.116	.123	.131	.141	.149	.162	.174	.184	.192	.199
	$b_0.550$.050	.034	.033	.051	.073	.091	.098	.104	.112	.119	.128	.139	.146	.155	.160
	$b_0.650$.055	.050	.050	.064	.080	.090	.094	.100	.106	.113	.120	.130	.134	.141	.145
	$b_0.750$.066	.052	.059	.065	.076	.079	.082	.087	.091	.095	.103	.109	.114	.119	.122
	$b_0.850$.098	.095	.090	.090	.091	.088	.088	.073	.092	.095	.101	.106	.108	.110	.111
	$b_0.925$.123	.114	.113	.120	.112	.107	.104	.062	.090	.094	.097	.092	.098	.095	.100
	$b_0.975$.144	.130	.132	.144	.129	.123	.114	.058	.090	.090	.094	.087	.094	.086	.090
	$a_1.000$.153	.140	.142	.157	.138	.131	.120	.055	.090	.090	.092	.084	.092	.082	.095

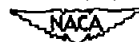
^aNo orifice.^bFaired value.^cExtrapolated value.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\tau = 0.95$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(j) $M = 0.56$; $B = 1$.

	J	2.336	2.301	2.267	2.252	2.222	2.194	2.172	2.145	2.128	2.106	2.079	2.049	2.030	2.006
M_x		.933	.938	.942	.951	.959	.966	.972	.980	.989	.996	1.003	1.009	1.015	1.024
$c_{d,i}$.30	.72	1.13	1.31	1.68	2.03	2.30	2.64	2.86	3.14	3.49	3.88	4.13	4.44
$c_{d,p}$		-.39	-.33	-.28	-.25	-.20	-.14	-.08	.02	.20	.40	.61	.83	.99	1.17
α_1		1.28	1.43	1.53	1.55	1.72	1.85	2.00	2.10	2.21	2.37	2.51	2.66	2.78	2.82
α_n		.2442	.2758	.2942	.2981	.3335	.3565	.3865	.4042	.4242	.4526	.4784	.5061	.5252	.5306
c_m		-.1209	-.1192	-.1195	-.1154	-.1179	-.1233	-.1230	-.1275	-.1343	-.1391	-.1528	-.1637	-.1682	-.1682
c_o		.0255	.0242	.0239	.0235	.0233	.0233	.0228	.0235	.0245	.0256	.0281	.0305	.0307	.0306
o/b		Pressure coefficient, P													
Upper surface	$a_{0.000}$	1.238	1.240	1.242	1.247	1.251	1.255	1.259	1.263	1.268	1.272	1.276	1.280	1.284	1.290
	$a_{.025}$.490	.501	.510	.520	.533	.543	.553	.560	.574	.587	.601	.610	.621	.632
	$a_{.050}$.256	.230	.213	.208	.196	.183	.173	.159	.150	.146	.149	.129	.119	.115
	$a_{.100}$	-.021	-.047	-.063	-.067	-.079	-.098	-.117	-.133	-.147	-.154	-.160	-.165	-.168	-.167
	$b_{.200}$	-.305	-.333	-.342	-.352	-.372	-.387	-.401	-.402	-.403	-.418	-.423	-.422	-.419	-.417
	$b_{.300}$	-.390	-.417	-.439	-.448	-.454	-.462	-.464	-.466	-.469	-.470	-.470	-.473	-.476	-.475
	$b_{.400}$	-.312	-.318	-.325	-.334	-.349	-.361	-.365	-.374	-.378	-.386	-.390	-.395	-.403	-.407
	$b_{.500}$	-.367	-.378	-.378	-.378	-.382	-.393	-.398	-.402	-.407	-.410	-.413	-.414	-.415	-.414
	$b_{.600}$	-.339	-.354	-.357	-.355	-.360	-.368	-.368	-.373	-.375	-.378	-.380	-.382	-.386	-.386
	$b_{.700}$	-.431	-.438	-.444	-.441	-.443	-.449	-.451	-.454	-.456	-.456	-.455	-.455	-.459	-.459
Lower surface	$b_{.800}$	-.488	-.496	-.500	-.499	-.493	-.503	-.504	-.507	-.508	-.507	-.507	-.507	-.508	-.507
	$b_{.900}$	-.268	-.282	-.282	-.291	-.328	-.368	-.387	-.419	-.448	-.507	-.535	-.603	-.607	-.613
	$b_{.950}$	-.027	-.050	-.076	-.096	-.130	-.162	-.199	-.249	-.310	-.406	-.524	-.684	-.714	-.723
	$a_{.0375}$	-.693	-.608	-.537	-.476	-.372	-.233	-.066	.011	.038	.089	.122	.149	.178	.201
	$a_{.075}$	-.568	-.405	-.225	-.107	.035	.073	.074	.083	.107	.130	.156	.185	.211	.231
	$a_{.150}$.048	.052	.035	.031	.028	.032	.045	.058	.079	.096	.114	.134	.150	.165
	$a_{.250}$.079	.069	.066	.068	.075	.083	.095	.105	.119	.132	.146	.161	.175	.185
	$a_{.350}$.045	.041	.041	.046	.052	.059	.069	.074	.087	.095	.105	.117	.127	.135
	$a_{.450}$.065	.066	.068	.071	.078	.083	.092	.096	.107	.116	.124	.136	.144	.152
	$a_{.550}$.036	.037	.037	.040	.044	.048	.055	.057	.067	.074	.081	.091	.099	.106
Lower surface	$a_{.650}$.053	.053	.052	.054	.058	.060	.067	.068	.076	.082	.090	.097	.106	.111
	$a_{.750}$.028	.024	.022	.022	.023	.022	.027	.027	.033	.038	.044	.051	.058	.061
	$a_{.850}$.053	.047	.043	.040	.041	.043	.047	.049	.055	.062	.069	.075	.084	.089
	$b_{.925}$.092	.092	.093	.077	.077	.086	.086	.089	.102	.107	.123	.130	.141	.145
	$b_{.975}$.120	.136	.142	.112	.112	.126	.123	.131	.150	.151	.178	.183	.204	.188
	$a_{1.000}$.134	.162	.173	.133	.133	.146	.146	.157	.182	.177	.214	.218	.248	.232

^aNo orifice.^bPaired values.^cExtrapolated value.

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.97^\circ$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(x) $M = 0.58$; $B = 1$.

J	2.454	2.379	2.311	2.279	2.245	2.225	2.198	2.172	2.154	2.129	2.103	2.084	2.063	2.043	2.022	2.003	1.986	1.976	1.951
M_x	.930	.949	.965	.974	.980	.985	.991	.999	1.008	1.016	1.021	1.029	1.036	1.043	1.050	1.057	1.065	1.069	1.079
a_{45}	-1.10	-.23	.58	.96	1.38	1.63	1.96	2.28	2.51	2.83	3.16	3.40	3.68	3.94	4.21	4.46	4.69	5.09	5.16
a_1	.67	.88	1.13	1.28	1.45	1.57	1.68	1.83	2.01	2.07	2.20	2.24	2.34	2.40	2.45	2.52	2.55	2.57	2.58
a_n	.1897	.1684	.2161	.2468	.2803	.3016	.3235	.3589	.3868	.3992	.4197	.4432	.4581	.4687	.4768	.4823	.4835	.4835	.4835
a_m	-.1273	-.1193	-.1213	-.1226	-.1230	-.1274	-.1330	-.1452	-.1540	-.1541	-.1595	-.1597	-.1626	-.1610	-.1635	-.1668	-.1664	-.1635	-.1649
a_c	.0297	.0282	.0278	.0281	.0272	.0278	.0289	.0301	.0334	.0325	.0326	.0334	.0333	.0325	.0332	.0331	.0329	.0335	.0328
a/b	Pressure coefficient, P																		
Upper surface	$a_{0.000}$	1.235	1.246	1.254	1.259	1.263	1.266	1.270	1.275	1.280	1.285	1.288	1.293	1.296	1.302	1.306	1.311	1.317	1.319
	.025	.547	.571	.598	.609	.617	.627	.639	.650	.664	.674	.683	.694	.707	.716	.723	.730	.741	.751
	.050	.364	.332	.302	.289	.263	.255	.246	.238	.234	.226	.216	.213	.204	.199	.195	.190	.183	.174
	.100	.076	.048	.022	.010	-.014	-.023	-.036	-.051	-.062	-.069	-.076	-.075	-.073	-.079	-.072	-.069	-.060	-.050
	.150	-.228	-.247	-.284	-.287	-.317	-.317	-.324	-.326	-.334	-.338	-.332	-.326	-.335	-.353	-.328	-.339	-.320	-.278
	.200	-.366	-.375	-.386	-.393	-.410	-.412	-.414	-.410	-.411	-.413	-.409	-.410	-.411	-.410	-.413	-.413	-.413	-.410
	.250	-.312	-.319	-.320	-.327	-.333	-.337	-.334	-.336	-.335	-.341	-.349	-.349	-.354	-.358	-.361	-.364	-.366	-.369
	.300	-.342	-.361	-.354	-.356	-.358	-.362	-.364	-.369	-.371	-.374	-.378	-.378	-.377	-.380	-.376	-.377	-.374	-.372
	.350	-.301	-.311	-.320	-.323	-.329	-.333	-.333	-.337	-.336	-.337	-.343	-.343	-.343	-.344	-.347	-.348	-.344	-.346
	.400	-.404	-.403	-.406	-.408	-.413	-.414	-.413	-.417	-.415	-.415	-.418	-.416	-.414	-.415	-.416	-.416	-.410	-.410
Lower surface	$a_{0.000}$	-.463	-.461	-.462	-.464	-.468	-.469	-.467	-.468	-.466	-.469	-.468	-.464	-.465	-.464	-.466	-.469	-.465	-.458
	.025	-.185	-.186	-.277	-.323	-.347	-.322	-.462	-.477	-.549	-.558	-.572	-.573	-.574	-.572	-.558	-.563	-.564	-.562
	.050	.010	-.040	-.104	-.153	-.189	-.250	-.309	-.469	-.621	-.671	-.688	-.689	-.683	-.683	-.677	-.666	-.667	-.658
	.075	-.811	-.717	-.593	-.534	-.475	-.420	-.364	-.302	-.225	-.150	-.092	-.063	-.039	-.022	-.009	0	.015	.028
	.100	-.730	-.638	-.508	-.451	-.373	-.289	-.169	-.033	.080	.111	.118	.135	.164	.184	.203	.220	.247	.262
	.150	-.685	-.584	-.353	-.197	.037	.082	.079	.073	.073	.079	.091	.106	.127	.141	.156	.167	.188	.199
	.200	-.620	-.403	.138	.131	.110	.105	.104	.107	.115	.125	.135	.146	.163	.172	.182	.192	.208	.216
	.250	-.413	.101	.081	.072	.060	.059	.064	.069	.080	.089	.096	.103	.117	.125	.130	.137	.152	.153
	.300	.101	.094	.088	.086	.083	.086	.093	.095	.109	.118	.123	.132	.144	.150	.157	.162	.176	.178
	.350	.056	.045	.039	.037	.038	.041	.047	.052	.061	.069	.076	.082	.089	.094	.099	.106	.109	.122
	.400	.060	.049	.048	.046	.049	.051	.058	.062	.071	.079	.082	.089	.090	.103	.108	.112	.130	.124
	.450	.043	.032	.026	.024	.026	.027	.033	.034	.041	.049	.050	.056	.066	.067	.071	.075	.090	.087
	.500	.066	.048	.041	.040	.043	.047	.054	.058	.066	.073	.076	.081	.091	.091	.095	.097	.112	.105
	$a_{0.925}$.092	.063	.066	.072	.077	.081	.097	.102	.116	.128	.136	.148	.168	.167	.174	.182	.145	.146
	$a_{0.975}$.118	.083	.090	.102	.110	.113	.138	.145	.162	.176	.190	.218	.268	.267	.242	.274	.255	.274
	$a_{1.000}$.131	.092	.104	.120	.130	.133	.163	.170	.188	.201	.212	.263	.290	.288	.265	.293	.268	.288

^a No orifice.^b Paired value.^c Extrapolated value.

NACA

TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($\alpha = 0.95^\circ$; $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$) - Continued(1) $M = 0.60$; $B = 1$.

β M_∞ α α_1 α_n α_m α_c	2.323	2.289	2.257	2.230	2.211	2.183	2.160	2.141	2.115	2.102	2.072	2.049	2.030	2.010	1.985	1.970
α_1	.995	1.004	1.008	1.016	1.025	1.028	1.036	1.042	1.050	1.060	1.063	1.071	1.077	1.085	1.093	1.104
α_2	.45	.86	1.25	1.58	1.82	2.17	2.46	2.70	3.03	3.19	3.58	3.88	4.13	4.39	4.72	4.92
α_3	-.86	-.73	-.62	-.55	-.51	-.48	-.46	-.45	-.44	-.44	-.42	-.40	-.38	-.34	-.28	-.23
α_4	1.02	1.20	1.35	1.55	1.59	1.67	1.81	1.85	1.92	1.89	2.07	2.19	2.29	2.37	2.43	2.47
α_5	.1939	.2306	.2619	.2994	.3084	.3216	.3468	.3538	.3592	.3584	.3890	.4100	.4287	.4451	.4541	.4632
α_6	-.1397	-.1390	-.1435	-.1495	-.1509	-.1483	-.1493	-.1513	-.1496	-.1384	-.1436	-.1450	-.1442	-.1473	-.1481	-.1485
α_7	.0334	.0345	.0353	.0367	.0367	.0366	.0361	.0361	.0352	.0345	.0333	.0330	.0326	.0324	.0322	.0315
c/b	Pressure coefficient, P															
UPPER SURFACE	b 0.000	1.272	1.277	1.280	1.285	1.290	1.293	1.297	1.301	1.306	1.313	1.315	1.320	1.324	1.329	1.334
	b .025	.707	.505	.509	.521	.535	.542	.553	.566	.576	.587	.596	.606	.615	.628	.641
	b .050	.352	.339	.319	.310	.306	.291	.285	.283	.272	.270	.262	.251	.247	.244	.241
	b .100	.069	.058	.039	.029	.022	.002	-.012	-.020	-.035	-.041	-.052	-.063	-.066	-.066	-.067
	b .200	-.252	-.249	-.268	-.287	-.278	-.298	-.268	-.246	-.258	-.257	-.268	-.271	-.316	-.322	-.302
	b .300	-.344	-.350	-.361	-.363	-.364	-.370	-.369	-.365	-.369	-.364	-.365	-.371	-.369	-.367	-.367
	b .400	-.296	-.301	-.311	-.317	-.321	-.327	-.326	-.325	-.327	-.322	-.326	-.335	-.332	-.329	-.330
	b .500	-.375	-.367	-.365	-.352	-.359	-.361	-.357	-.354	-.358	-.357	-.360	-.367	-.362	-.357	-.356
	b .600	-.339	-.330	-.324	-.317	-.308	-.312	-.314	-.314	-.320	-.318	-.319	-.327	-.324	-.317	-.315
	b .700	-.400	-.396	-.394	-.394	-.393	-.392	-.387	-.388	-.392	-.388	-.388	-.394	-.390	-.382	-.379
LOWER SURFACE	b .800	-.448	-.445	-.445	-.442	-.444	-.440	-.442	-.438	-.439	-.438	-.438	-.442	-.438	-.427	-.424
	b .900	-.415	-.406	-.401	-.385	-.378	-.368	-.367	-.358	-.357	-.357	-.354	-.356	-.362	-.358	-.348
	b .950	-.267	-.388	-.513	-.612	-.649	-.666	-.667	-.664	-.664	-.657	-.652	-.653	-.649	-.639	-.627
	b .0375	-.551	-.509	-.465	-.415	-.370	-.322	-.272	-.229	-.164	-.070	.038	.121	.153	.187	.217
	b .075	-.471	-.435	-.391	-.343	-.295	-.243	-.185	-.114	.084	.115	.145	.164	.186	.215	.239
	b .150	-.430	-.409	-.375	-.328	-.270	-.208	.080	.103	.098	.100	.107	.124	.142	.164	.182
	b .250	-.117	.047	.138	.165	.154	.136	.130	.131	.129	.138	.147	.159	.173	.191	.206
	b .350	.101	.087	.063	.065	.118	.105	.091	.088	.089	.097	.105	.113	.124	.141	.151
	b .450	.082	.072	.049	.052	.071	.016	.102	.089	.072	.055	.087	.083	.102	.116	.127
	b .550	.063	.057	.051	.052	.029	-.033	.067	.093	.083	.078	.084	.088	.097	.111	.119
	b .650	.060	.058	.055	.061	.063	.058	.009	.061	.114	.111	.103	.101	.107	.122	.131
	b .750	.055	.055	.054	.065	.072	.063	.037	.053	.111	.082	.097	.097	.103	.118	.134
	b .850	.043	.047	.047	.054	.059	.060	.070	.071	.068	.012	.069	.078	.076	.092	.097
	b .925	.031	.038	.040	.039	.042	.041	.047	.047	.003	-.053	.014	.035	.036	.052	.045
	b .975	.023	.033	.035	.028	.027	.016	.003	-.003	-.052	-.100	-.032	-.003	.002	.013	.005
	b 1.000	.019	.029	.032	.022	.020	-.003	-.027	-.035	-.082	-.124	-.058	-.025	-.013	-.008	-.041

a No orifices.

b Paired value.

c Extrapolated value.



TABLE 9.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS OF AN

NACA 16-504.40 PROPELLER BLADE SECTION ($x = 0.95$) $\beta_x = 38.35^\circ$; $\beta_{0.75R} = 45^\circ$ - Concluded(a) $M = 0.65$; $\pi = 1$.

	2.277	2.245	2.225	2.199	2.178	2.159	2.125	2.115	2.103	2.068	2.064	2.042	2.019
$\frac{1}{2}C_{Df}$	1.060	1.069	1.076	1.082	1.089	1.100	1.103	1.115	1.123	1.126	1.136	1.144	1.150
$\frac{1}{2}C_{Df}$	1.01	1.40	1.65	1.97	2.23	2.47	2.90	3.01	3.18	3.63	3.68	3.97	4.27
$\frac{1}{2}C_{Df}$	-1.40	-1.33	-1.27	-1.19	-1.13	-1.07	-.96	-.93	-.89	-.77	-.76	-.68	-.60
$\frac{1}{2}C_{Df}$.95	1.06	1.10	1.20	1.30	1.35	1.47	1.57	1.64	1.80	1.84	1.91	1.95
$\frac{1}{2}C_{Df}$.1832	.2058	.2119	.2303	.2481	.2574	.2768	.2965	.3084	.3361	.3439	.3577	.3635
$\frac{1}{2}C_{Df}$	-.1323	-.1485	-.1458	-.1454	-.1416	-.1390	-.1369	-.1364	-.1345	-.1337	-.1360	-.1363	-.1337
$\frac{1}{2}C_{Df}$.0410	.0401	.0395	.0392	.0384	.0367	.0360	.0363	.0354	.0349	.0346	.0343	.0332
a/b	Pressure coefficient, P												
Upper surface	$a_{0.000}$	1.313	1.319	1.324	1.327	1.331	1.339	1.342	1.349	1.355	1.377	1.364	1.370
	$a_{.025}$.618	.632	.641	.652	.663	.673	.679	.698	.710	.717	.730	.740
	$a_{.050}$.460	.467	.463	.499	.495	.486	.472	.472	.468	.468	.461	.453
	$a_{.100}$.145	.130	.125	.120	.112	.099	.079	.077	.073	.068	.075	.077
	$a_{.200}$	-.159	-.147	-.177	-.155	-.155	-.156	-.164	-.162	-.156	-.163	-.156	-.164
	$a_{.300}$	-.264	-.272	-.270	-.269	-.265	-.267	-.271	-.265	-.268	-.266	-.264	-.270
	$a_{.400}$	-.223	-.237	-.235	-.236	-.235	-.238	-.245	-.243	-.242	-.244	-.242	-.247
	$a_{.500}$	-.307	-.313	-.312	-.307	-.305	-.305	-.309	-.305	-.299	-.301	-.294	-.297
	$a_{.600}$	-.298	-.292	-.287	-.281	-.277	-.274	-.272	-.264	-.254	-.250	-.245	-.247
	$a_{.700}$	-.369	-.370	-.365	-.356	-.348	-.343	-.338	-.330	-.321	-.319	-.312	-.314
Lower surface	$a_{.800}$	-.417	-.416	-.409	-.395	-.386	-.380	-.378	-.371	-.366	-.364	-.356	-.357
	$a_{.900}$	-.532	-.517	-.530	-.518	-.510	-.487	-.501	-.492	-.503	-.487	-.476	-.474
	$a_{.950}$	-.605	-.616	-.609	-.597	-.588	-.583	-.580	-.571	-.566	-.564	-.555	-.553
	$a_{0.000}$	-.0375	-.0427	-.0378	-.0348	-.0308	-.0272	-.0236	-.0193	-.0144	-.0106	-.0075	-.0066
	$a_{.075}$	-.075	-.074	-.087	-.087	-.087	-.087	-.087	-.087	-.087	-.087	-.087	-.087
	$a_{.150}$	-.130	-.134	-.134	-.134	-.134	-.134	-.134	-.134	-.134	-.134	-.134	-.134
	$a_{.250}$	-.192	-.192	-.192	-.192	-.192	-.192	-.192	-.192	-.192	-.192	-.192	-.192
	$a_{.350}$	-.242	-.242	-.242	-.242	-.242	-.242	-.242	-.242	-.242	-.242	-.242	-.242
	$a_{.450}$	-.009	-.075	-.106	-.148	-.156	-.163	-.168	-.168	-.176	-.179	-.189	-.196
	$a_{.550}$	-.095	-.098	-.100	-.107	-.106	-.103	-.093	-.095	-.104	-.111	-.123	-.131
	$a_{.650}$	-.110	-.103	-.102	-.105	-.104	-.101	-.101	-.107	-.116	-.124	-.136	-.144
	$a_{.750}$	-.066	-.056	-.055	-.058	-.059	-.061	-.059	-.067	-.076	-.086	-.099	-.106
	$a_{.850}$	-.051	-.063	-.051	-.047	-.045	-.041	-.036	-.042	-.049	-.059	-.073	-.078
	$a_{.925}$	-.108	-.083	-.064	-.054	-.051	-.048	-.047	-.042	-.043	-.043	-.060	-.063
	$a_{.975}$	-.124	-.098	-.077	-.061	-.058	-.058	-.058	-.052	-.045	-.038	-.055	-.056
	$a_{1.000}$	-.133	-.106	-.084	-.065	-.064	-.064	-.065	-.058	-.045	-.038	-.054	-.052

^aNo orifice.^bPaired value.^cExtrapolated value.

NACA

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($\alpha = 0.975^\circ$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$)(a) $N = 1140$ rpm.

	J	1.679	1.794	1.898	1.974	2.080	2.201	2.317	2.445	2.563	2.744	2.846	2.511	2.391	2.275	2.147	2.032	1.939	1.830	1.749	1.600
M_x		.607	.618	.627	.637	.644	.654	.668	.685	.695	.716	.704	.688	.678	.664	.642	.635	.629	.622	.615	.602
α_1		9.17	7.54	6.12	5.10	3.72	2.20	.80	-.70	-2.02	-3.95	-2.92	-1.45	-.08	1.30	2.87	4.34	5.57	7.04	8.17	10.32
$\Delta\delta$		1.16	.94	.74	.60	.45	.20	-.05	-.32	-.57	-.95	-.75	-.46	-.20	.05	.32	.50	.67	.87	1.02	1.31
α_1		5.87	5.17	4.28	3.67	3.05	2.30	1.61	1.09	.55	-.47	.09	.81	1.32	1.83	2.55	3.28	3.85	4.67	5.31	6.10
α_n		.6819	.5987	.4935	.4229	.3548	.2700	.1884	.1265	-.0639	-.0548	-.0110	-.0942	-.1529	-.2139	-.2981	-.3813	-.4432	-.5406	-.6123	-.7097
α_m		-.0787	-.0785	-.0793	-.0753	-.0723	-.0702	-.0679	-.0674	-.0705	-.0767	-.0764	-.0688	-.0666	-.0678	-.0696	-.0725	-.0771	-.0785	-.0831	-.0773
α_c		-.0394	-.0251	-.0120	-.0079	-.0034	-.0025	-.0073	-.0143	-.0174	-.0223	-.0192	-.0151	-.0105	-.0067	-.0011	-.0038	-.0083	-.0165	-.0280	-.0455
Pressure coefficient, P																					
Upper surface		1.095	1.099	1.102	1.105	1.108	1.111	1.117	1.123	1.127	1.135	1.131	1.125	1.121	1.115	1.111	1.104	1.102	1.100	1.098	1.093
		-.025	-1.638	-1.587	-.847	-.448	-.272	-.016	.237	.448	.535	.658	.604	.485	.336	.153	-.112	-.379	-.525	-1.396	-1.619
		.050	-1.540	-1.072	-.569	-.442	-.324	-.164	-.002	.161	.286	.338	.287	.186	.067	-.056	-.232	-.372	-.517	-.711	-1.259
		.100	-.860	-.542	-.483	-.409	-.325	-.244	-.147	-.031	.001	.086	.047	-.025	-.104	-.181	-.281	-.379	-.463	-.535	-1.277
		.200	-.460	-.439	-.384	-.338	-.291	-.246	-.196	-.118	-.121	-.076	-.097	-.137	-.172	-.213	-.270	-.327	-.380	-.427	-.493
		.300	-.415	-.379	-.327	-.289	-.249	-.215	-.182	-.118	-.139	-.118	-.129	-.142	-.164	-.194	-.236	-.280	-.326	-.365	-.401
		.400	-.433	-.391	-.341	-.306	-.272	-.244	-.210	-.156	-.178	-.152	-.163	-.184	-.198	-.223	-.262	-.300	-.340	-.377	-.414
		.500	-.391	-.351	-.309	-.275	-.241	-.214	-.183	-.125	-.146	-.150	-.140	-.151	-.170	-.194	-.231	-.272	-.311	-.346	-.378
		.600	-.399	-.361	-.320	-.289	-.256	-.231	-.201	-.145	-.171	-.160	-.163	-.173	-.189	-.211	-.249	-.285	-.323	-.355	-.385
		.700	-.397	-.363	-.323	-.296	-.266	-.241	-.210	-.156	-.184	-.177	-.179	-.187	-.200	-.223	-.260	-.292	-.328	-.355	-.385
		.800	-.366	-.337	-.306	-.279	-.254	-.235	-.207	-.151	-.178	-.170	-.175	-.181	-.195	-.219	-.254	-.282	-.313	-.332	-.356
		.900	-.349	-.326	-.303	-.282	-.261	-.244	-.219	-.165	-.201	-.211	-.203	-.199	-.207	-.231	-.260	-.285	-.313	-.328	-.346
		.950	-.220	-.204	-.181	-.165	-.144	-.132	-.108	-.057	-.093	-.106	-.095	-.091	-.099	-.121	-.144	-.168	-.195	-.205	-.218
Lower surface		.0375	.521	.453	.363	.281	.178	-.036	-.125	-.232	-.534	-1.004	-.838	-.362	-.195	-.072	.079	.211	.294	.401	.467
		.075	.385	.331	.262	.202	.130	.032	-.061	-.116	-.273	-.598	-.427	-.211	-.106	-.037	.058	.148	.206	.288	.338
		.150	.278	.241	.193	.156	.110	.049	0	-.020	-.125	-.326	-.208	-.089	-.031	.010	.060	.116	.150	.208	.244
		.250	.205	.181	.148	.124	.093	.049	.019	.024	-.055	-.177	-.097	-.034	.002	.028	.056	.001	.112	.153	.179
		.350	.167	.149	.124	.105	.083	.058	.028	.042	-.022	-.103	-.048	-.007	.015	.034	.053	.077	.091	.125	.145
		.450	.161	.145	.127	.113	.097	.065	.044	.063	.006	-.050	-.013	.017	.035	.050	.070	.089	.098	.127	.141
		.550	.138	.126	.112	.100	.087	.060	.042	.066	.015	-.024	.002	.023	.035	.045	.061	.077	.085	.108	.120
		.650	.111	.099	.089	.078	.067	.047	.033	.060	.015	-.013	.005	.020	.027	.034	.043	.057	.061	.083	.095
		.750	.100	.094	.086	.078	.070	.050	.041	.072	.028	.010	.022	.033	.036	.041	.047	.057	.059	.076	.084
		.850	.085	.087	.085	.078	.077	.060	.058	.092	.051	.041	.052	.057	.055	.054	.053	.061	.058	.066	.070
		.925	.076	.078	.082	.083	.083	.073	.074	.112	.075	.069	.074	.077	.073	.071	.066	.067	.059	.067	.066
		.975	.139	.135	.120	.145	.135	.145	.164	.128	.116	.143	.114	.113	.103	.091	.093	.078	.118	.118	.118
		1.000	.215	.200	.153	.220	.200	.197	.212	.208	.183	.162	.197	.145	.152	.127	.108	.122	.115	.187	.200

No orifice.

b Paired value.



TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75H} = 45^\circ$; $B = 2$) - Continued(b) $N = 1350$ rpm.

J	2.739	2.628	2.502	2.408	2.323	2.231	2.152	2.049	2.097	2.169	2.257	2.355	2.470	2.575	2.696
M_x	.855	.835	.817	.804	.791	.778	.769	.760	.763	.764	.782	.796	.811	.828	.845
α_L	-3.90	-2.73	-1.35	-.27	.73	1.83	2.81	4.12	3.50	2.60	1.40	.35	-.98	-2.37	-3.45
$\Delta\delta$	-1.52	-1.19	-.72	-.43	-.18	.09	.33	.64	.50	.28	-.01	-.27	-.62	-.98	-1.40
α_1	-.50	.12	.86	1.40	1.85	2.31	2.90	3.49	3.21	2.74	2.12	1.65	1.04	.47	-.23
c_n	-.0594	.0135	.0994	.1632	.2155	.2703	.3394	.4058	.3755	.3213	.2471	.1935	.1213	.0548	-.0271
c_m	-.0882	-.0926	-.0859	-.0783	-.0793	-.0824	-.0826	-.0839	-.0832	-.0836	-.0810	-.0777	-.0813	-.0822	-.0918
c_o	-.0266	-.0223	-.0174	-.0130	-.0069	-.0049	-.0002	-.0049	-.0019	-.0026	-.0071	-.0104	-.0155	-.0190	-.0214
c/b	Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.195	1.186	1.178	1.172	1.167	1.161	1.157	1.153	1.155	1.155	1.162	1.168	1.175	1.183
	.025	.708	.643	.536	.443	.303	.132	-.089	-.344	-.214	-.018	.195	.355	.498	.595
	.050	.394	.327	.227	.138	.030	-.096	-.245	-.418	-.329	-.196	-.049	.070	.193	.283
	.100	.118	.063	-.009	-.077	-.151	-.231	-.317	-.409	-.362	-.291	-.201	-.125	-.034	.030
	.200	-.086	-.113	-.148	-.183	-.220	-.259	-.302	-.353	-.325	-.288	-.244	-.210	-.158	-.098
	.300	-.139	-.151	-.161	-.175	-.198	-.228	-.258	-.300	-.278	-.248	-.214	-.193	-.163	-.114
	.400	-.173	-.171	-.182	-.195	-.213	-.239	-.265	-.303	-.283	-.257	-.226	-.209	-.184	-.170
	.500	-.187	-.175	-.171	-.188	-.208	-.233	-.262	-.296	-.277	-.253	-.221	-.203	-.173	-.162
	.600	-.212	-.195	-.202	-.215	-.231	-.256	-.285	-.317	-.300	-.277	-.245	-.228	-.204	-.197
	.700	-.226	-.215	-.219	-.230	-.246	-.273	-.298	-.327	-.311	-.291	-.261	-.242	-.218	-.212
	.800	-.229	-.243	-.223	-.232	-.251	-.276	-.299	-.325	-.311	-.294	-.267	-.248	-.223	-.217
Lower surface	.900	-.276	-.244	-.231	-.237	-.254	-.281	-.301	-.327	-.313	-.296	-.268	-.250	-.229	-.233
	.950	-.107	-.086	-.085	-.097	-.113	-.138	-.156	-.181	-.166	-.152	-.126	-.110	-.087	-.093
	$a_{0.000}$	-1.193	-1.178	-.981	-.198	-.158	-.034	.099	.201	.154	.059	-.070	-.193	-.775	-1.101
	.075	-.965	-1.006	-.158	-.141	-.073	-.011	.075	.140	.110	.048	-.033	-.105	-.126	-.748
	.150	-.306	-.119	-.071	-.075	-.014	.019	.067	.103	.089	.055	.015	-.036	-.063	-.068
	.250	-.212	-.096	-.027	-.010	.014	.037	.062	.082	.073	.055	.032	.001	-.014	-.041
	.350	-.162	-.055	0	.016	.031	.048	.062	.074	.069	.058	.045	.021	.011	-.015
	.450	-.100	-.015	.021	.034	.045	.058	.079	.086	.085	.074	.055	.036	.029	.009
	.550	-.054	.021	.034	.041	.052	.063	.083	.086	.086	.078	.063	.044	.043	.028
	.650	-.032	.013	.029	.034	.040	.046	.058	.059	.061	.055	.046	.032	.034	.023
	.750	.001	.033	.042	.041	.046	.049	.058	.058	.060	.056	.051	.040	.046	.040
	$b_{0.900}$.048	.063	.068	.067	.060	.060	.063	.060	.068	.067	.058	.059	.067	.049
	.925	.084	.098	.095	.088	.083	.078	.080	.078	.081	.081	.081	.095	.098	.094
	$b_{0.975}$.142	.152	.175	.162	.158	.162	.172	.138	.142	.140	.152	.181	.160	.183
	$a_{1.000}$.188	.205	.250	.258	.250	.282	.284	.220	.222	.205	.230	.300	.220	.260

^aNo orifice.^bPaired value.

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(c) $N = 1500$ rpm.

	σ	M_x	α_x	$\Delta\delta$	α_t	α_n	α_m	α_g					
		2.067	2.145	2.254	2.378	2.475	2.561	2.551	2.434	2.336	2.235	2.119	2.040
		.844	.892	.865	.884	.899	.917	.910	.890	.874	.860	.842	.833
		3.89	2.90	1.55	.08	-1.04	-2.22	-1.89	-.57	.57	1.78	3.22	4.23
		.78	.46	.03	-.45	-.89	-1.45	-1.29	-.70	-.28	.11	.57	.88
		3.73	3.03	2.35	1.55	.89	.16	.34	1.15	1.85	2.30	3.26	3.91
		.4381	.3552	.2748	.1797	.1045	.0187	.0400	.1342	.2168	.2700	.3826	.4977
		-.0915	-.0896	-.0885	-.0901	-.1008	-.1137	-.1055	-.0960	-.0864	-.0882	-.0882	-.0909
		-.0019	.0028	.0096	.0157	.0199	.0248	.0216	.0180	.0137	.0090	.0021	-.0045
c/b		Pressure coefficient, P											
Upper surface	a	0.000	1.191	1.195	1.201	1.210	1.219	1.228	1.224	1.214	1.206	1.199	1.190
	b	.025	-.189	.046	.274	.412	.567	.665	.642	.528	.398	.225	-.047
	c	.050	-.347	-.179	0	.158	.260	.356	.333	.222	.105	-.035	-.246
	d	.100	-.473	-.313	-.193	-.076	.002	.085	.063	-.028	-.116	-.217	-.357
	e	.200	-.371	-.315	-.259	-.206	-.180	-.151	-.162	-.182	-.222	-.267	-.338
	f	.300	-.303	-.263	-.232	-.198	-.179	-.209	-.192	-.183	-.208	-.237	-.276
	g	.400	-.329	-.294	-.262	-.236	-.219	-.233	-.208	-.225	-.242	-.266	-.308
	h	.500	-.312	-.274	-.244	-.213	-.193	-.169	-.169	-.198	-.220	-.248	-.287
	i	.600	-.347	-.309	-.286	-.262	-.252	-.236	-.240	-.254	-.265	-.284	-.321
	j	.700	-.377	-.342	-.316	-.293	-.285	-.275	-.274	-.287	-.293	-.314	-.350
	k	.800	-.364	-.337	-.324	-.316	-.313	-.293	-.297	-.307	-.296	-.309	-.341
	l	.900	-.357	-.318	-.285	-.246	-.237	-.333	-.238	-.230	-.254	-.290	-.333
	m	.950	-.164	-.135	-.108	-.074	-.047	-.017	-.026	-.099	-.084	-.116	-.150
Lower surface	a	.0375	.198	.079	-.097	-.625	-.801	-.888	-.879	-.771	-.377	-.060	.118
	b	.075	.144	.065	-.043	-.259	-.746	-.843	-.835	-.697	-.071	-.019	.090
	c	.150	.121	.074	.033	.004	-.277	-.700	-.691	.036	-.008	.040	.099
	d	.250	.092	.072	.041	.016	.054	-.317	-.021	.027	.021	.050	.086
	e	.350	.085	.077	.044	.024	.035	.053	.065	.023	.030	.050	.077
	f	.450	.105	.090	.062	.044	.045	.078	.068	.044	.051	.067	.088
	g	.550	.097	.085	.062	.046	.043	.063	.056	.044	.051	.064	.082
	h	.650	.071	.062	.046	.033	.030	.041	.043	.031	.037	.049	.059
	i	.750	.067	.062	.049	.040	.038	.045	.037	.038	.042	.049	.056
	j	.850	.079	.079	.070	.069	.070	.080	.075	.060	.065	.069	.070
	k	.925	.087	.092	.091	.094	.103	.118	.113	.098	.092	.089	.084
	l	.975	.100	.106	.105	.118	.120	.152	.162	.132	.114	.102	.094
	m	1.000	.104	.114	.114	.138	.125	.170	.200	.157	.125	.110	.099

a) No orifice.

b) Paired values.

NACA

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$;

$\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued.

(a) $N = 1600$ rpm.

J M_∞ α β ϕ θ ψ χ ζ	2.177 .907 2.50 .47 2.92 .3419 -.1010 .0123	2.278 .925 1.26 -.10 2.21 .2590 -.0980 .0190	2.370 .940 1.17 -.60 1.37 .1619 -.1069 .0241	2.460 .955 -.87 -1.07 .67 .0781 -.1116 .0283	2.553 .973 -1.93 -1.45 -.34 -.0394 -.1113 .0347	2.581 .973 -2.22 -1.51 -.79 -.0929 -.1049 .0373	2.507 .960 -1.40 -1.30 .20 .0232 -.1144 .0312	2.423 .946 -.44 -.88 1.07 .1292 -.1090 .0266	2.323 .928 .72 -.34 1.76 .2065 -.1009 .0220	2.232 .912 1.82 .17 2.53 .2955 -.0974 .0154	2.119 .893 3.22 .78 3.35 .3923 -.1024 .0051
a/b	Pressure coefficient, P										
Upper surface	.0000 .025 .050 .100 .200 .300 .400 .500 .600 .700 .800 .900 .950	1.223 .214 -.040 -.230 -.347 -.266 -.280 -.269 -.318 -.383 -.422 -.448 -.073	1.232 .391 .105 -.121 -.289 -.213 -.233 -.244 -.303 -.340 -.384 -.471 -.069	1.241 .520 .218 -.027 -.248 -.200 -.201 -.214 -.268 -.305 -.347 -.504 -.080	1.249 .620 .320 .063 -.176 -.213 -.274 -.248 -.299 -.281 -.316 -.485 -.097	1.259 .710 .410 .143 -.098 -.174 -.237 -.239 -.298 -.351 -.362 -.472 -.110	1.252 .666 .366 .101 -.137 -.163 -.259 -.259 -.294 -.302 -.316 -.485 -.124	1.244 .577 .277 .023 -.209 -.233 -.228 -.203 -.252 -.292 -.318 -.504 -.093	1.234 .462 .165 -.071 -.253 -.211 -.224 -.232 -.285 -.318 -.365 -.494 -.068	1.225 .304 .032 -.174 -.313 -.237 -.249 -.263 -.323 -.360 -.404 -.437 -.069	1.216 .066 -.150 -.333 -.384 -.301 -.328 -.312 -.358 -.416 -.445 -.337 -.100
Lower surface	.0375 .075 .150 .250 .350 .450 .550 .650 .750 .850 .925 .975 a1.000	.009 .022 .070 .065 .063 .076 .073 .051 .049 .060 .076 .088 .093	-.319 -.022 .022 .033 .038 .097 .052 .033 .031 .046 .063 .076 .082	-.560 -.503 -.221 .078 .056 .058 .049 .026 .022 .037 .056 .074 .082	-.679 -.644 -.506 -.365 .018 .088 .074 .043 .030 .043 .058 .085 .098	-.754 -.724 -.610 -.451 -.369 -.248 -.003 .040 .041 .058 .071 .089 .094	-.780 -.749 -.642 -.474 -.399 -.337 -.203 -.006 .026 .051 .070 .078 .080	-.739 -.706 -.587 -.423 -.297 .035 .067 .051 .029 .023 .058 .071 .091	-.661 -.624 -.481 -.003 .033 .046 .056 .024 .024 .041 .061 .076 .084	-.525 -.449 .057 .033 .031 .046 .044 .040 .024 .041 .071 .085 .092	.110 .087 .103 .084 .078 .086 .083 .061 .061 .054 .082 .100 .108

^aNo orifices.
^bPaired values.

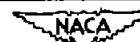


TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Continued(a) $M = 0.56$.

J	2.147	2.179	2.218	2.258	2.284	2.314	2.354	2.395	2.434	2.475	2.517	2.560	2.610	2.654	2.697
M_x	.988	.978	.968	.960	.950	.942	.932	.922	.913	.904	.895	.886	.879	.870	.859
α_x	2.87	2.47	1.99	1.51	1.19	.83	.36	-.12	-.57	-1.04	-1.51	-1.99	-2.53	-3.01	-3.46
α_1	0	-.12	-.21	-.28	-.32	-.36	-.46	-.61	-.76	-.92	-1.07	-1.20	-1.36	-1.48	-1.60
α_2	2.80	2.62	2.30	2.14	1.91	1.82	1.60	1.44	1.18	.93	.54	.15	-.09	-.36	-.53
α_n	.3265	.3077	.2684	.2490	.2239	.2110	.1877	.1677	.1368	.1077	.0626	.0174	-.0097	-.0413	-.0619
α_m	-.1255	-.1254	.1170	-.1080	-.1019	-.0998	-.0990	-.1013	-.1006	-.1001	-.1008	-.1024	-.0985	-.0995	-.0926
α_c	.0295	.0294	.0271	.0249	.0238	.0227	.0203	.0210	.0201	.0193	.0197	.0204	.0214	.0221	.0238
a/b	Pressure coefficient, P														
Upper surface	1.000	1.268	1.262	1.257	1.252	1.246	1.242	1.236	1.231	1.226	1.222	1.217	1.212	1.211	1.203
	.025	.360	.381	.404	.438	.475	.466	.487	.520	.548	.570	.611	.636	.665	.685
	.050	.094	.105	.121	.147	.160	.168	.186	.216	.240	.260	.297	.322	.351	.370
	.100	-.120	-.109	-.098	-.078	-.071	-.066	-.054	-.031	-.012	.003	.033	.053	.080	.095
	.200	-.287	-.288	-.288	-.285	-.279	-.269	-.260	-.224	-.200	-.186	-.160	-.145	-.124	-.109
	.300	-.239	-.239	-.239	-.223	-.200	-.199	-.205	-.198	-.186	-.178	-.164	-.157	-.142	-.137
	.400	-.264	-.260	-.253	-.226	-.222	-.221	-.226	-.226	-.220	-.218	-.208	-.203	-.189	-.181
	.500	-.255	-.247	-.232	-.221	-.222	-.226	-.229	-.214	-.203	-.194	-.178	-.171	-.156	-.156
	.600	-.295	-.286	-.286	-.279	-.279	-.286	-.279	-.267	-.256	-.254	-.233	-.216	-.200	-.193
	.700	-.334	-.333	-.331	-.321	-.319	-.317	-.309	-.303	-.296	-.287	-.261	-.251	-.230	-.219
	.800	-.385	-.383	-.380	-.368	-.362	-.363	-.357	-.350	-.337	-.318	-.283	-.260	-.225	-.209
Lower surface	.900	-.543	-.542	-.542	-.535	-.532	-.520	-.478	-.398	-.297	-.237	-.215	-.216	-.212	-.214
	.950	-.632	-.615	-.507	-.309	-.174	-.105	-.065	-.038	-.034	-.041	-.044	-.049	-.050	-.060
	.0375	-.059	-.156	-.268	-.343	-.422	-.504	-.573	-.652	-.716	-.783	-.878	-.958	-1.028	-1.102
	.075	.009	-.024	-.151	-.279	-.376	-.459	-.533	-.614	-.674	-.736	-.827	-.903	-.967	-1.036
	.150	.064	.049	.045	.068	.073	.067	.025	-.124	-.203	-.300	-.511	-.673	-.748	-.811
	.250	.064	.055	.042	.047	.045	.043	.048	.060	.063	.079	.095	.038	.017	-.016
	.350	.065	.063	.037	.047	.043	.036	.042	.070	.072	.051	.060	.053	.030	.007
	.450	.073	.066	.055	.062	.053	.045	.044	.047	.049	.046	.048	.042	.039	.027
	.550	.064	.058	.053	.052	.048	.042	.041	.044	.048	.046	.049	.044	.044	.034
	.650	.035	.032	.022	.026	.023	.019	.001	.026	.031	.031	.034	.031	.030	.024
	.750	.021	.021	.012	.018	.016	.014	.001	.029	.037	.041	.046	.043	.045	.039
	.850	.027	.027	.015	.021	.015	.024	.021	.049	.070	.069	.076	.070	.074	.071
	.925	.057	.048	.035	.035	.035	.044	.061	.081	.098	.103	.112	.112	.117	.112
	.975	.103	.075	.060	.060	.061	.072	.108	.127	.128	.140	.154	.156	.162	.164
	1.000	.135	.095	.080	.077	.081	.091	.140	.156	.145	.164	.182	.185	.192	.197

*No orifice.

bFairied value.

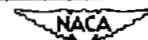


TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($\alpha = 0.975$; $\beta_T = 37.90^\circ$) $\beta_{0.75R} = 45^\circ$; $B = 2$ - Continued $(r) M = 0.58$.

$\frac{J}{M}$ α_T $\Delta\beta$ α_1 α_n α_m α_c	2.148	2.181	2.214	2.251	2.285	2.318	2.354	2.394	2.434	2.473	2.519	2.555	2.593	2.647	2.693
$\frac{J}{M}$	1.024	1.014	1.004	.995	.985	.976	.967	.957	.947	.938	.930	.919	.912	.901	.892
α_T	2.86	2.45	2.04	1.99	1.18	.78	.36	-.11	-.57	-1.02	-1.53	-1.93	-2.35	-2.93	-3.42
$\Delta\beta$.01	-.20	-.38	-.54	-.65	-.72	-.75	-.79	-.88	-.99	-1.16	-1.31	-1.45	-1.64	-1.78
α_1	2.55	2.34	2.17	2.00	1.81	1.60	1.35	1.15	1.02	.79	.61	.40	.22	-.21	-.42
α_n	.2987	.2729	.2542	.2339	.2103	.1871	.1590	.1355	.1200	.0935	.0716	.0465	.0278	-.0245	-.0490
α_m	-.1218	-.1200	-.1168	-.1191	-.1213	-.1160	-.1122	-.1109	-.1075	-.1095	-.1101	-.1083	-.1055	-.1082	-.1062
α_c	.0315	.0307	.0290	.0306	.0322	.0299	.0265	.0264	.0263	.0246	.0248	.0242	.0235	.0241	.0243
c/b	Pressure coefficient, P														
Upper surface	0.000	1.290	1.283	1.277	1.272	1.266	1.261	1.256	1.250	1.244	1.240	1.235	1.230	1.224	1.215
	.430	.430	.435	.439	.445	.450	.453	.455	.457	.459	.461	.463	.465	.468	.476
	.050	.169	.185	.188	.204	.219	.229	.247	.265	.287	.308	.326	.346	.367	.413
	.100	-.060	-.041	-.042	-.025	-.013	-.007	.006	.019	.033	.048	.060	.076	.094	.133
	.200	-.231	-.231	-.239	-.234	-.234	-.233	-.224	-.216	-.204	-.187	-.175	-.160	-.141	-.104
	.300	-.208	-.213	-.232	-.240	-.243	-.242	-.241	-.240	-.233	-.226	-.222	-.215	-.194	-.180
	.400	-.231	-.226	-.233	-.222	-.233	-.235	-.247	-.258	-.257	-.250	-.252	-.252	-.212	-.194
	.500	-.220	-.211	-.209	-.198	-.204	-.202	-.203	-.209	-.204	-.187	-.180	-.173	-.164	-.174
	.600	-.258	-.247	-.252	-.249	-.252	-.253	-.255	-.256	-.247	-.238	-.236	-.237	-.230	-.212
	.700	-.293	-.290	-.296	-.292	-.294	-.295	-.292	-.287	-.281	-.277	-.281	-.277	-.259	-.243
Lower surface	.800	-.342	-.338	-.340	-.335	-.334	-.332	-.331	-.330	-.325	-.319	-.317	-.299	-.279	-.245
	.900	-.487	-.486	-.490	-.489	-.491	-.493	-.495	-.494	-.484	-.448	-.402	-.325	-.247	-.222
	.950	-.572	-.572	-.576	-.576	-.554	-.402	-.248	-.153	-.084	-.030	-.016	-.015	-.028	-.056
	.0375	-.125	-.196	-.250	-.321	-.400	-.457	-.527	-.593	-.657	-.728	-.795	-.859	-.938	-1.006
	.075	-.073	-.187	-.249	-.314	-.385	-.436	-.503	-.565	-.625	-.691	-.757	-.816	-.889	-.954
	.150	.100	.115	.056	-.094	-.231	-.296	-.368	-.429	-.488	-.556	-.623	-.679	-.746	-.807
	.250	.082	.086	.080	.092	.086	.081	.089	-.069	-.137	-.198	-.269	-.295	-.276	-.365
	.350	.071	.066	.057	.065	.073	.076	.081	.078	.077	.074	.061	.054	.043	-.019
	.450	.092	.084	.071	.070	.072	.072	.077	.078	.082	.084	.080	.077	.066	.054
	.550	.080	.072	.060	.058	.055	.055	.057	.058	.063	.067	.064	.065	.058	.053
	.650	.050	.042	.032	.029	.023	.024	.025	.026	.033	.040	.038	.040	.039	-.037
	.750	.031	.026	.018	.015	.011	.012	.014	.017	.025	.036	.038	.044	.046	.047
	b ^a .850	.057	.048	.036	.028	.023	.020	.021	.030	.047	.070	.076	.079	.081	.083
	.925	.096	.083	.067	.056	.044	.038	.036	.039	.061	.089	.101	.113	.119	.123
	b ^a .975	.137	.117	.098	.087	.067	.056	.073	.067	.087	.149	.138	.140	.160	.171
	a ^b 1.000	.159	.136	.115	.105	.080	.067	.112	.085	.110	.208	.165	.168	.205	.215

^aNo orifice.^bPaired value.

NACA

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($x = 0.975$; $B_x = 37.90^\circ$; $B_{0.75R} = .45^\circ$; $B = 2$) - Continued(g) $M = 0.60$.

J	2.143	2.172	2.205	2.243	2.275	2.308	2.330	2.375	2.411	2.447	2.477	2.525	2.555	2.600	2.642
M_x	1.059	1.050	1.039	1.034	1.025	1.015	1.004	.997	.988	.979	.967	.960	.949	.939	.931
α_x	2.92	2.56	2.15	1.68	1.30	.90	.64	.11	-.31	-.72	-1.06	-1.60	-1.93	-2.43	-2.88
$\Delta\theta$	-.48	-.49	-.52	-.60	-.70	-.83	-.92	-1.11	-1.23	-1.32	-1.38	-1.45	-1.50	-1.57	-1.64
c_{L1}	2.20	2.07	1.79	1.60	1.44	1.23	1.03	.93	.64	.45	.31	.10	-.04	-.36	-.60
c_{L2}	.2552	.2416	.2084	.1868	.1687	.1445	.1200	.1094	.0752	.0523	.0358	.0123	-.0045	-.0413	-.0703
c_m	-.1220	-.1206	-.1173	-.1186	-.1214	-.1209	-.1236	-.1236	-.1204	-.1183	-.1171	-.1191	-.1209	-.1183	-.1200
c_c	.0293	.0310	.0305	.0315	.0330	.0324	.0338	.0345	.0335	.0311	.0309	.0306	.0302	.0296	.0293
c/b	Pressure coefficient, P														
Upper surface	$a_{0.000}$	1.312	1.307	1.299	1.296	1.290	1.284	1.277	1.273	1.267	1.262	1.256	1.251	1.245	1.240
	$a_{0.025}$.485	.494	.522	.541	.552	.569	.581	.600	.623	.646	.655	.678	.691	.713
	$a_{0.050}$.215	.217	.241	.255	.266	.279	.288	.305	.326	.345	.353	.374	.386	.405
	$a_{0.100}$	-.003	0	.020	.031	.038	.047	.052	.063	.076	.091	.094	.110	.118	.133
	$a_{0.200}$	-.193	-.197	-.191	-.188	-.187	-.186	-.184	-.175	-.163	-.150	-.147	-.133	-.127	-.111
	$a_{0.300}$	-.208	-.216	-.216	-.215	-.209	-.206	-.207	-.203	-.199	-.197	-.202	-.196	-.198	-.194
	$a_{0.400}$	-.227	-.236	-.247	-.246	-.245	-.253	-.259	-.257	-.255	-.250	-.258	-.258	-.260	-.253
	$a_{0.500}$	-.206	-.207	-.202	-.203	-.209	-.226	-.240	-.248	-.257	-.263	-.272	-.267	-.272	-.274
	$a_{0.600}$	-.237	-.235	-.229	-.230	-.232	-.240	-.251	-.261	-.273	-.280	-.289	-.295	-.293	-.289
	$a_{0.700}$	-.262	-.265	-.260	-.259	-.260	-.265	-.271	-.272	-.272	-.274	-.279	-.278	-.266	-.252
Lower surface	$b_{0.0375}$	-.143	-.181	-.243	-.292	-.345	-.395	-.456	-.510	-.574	-.626	-.692	-.752	-.816	-.884
	$b_{0.075}$	-.140	-.178	-.245	-.295	-.347	-.397	-.455	-.504	-.561	-.606	-.665	-.719	-.778	-.840
	$b_{0.150}$	-.028	-.081	-.149	-.189	-.227	-.274	-.330	-.378	-.434	-.482	-.546	-.601	-.658	-.715
	$b_{0.250}$.112	.109	.014	-.060	-.102	-.178	-.229	-.267	-.314	-.348	-.394	-.435	-.479	-.523
	$b_{0.350}$.117	.107	.090	.046	.029	-.013	-.053	-.098	-.191	-.147	-.154	-.202	-.220	-.282
	$b_{0.450}$.095	.093	.098	.104	.105	.105	.098	.092	.079	.066	.049	.026	.023	.011
	$b_{0.550}$.076	.073	.076	.081	.081	.083	.082	.081	.082	.083	.074	.071	.066	.061
	$b_{0.650}$.040	.037	.039	.042	.044	.045	.046	.048	.052	.057	.051	.055	.053	.054
	$b_{0.750}$.022	.017	.018	.020	.021	.023	.027	.029	.036	.043	.041	.050	.051	.058
	$b_{0.850}$.053	.051	.043	.041	.040	.028	.023	.032	.038	.048	.050	.078	.080	.093
	$b_{0.925}$.113	.103	.093	.084	.072	.064	.054	.049	.047	.054	.060	.089	.103	.122
Paired values	$b_{0.975}$.169	.143	.134	.120	.100	.101	.084	.060	.056	.077	.096	.143	.160	.180
	$b_{1.000}$.204	.167	.157	.140	.113	.123	.103	.069	.060	.112	.150	.212	.208	.220

^aNo orifice.^bPaired values.

TABLE 10.- PRESSURE COEFFICIENTS AND AERODYNAMIC CHARACTERISTICS

OF THE BLADE SECTION ($\alpha = 0.975$; $\beta_x = 37.90^\circ$; $\beta_{0.75R} = 45^\circ$; $B = 2$) - Concluded(h) $M = 0.65$.

	J	2.110	2.136	2.150	2.164	2.199	2.222	2.235	2.273	2.293	2.324	2.354	2.383	2.413	2.450	2.483	2.520
M_x	1.162	1.152	1.144	1.135	1.127	1.121	1.113	1.101	1.090	1.080	1.072	1.060	1.052	1.042	1.034	1.025	
α_x	3.34	3.01	2.83	2.66	2.22	1.94	1.78	1.32	1.08	.71	.36	.02	-.33	-.76	-1.13	-1.54	
$\Delta\delta$	-.950	-1.038	-1.080	-1.130	-1.235	-1.300	-1.338	-1.432	-1.480	-1.550	-1.618	-1.670	-1.718	-1.765	-1.810	-1.840	
α_1	1.90	1.68	1.57	1.43	1.27	1.18	1.06	.82	.63	.47	.27	.02	-.28	-.36	-.59	-.87	
c_n	-.2187	-.1935	-.1813	-.1639	-.1477	-.1368	-.1226	-.0961	-.0742	-.0548	-.0316	-.0026	-.0323	-.0426	-.0697	-.1019	
c_m	-.1036	-.1070	-.1044	-.1047	-.1055	-.1047	-.1027	-.1029	-.1014	-.1000	-.0998	-.0909	-.0900	-.0891	-.0857	-.0865	
c_c	.0309	.0317	.0324	.0332	.0334	.0338	.0345	.0355	.0360	.0375	.0382	.0395	.0400	.0410	.0421	.0430	
c/b	Pressure coefficient, P																
Upper surface	$a_{0.000}$	1.383	1.375	1.370	1.363	1.357	1.353	1.348	1.340	1.333	1.326	1.321	1.313	1.307	1.301	1.297	1.290
	.025	.582	.611	.607	.609	.616	.623	.637	.635	.660	.678	.684	.695	.703	.712	.728	.741
	.050	.322	.344	.336	.336	.341	.346	.356	.372	.377	.392	.397	.405	.414	.419	.436	.446
	.100	.098	.126	.121	.118	.124	.128	.133	.146	.149	.160	.162	.168	.170	.172	.184	.191
	.200	-.077	-.066	-.076	-.084	-.084	-.086	-.085	-.080	-.081	-.075	-.074	-.072	-.070	-.069	-.056	-.050
	.300	-.109	-.100	-.113	-.124	-.128	-.134	-.135	-.134	-.134	-.127	-.129	-.134	-.139	-.143	-.140	-.131
	.400	-.144	-.142	-.157	-.172	-.175	-.181	-.184	-.173	-.175	-.170	-.176	-.181	-.183	-.185	-.181	-.186
	.500	-.144	-.138	-.155	-.169	-.173	-.178	-.178	-.179	-.186	-.187	-.195	-.208	-.216	-.223	-.222	-.215
	.600	-.166	-.160	-.177	-.188	-.193	-.203	-.210	-.210	-.215	-.217	-.228	-.239	-.248	-.255	-.257	-.257
	.700	-.184	-.179	-.199	-.216	-.223	-.234	-.242	-.243	-.249	-.255	-.265	-.276	-.284	-.290	-.288	-.292
	.800	-.224	-.216	-.236	-.252	-.258	-.270	-.275	-.274	-.278	-.282	-.293	-.303	-.308	-.314	-.314	-.323
	.900	-.354	-.347	-.364	-.376	-.383	-.393	-.401	-.404	-.410	-.418	-.432	-.446	-.455	-.463	-.465	-.475
	.950	-.420	-.416	-.431	-.445	-.450	-.460	-.468	-.473	-.480	-.489	-.504	-.520	-.532	-.540	-.546	-.555
Lower surface	$a_{0.000}$	-.0375	-.004	-.052	-.083	-.117	-.150	-.184	-.211	-.249	-.291	-.339	-.386	-.429	-.480	-.522	-.573
	.075	-.002	-.045	-.078	-.111	-.141	-.178	-.215	-.259	-.302	-.351	-.397	-.442	-.489	-.528	-.573	-.615
	.150	.040	.004	-.027	-.061	-.087	-.121	-.152	-.186	-.225	-.264	-.304	-.344	-.387	-.424	-.467	-.511
	.250	.051	.024	-.004	-.034	-.053	-.081	-.103	-.127	-.153	-.180	-.211	-.247	-.279	-.309	-.340	-.374
	.350	.109	.084	.031	-.017	-.022	-.043	-.066	-.085	-.103	-.120	-.150	-.200	-.232	-.240	-.290	-.314
	.450	.162	.133	.083	.037	.013	-.012	-.033	-.053	-.075	-.096	-.124	-.155	-.184	-.208	-.234	-.261
	.550	.147	.155	.125	.074	.041	.004	-.020	-.038	-.056	-.075	-.103	-.135	-.162	-.187	-.213	-.240
	.650	.103	.115	.096	.079	.059	.024	-.016	-.047	-.075	-.096	-.127	-.166	-.192	-.214	-.236	-.262
	.750	.083	.091	.072	.063	.059	.050	.040	.021	.009	-.009	-.037	-.119	-.146	-.156	-.175	-.178
	.850	.107	.116	.094	.069	.082	.090	.091	.086	.072	.059	.044	-.010	-.029	-.038	-.050	-.049
	.925	.139	.151	.129	.120	.122	.124	.130	.138	.133	.123	.110	.091	.082	.075	.070	.062
	.975	.167	.188	.148	.160	.154	.152	.161	.180	.175	.180	.179	.171	.171	.157	.161	.151
	$a_{1.000}$.180	.207	.158	.180	.170	.166	.176	.201	.195	.218	.231	.215	.218	.200	.210	.197

^aNo orifice.^bFaired value.

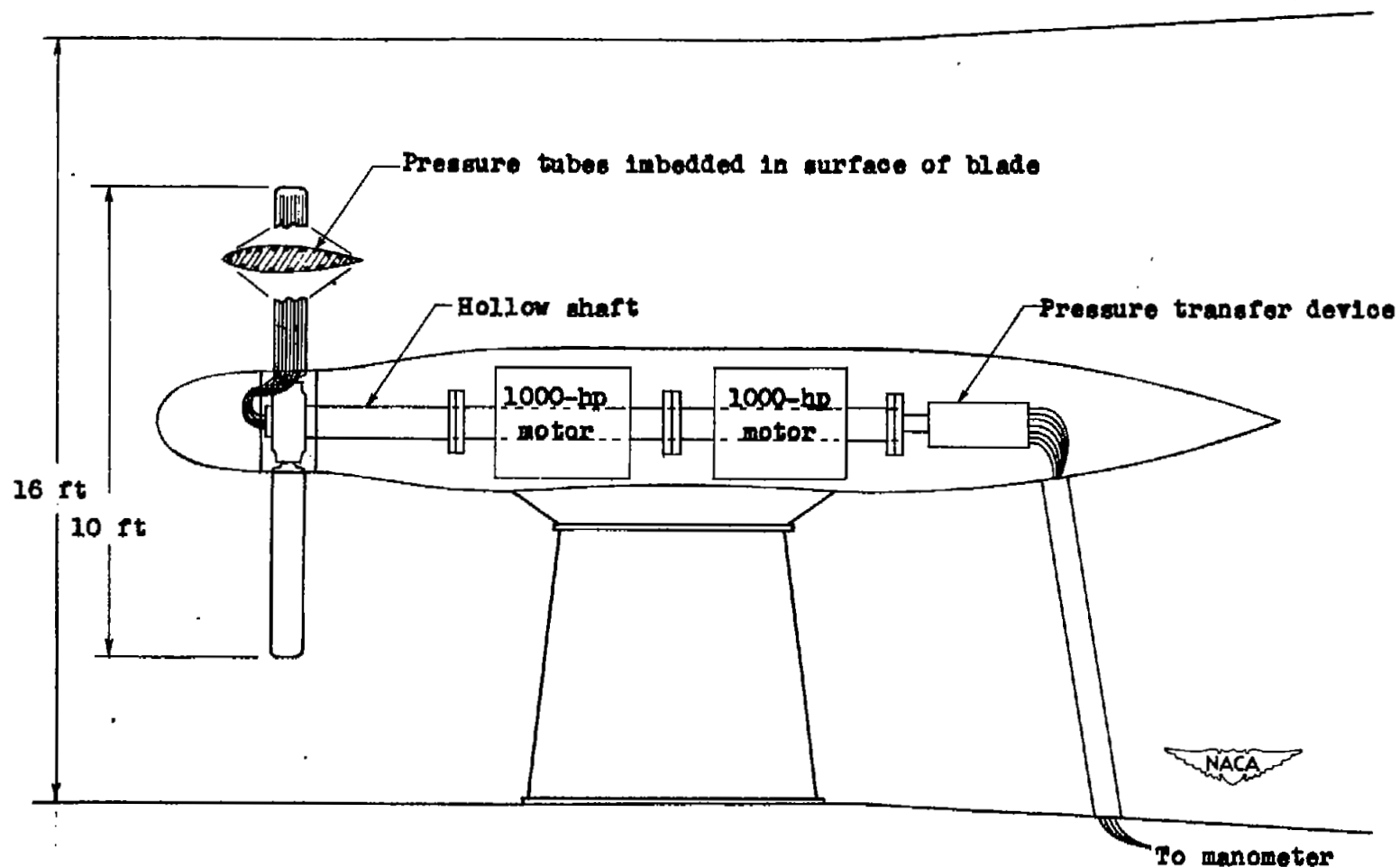


Figure 1.- Diagram of the apparatus used to obtain pressure distributions on the sections of operating propellers.

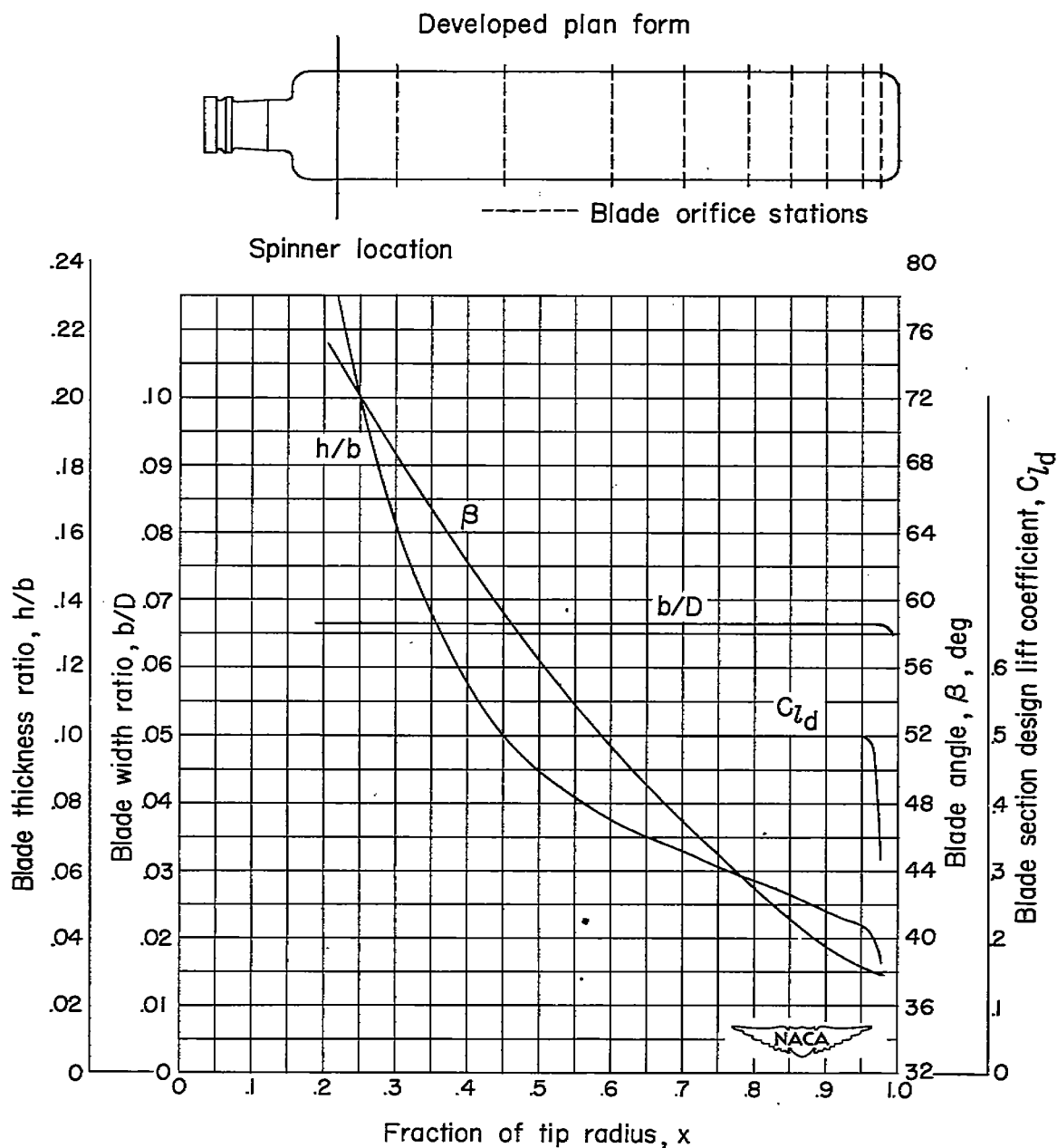


Figure 2.- Blade-form curves for NACA 10-(5)(066)-03.

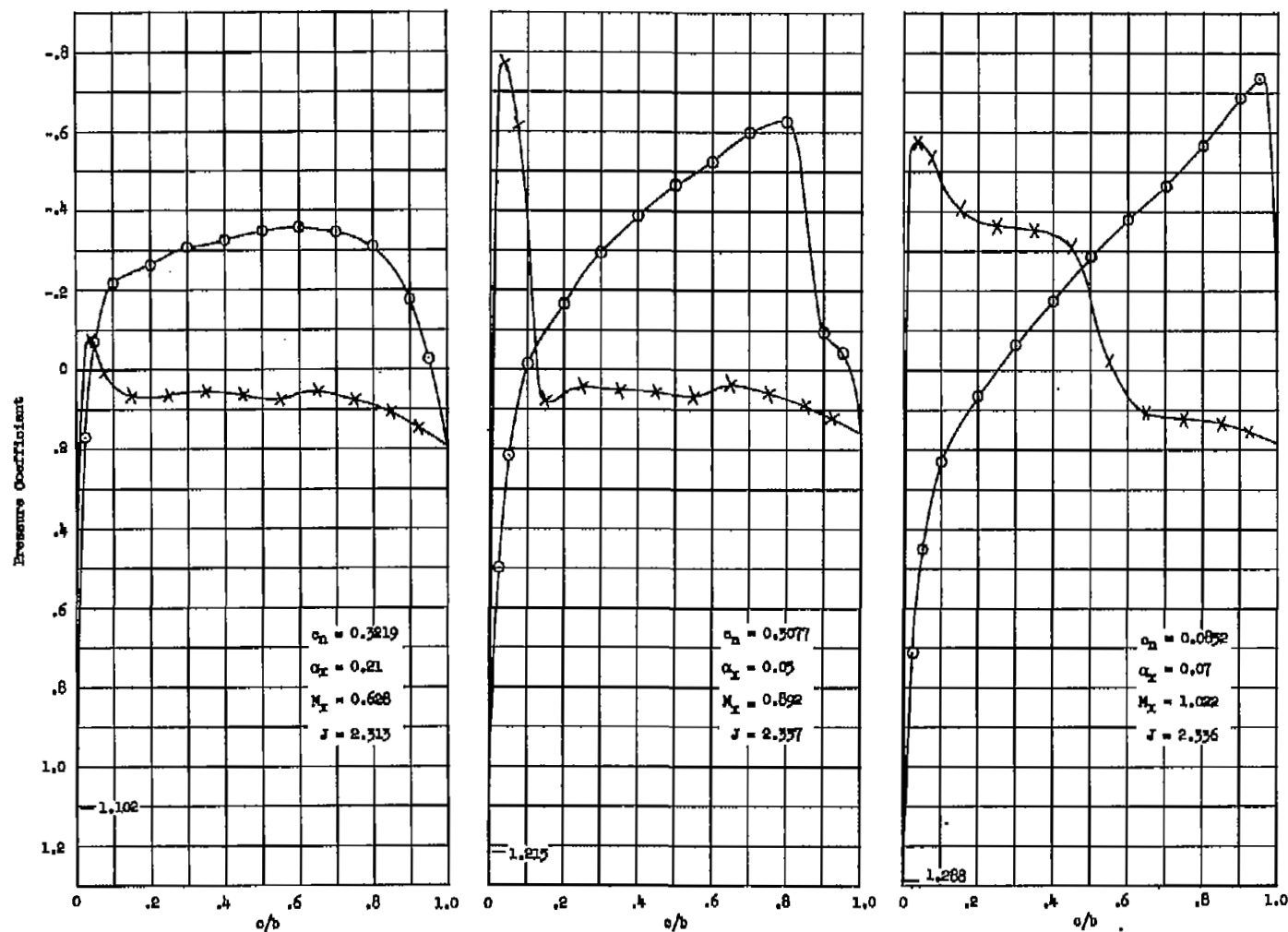


Figure 4.- Typical pressure distributions along the chord of the NACA 16-504.80 blade section located at the $x = 0.90$ radius.



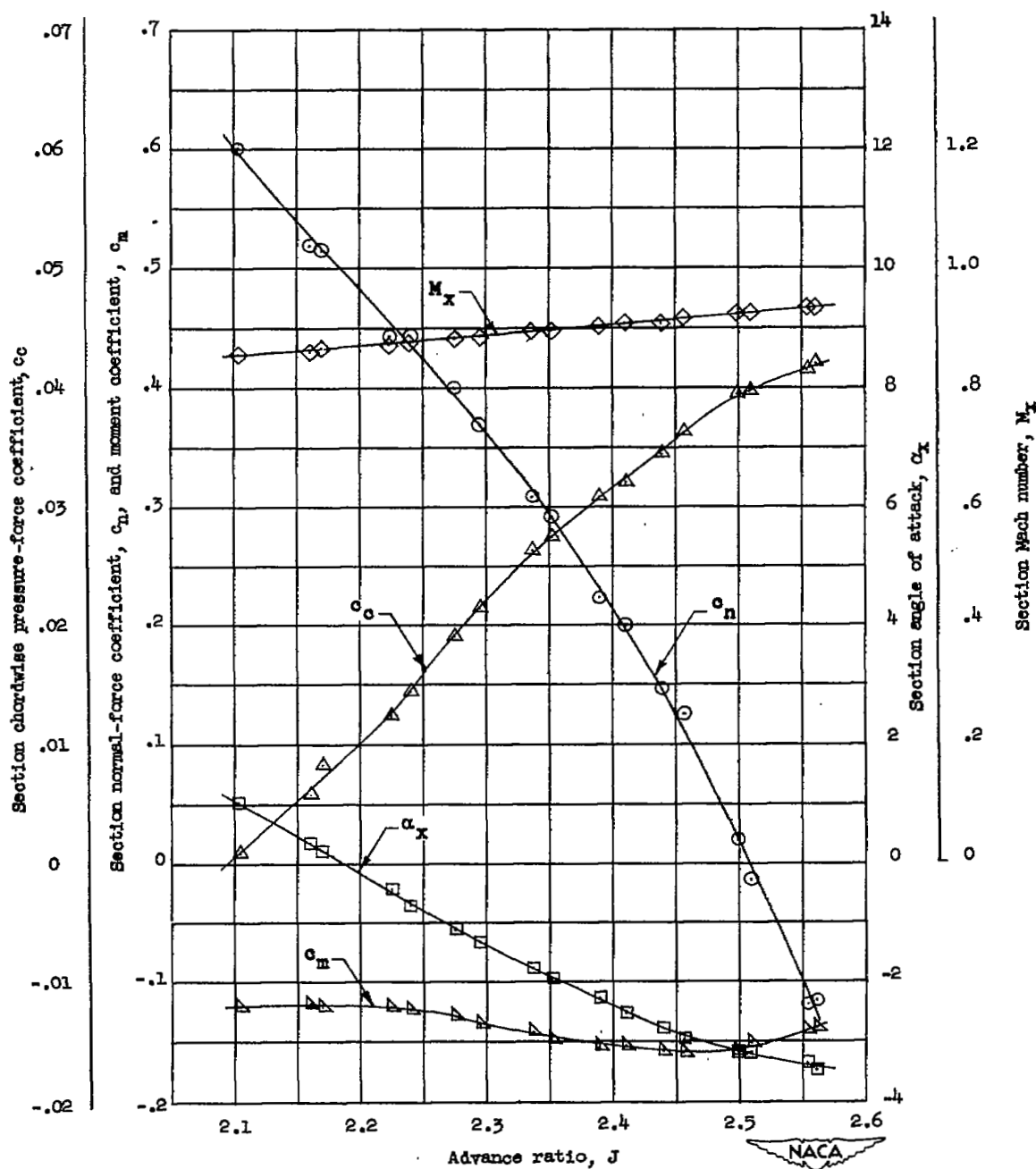


Figure 5.- Variation of section normal-force coefficient, moment coefficient, chordwise pressure-force coefficient, angle of attack, and Mach number with advance ratio for the blade section at the 0.90 radius, from table 8(d). $\beta_{0.75R} = 45^\circ$; 1600 rpm.

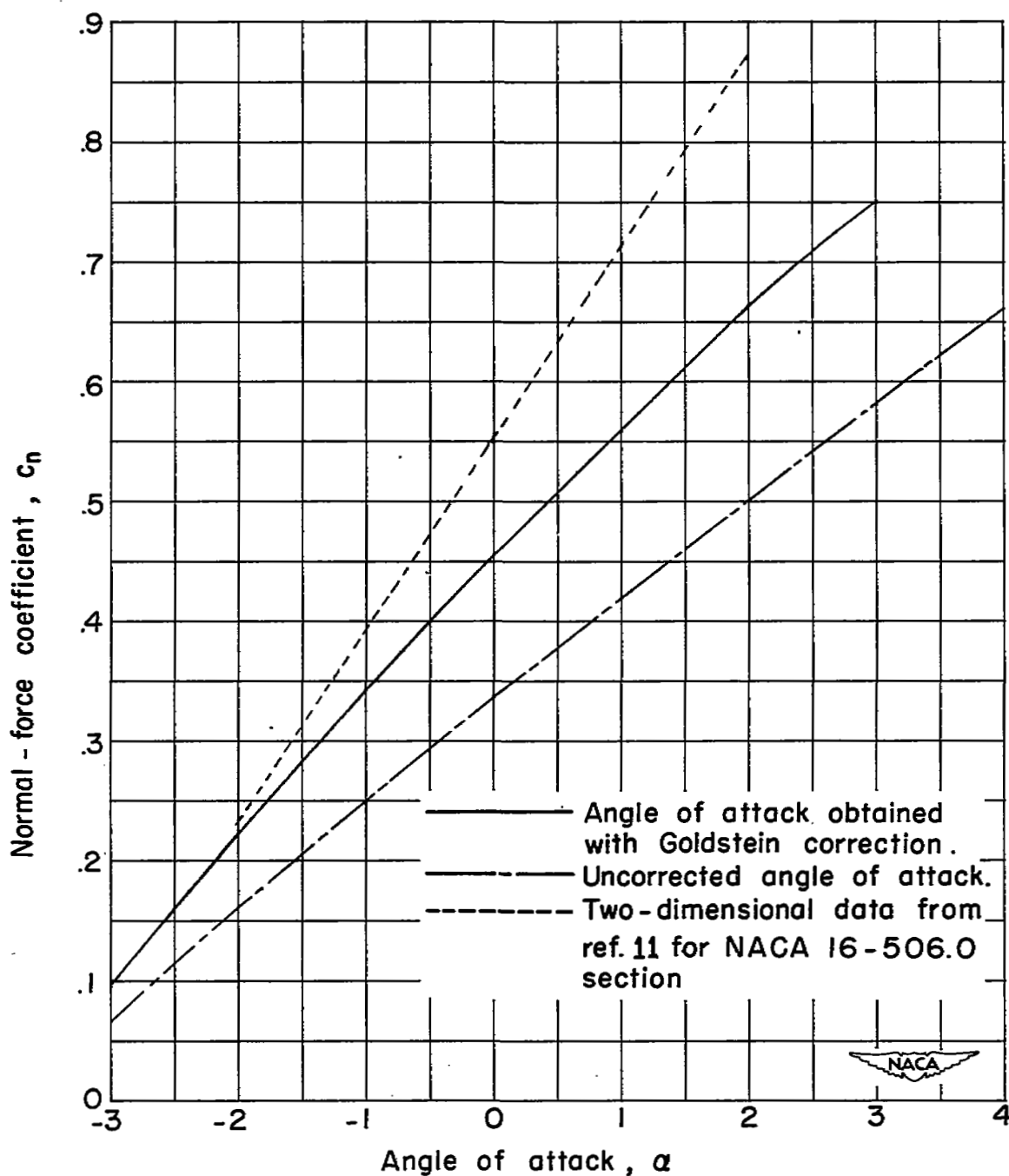


Figure 6.- Variation of normal-force coefficient with angle of attack for NACA 16-505.85 section showing effect of induced angle correction. $x = 0.78$; $M_x = 0.70$.



LANGLEY RESEARCH CENTER

3 1176 01360 5713

DO NOT REMOVE SLIP FROM MATERIAL

Delete your name from this slip when returning material to the library.

NAME	DATE	MS
Shelby Mom's	12/6/95	185